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16. Abstract <p>The Network Analysis Program (NAP-II), which has the capability of simultaneously solving for orbits and tracking station error model terms, was, after several modifications, used in the calibration of Minitrack stations using Minitrack satellite measurements (self-calibration). Several support programs were written to aid in this task.</p> <p>A simultaneous four-arc solution was obtained. A comparison with optically determined arcs for the same time spans showed RMS position differences of 67m, 86m, 124m and 168m for the 4 arcs considered.</p> <p>An apparatus incorporating a diffraction grating was designed and successfully used to measure the drift rate of the Fort Myers MOTS camera drive.</p>			
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PREFACE

The objective of this work was to perform a study, prepare a Minitrack error model with as many of the coefficients as practical being established by pre-flight calibration measurements, prepare a computational method to utilize the error model, and to monitor the MOTS camera drive stability using a diffraction grating.

The NAP-II program, which has the capability of simultaneously solving for orbits and tracking station error model terms, was modified to substantially increase its computational speed and substantially reduce its disk memory requirements, thus making it possible to meet the contract objective within the required time-scale.

Twenty-five short optically determined reference arcs were used to calibrate the Fort Myers Minitrack station.

The NAP program was used to obtain a simultaneous four-arc solution (total length 25 days) of the 4 orbits and Minitrack station calibration numbers (for all stations).

A diffraction grating was designed and used for monitoring the stability of the Fort Myers MOTS camera drive.

The multi-arc approach to the self-calibration of Minitrack stations appears to give very good results when judged on the comparison between Minitrack and optically determined orbits. The four arcs processed under this contract showed RMS position differences of 67m, 86m, 124m and 168m, respectively. This compares favorably with an RMS position difference of 165m for the first arc based on "aircraft calibrated" Minitrack measurements.

Use of the diffraction grating apparatus developed under this contract provides a simple and inexpensive means of correcting plate errors caused by the (periodic) instability of the MOTS camera drive.

It is recommended that the approach to Minitrack self-calibration developed under this contract be further tested using other satellites (than GEOS-I) before "aircraft calibration" is finally abandoned.

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SECTION 1

MONITORING OF MOTS STABILITY BY MEANS OF A DIFFRACTION GRATING APPARATUS

1.1 INTRODUCTION

The NASA MOTS camera and the U. S. Air Force PC-1000 camera employ the same 1000mm f/5 Baker telephoto lens. The PC-1000 uses an alt-azimuth mount and is locked in a fixed orientation (relative to the earth) throughout each exposure. A precisely timed shutter provides intermittent exposures of star trails to serve as control points. The MOTS camera, by contrast, uses an equatorial mount and is sidereally driven to maintain a fixed orientation with respect to the right ascension declination frame. By virtue of this mode of operation, MOTS does not require a precisely timed shutter and provides a greater abundance of stellar images than a PC-1000. Both MOTS and PC-1000 can potentially produce accuracies of about 0.6 seconds of arc for satellite directions. This potential, however, may not be routinely realized.

One of the key advantages claimed for the PC-1000 (and for the fixed camera mode of operation, in general) is that any significant drift in the orientation of the camera throughout an exposure can be detected (and generally corrected for) by virtue of separate reductions performed on each sequence of stellar exposures. Brown, (Reference 1) reports results of an investigation of the stability of a PC-1000 over a period of about one half hour. Reductions were performed on exposures made at 5 minute intervals, leading to results plotted in Figure 1, which depicts the temporal variation of the three angular elements of orientation about their respective means. The plotted results for hour angle are normalized by the customary process of multiplication by cosine of declination. Each point is accompanied by a vertical bar defining its plus and minus 1 sigma confidence intervals. The 1 sigma values for declination and normalized hour angle are slightly less than 0.2 second of arc; for swing angle, they are

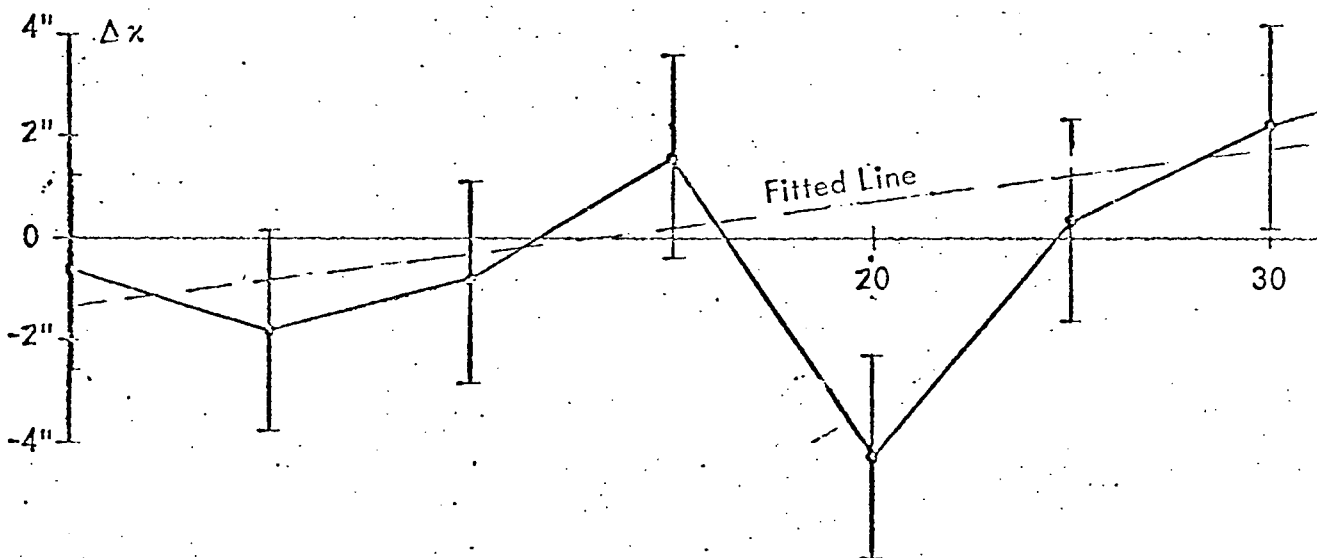
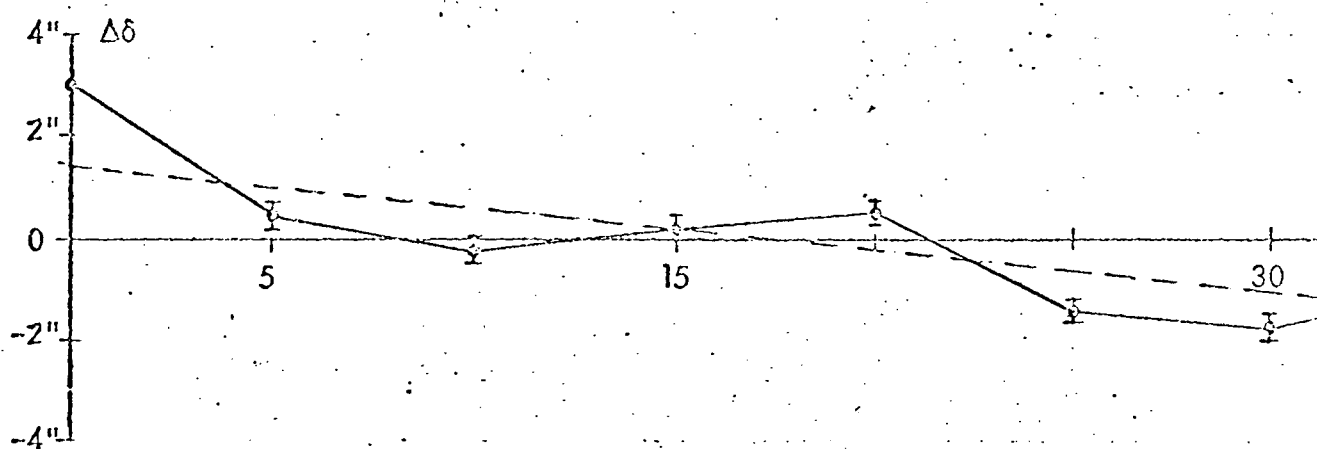
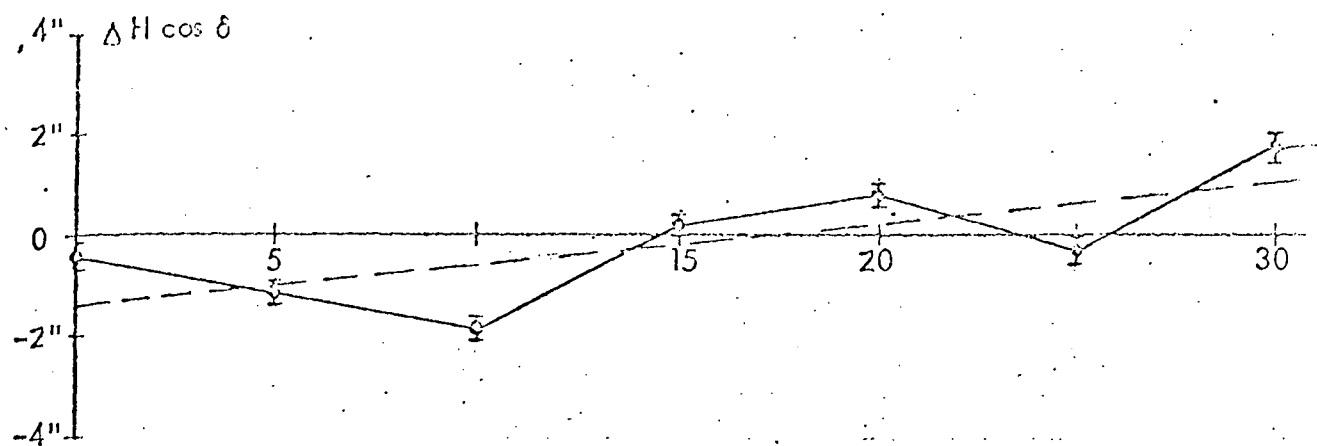


FIGURE 1. Variation in angular stability of PC-1000 camera over period of 35 minutes as reported in reference 1.

generally about ten times greater, averaging close to 2 seconds of arc. This disparity in sigmas is attributable to the fact that the focal length (1000mm) of the PC-1000 is about 10 times greater than the semi-diagonal of the plate format. The projective effect of an error of 0.2 second of arc in the direction of the camera axis is equivalent to that of an error of about 1 micron on the plate. By the same token, the projective effect of an error of 2 seconds in swing angle is equivalent to that of an error of about 1 micron near the edge of the plate. Thus, there is no actual projective disparity in the relative sigmas of the angular elements.

Figure 1 clearly demonstrates that significant changes in the orientation of the PC-1000 can occur throughout a period as short as 5 minutes. Indeed, changes in hour angle and declination of as much as 2 seconds of arc in 5 minutes are not unusual. Be this as it may, the fact is that in a fixed camera operation, any changes of significance can be detected and their effects on directions of satellites can be largely removed by an interpolative process. Thus while stability is a problem in PC-1000 operations, it is a problem that can be routinely overcome.

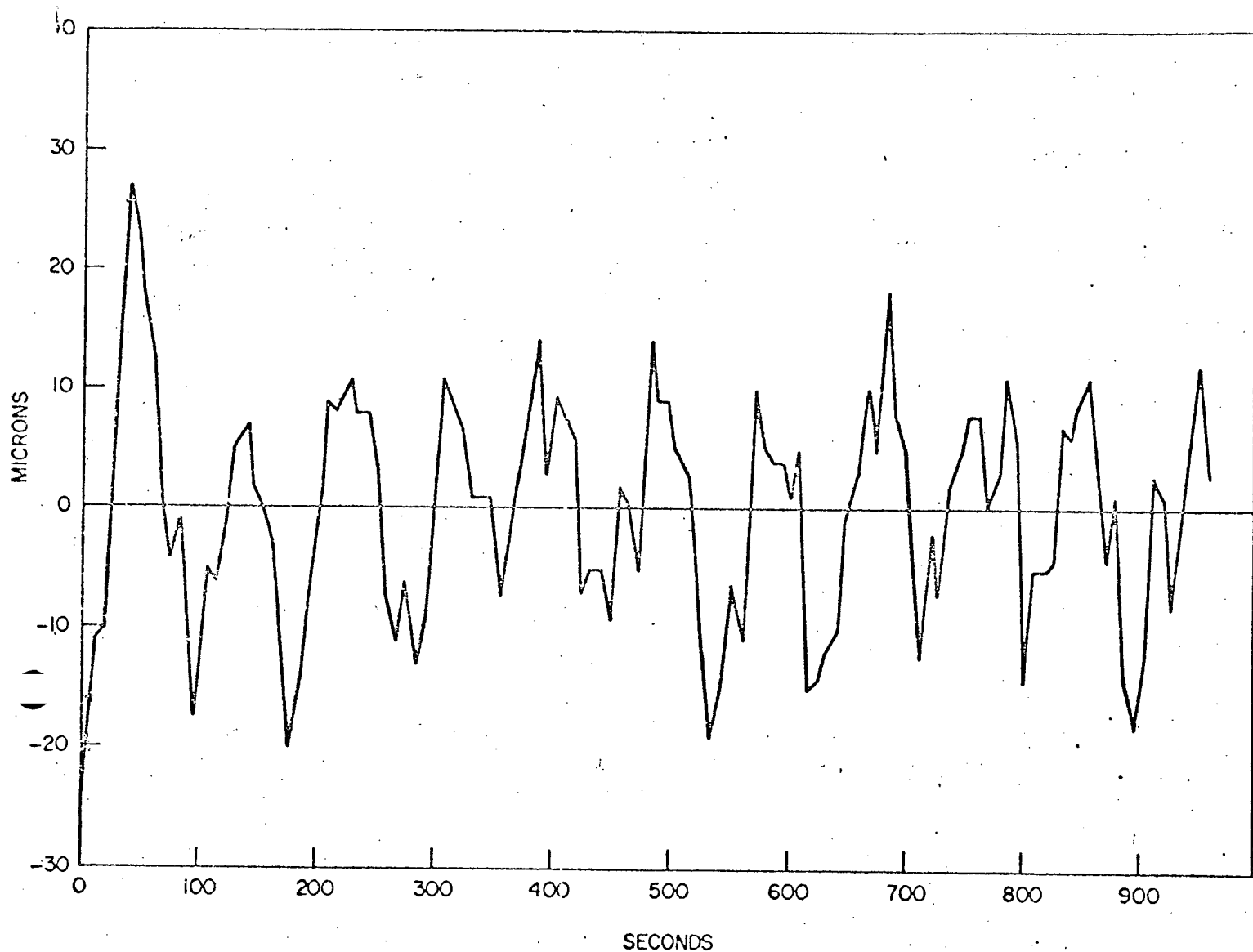
In general, MOTS is subject to the same sources of instability as the PC-1000 (e.g., thermal imbalances, wind loading, etc.). However, MOTS is also subject to drifts induced by the sidereal drive. Whatever their origin, small instabilities in MOTS orientation cannot be routinely detected because their primary effect is merely to cause a slight enlargement in the sizes of stellar images. This is a matter of no consequence insofar as the plate reduction itself is concerned, for instability affects all stars alike and hence does not degrade the residuals produced by the least squares adjustment. However, flashes are affected by the instantaneous rather than the integrated effects of instability. Hence, satellite directions derived from MOTS observations inherit fully the instantaneous departures in orientation of the camera from the mean orientation deduced from the stellar exposures. Clearly then, a simple, practical, routine means for monitoring the stability of MOTS orientation throughout an exposure would constitute a significant advance. The objective of the present investigation is to evaluate an approach that holds promise in this regard.

1.2 GENERAL CHARACTERISTICS OF ERROR INDUCED BY MOTS SIDEREAL DRIVE

A study reported by Harris, Cartwright and Oosterhout (Reference 2) provides a good understanding of the nature of the errors induced by the MOTS sidereal drive. The data analyzed in Reference 2 consists of MOTS images of a stationary collimator generating an artificial star produced by a pinhole illuminated by a strobe light of 1 millisecond duration flashing at 10 second intervals. The exposures of the flashing collimator were made over a period of 16 minutes with the MOTS axis in a nominally horizontal orientation and with the camera being driven in the normal sidereal mode. This generated a set of almost 100 successive images which, with a flawless drive, would ideally be at a constant declination and spaced at equal increments of hour angle. Departures of actual images from their ideal positions provide the desired measure of errors of the drive. In the analysis provided in Reference 1, polynomials in time were fitted to the measured x and y coordinates of the collimator images in order to account for low order effects such as the slight curvature of the trials. The residuals about the fitted polynomials reflect the combined effect of plate measuring errors and higher order sidereal drifts (slow thermal drifts and the like would be absorbed by the fitted polynomials).

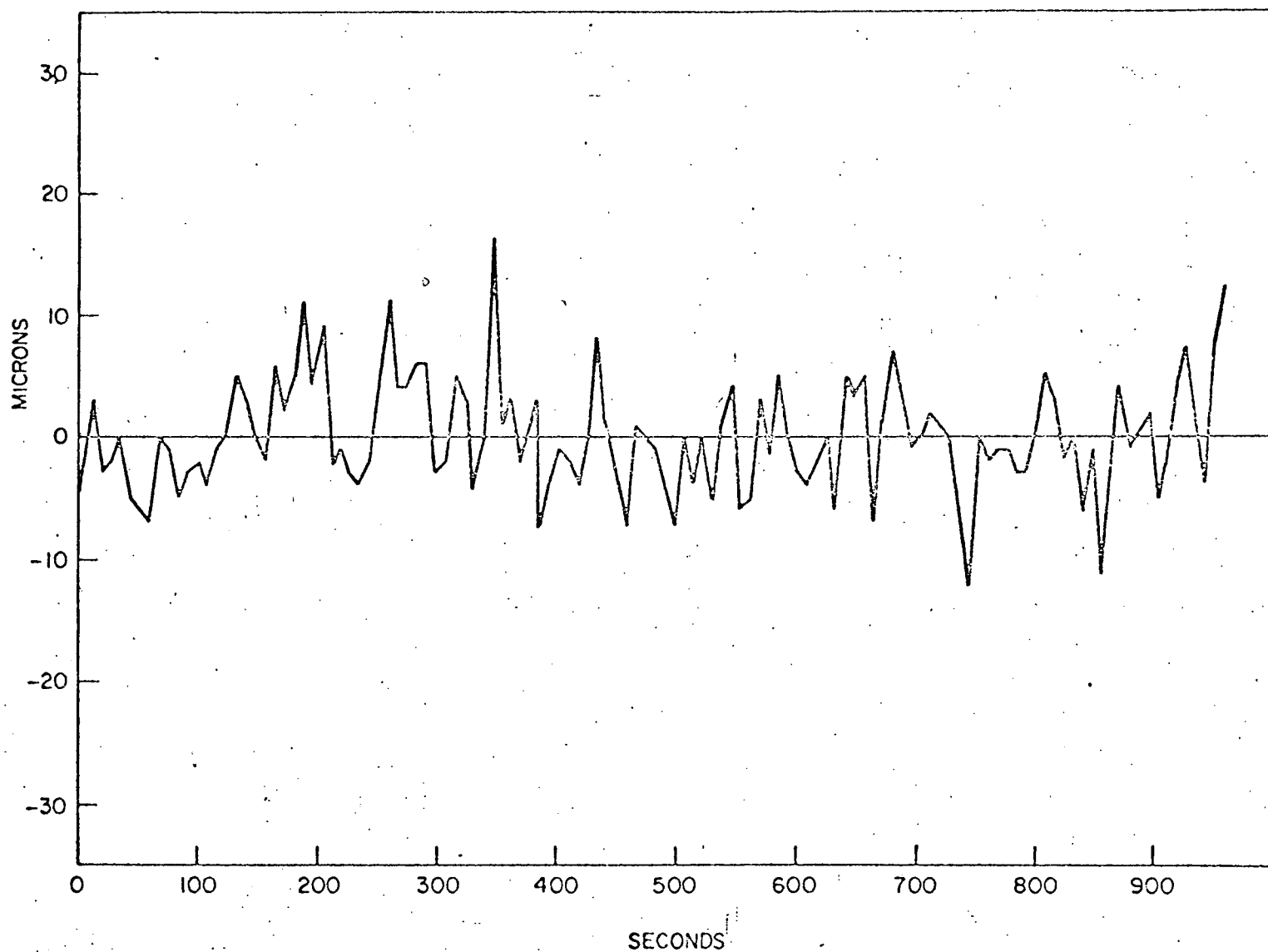
Graphs of residuals in right ascension and declination for a particular trial presented in Reference 2 are reproduced in Figures 2 and 3 below. The most significant finding of Reference 1, namely the existence of a well defined periodic drift in right ascension, is well illustrated in Figure 2. The period of the drift is almost precisely 90 seconds and is attributed to the interaction of the worm and sector gears of the drive system. The amplitude of the drift is reported in most cases to range between 2 and 3 arc seconds in right ascension and to be only about half as great in declination.

Because of geometrical considerations, the procedure employed in Reference 1 to monitor MOTS stability is not one that can be practically adopted to effect a routine calibration of drift affecting operational plates. The procedure has served well, however, to define the essential characteristics of MOTS drift, thereby making clear the problem to be overcome by any method designed for routine operational calibration of drift.



Sudbury Data Pass No.6 6th Power Residuals ΔX vs. Time


FIGURE 2. Angular stability of MOTS in right ascension as determined by flashing collimator method reported in reference [2] (5 microns = 1 second of arc).



Sudbury Data Pass No. 6 Quadratic Residuals ΔY vs. Time

FIGURE 3. Angular stability of MOTS in declination as determined by flashing collimator method reported in reference [2] (5 microns = 1 second of arc).

1.3 THE DIFFRACTION GRATING METHOD

The present investigation is concerned with the evaluation of a method of monitoring MOTS stability proposed to NASA by DBA Systems. As originally conceived, it involved placement of a coarse diffraction grating in front of the MOTS lens to generate measurable first order diffraction images of sufficiently bright stars. A series of six exposures would be made at suitable intervals with orientation of the grating being changed in nominal 15 degree steps between exposures. This sequence of exposures was to provide material for a 'precalibration' of MOTS drift. Shortly before the exposure of the satellite, the diffraction grating would be automatically retracted; immediately following the completion of the satellite observations, the grating would be returned in front of the objective for a series of six 'postcalibration' exposures at 15 degree steps. A ten times enlargement of the image generated by this process for a sufficiently bright star would have the general appearance shown here: . Now, in theory, the mean of a pair of opposing diffraction images will coincide precisely with the center of the associated primary central image. It follows that, should the central image wander slightly in position (because of drift of the mount), the locus of the wander can be reconstructed from the means of diffraction images taken at different times. The principle of the diffraction grating approach is thus straightforward and simple.

From early experiments, a more satisfactory operational method of implementing the diffraction grating approach evolved. It was learned that it was not really necessary to employ the entire aperture of the MOTS in order to obtain satisfactory images; rather, a diffraction grating having a diameter of less than half that of the MOTS objective could provide altogether acceptable results. This finding meant that the grating could remain in place and undergo its series of step rotations throughout the period in which satellite observations were being made. This obviates the need for interpolation between pre and post-calibration series of exposures and provides instead a running calibration spanning the interval of actual interest.

The final version of the apparatus that evolved from exploratory exercises is shown at half scale in Figure 4. The grating itself is of 3.5-inch diameter and is supported over the center of the field of the objective by a three-legged spider. The grating and spider obscure about 20 percent of the area of the aperture. With the particular grating employed, 25 percent of the light incident on the grating goes into the central image. Accordingly, the effective loss of light due to the imposition of the grating is only about 15 percent. The grating is rotated by means of a belt-driven turntable connected to a motor. A remote manually operated, pushbutton switch causes a spring loaded solenoid plunger to retract from one of a series of slots spaced at 15 degree intervals near the rim of the turntable. This retraction immediately trips a microswitch which starts the drive motor. The turntable is driven 15 degrees, whereupon the spring loaded plunger slips into the next slot, tripping a microswitch which turns off the drive motor. This rotation of 15 degrees is accomplished in about one half second. Thus the operator merely activates the pushbutton switch for an instant whenever he wishes to effect an increment of rotation of the grating.

The grating itself is constructed from nylon monofilament of 0.015 inch diameter spaced at 0.030 inch intervals (thus the width of the grating openings is equal to the diameter of the monofilament, causing half the light to be absorbed by the grating). This generates about $N = 115$ openings over the 3.5-inch aperture of the grating. A Xerox print of the grating is provided by Figure 5. For the adopted design, the theory of diffraction gratings shows that one fourth of the light impinging on the grating will be directed to the central image; each of the first order images will receive about 10 percent of the original light (or, more precisely, a fraction of $1/\pi^2$ of the light). The angular distance between the central image and each of the first order images is $\theta = \lambda/d$ where λ is the wavelength of the light and d is the center to center spacing of the grating divisions. For blue light ($\lambda = 0.0005\text{mm}$) and a spacing of $d = 0.030$ inches (or 0.75mm), the value of θ becomes $1/1500$ radian. Because the MOTS focal length is nominally 1000mm , this corresponds to a spacing of about 0.670mm on the MOTS plate.

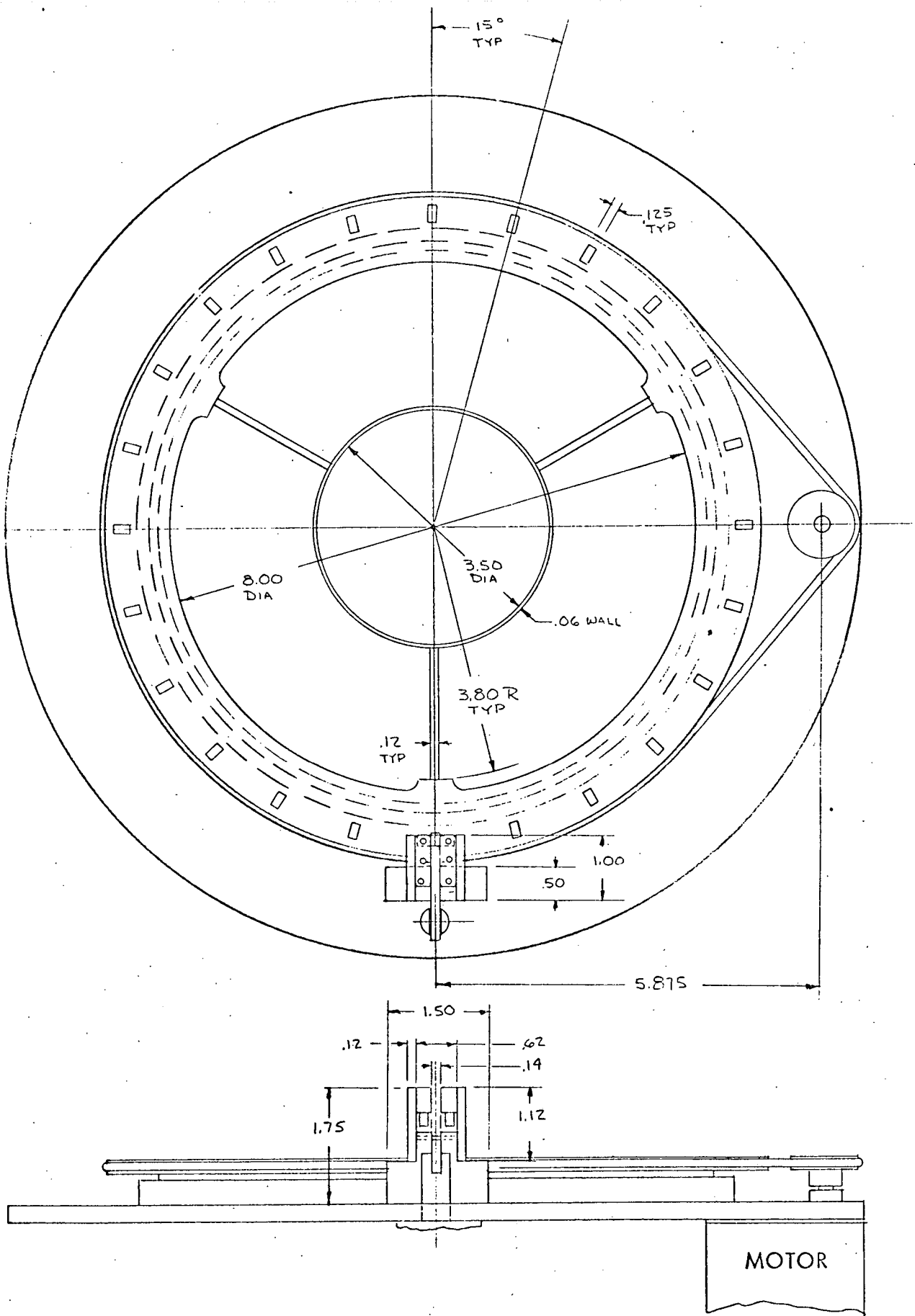


FIGURE 4. Half scale drawing of diffraction grating apparatus employed to monitor MOTS stability.

Event	Time	EST	Event	Time	Event	Time
Start Drive	T = 1 ^h 55 ^m		Start Drive	T + 10 ^m 00 ^s	Start Drive	T + 20 ^m 00 ^s
Open Shutter	T + 0 ^m 59 ^s		Open Shutter	T + 10 ^m 59 ^s	Open Shutter	T + 20 ^m 59 ^s
Shift Grating	T + 1 ^m 15 ^s		Shift Grating	T + 11 ^m 15 ^s	Shift Grating	T + 21 ^m 15 ^s
Shift Grating	T + 1 ^m 30 ^s		Shift Grating	T + 11 ^m 30 ^s	Shift Grating	T + 21 ^m 30 ^s
Shift Grating	T + 1 ^m 45 ^s		Shift Grating	T + 11 ^m 45 ^s	Shift Grating	T + 21 ^m 45 ^s
Shift Grating	T + 2 ^m 00 ^s		Shift Grating	T + 12 ^m 00 ^s	Shift Grating	T + 22 ^m 00 ^s
Shift Grating	T + 2 ^m 15 ^s		Shift Grating	T + 12 ^m 15 ^s	Shift Grating	T + 22 ^m 15 ^s
Shift Grating	T + 2 ^m 30 ^s		Shift Grating	T + 12 ^m 30 ^s	Shift Grating	T + 22 ^m 30 ^s
Shift Grating	T + 2 ^m 45 ^s		Shift Grating	T + 12 ^m 45 ^s	Shift Grating	T + 22 ^m 45 ^s
Shift Grating	T + 3 ^m 00 ^s		Shift Grating	T + 13 ^m 00 ^s	Shift Grating	T + 23 ^m 00 ^s
Shift Grating	T + 3 ^m 15 ^s		Shift Grating	T + 13 ^m 15 ^s	Shift Grating	T + 23 ^m 15 ^s
Shift Grating	T + 3 ^m 30 ^s		Shift Grating	T + 13 ^m 30 ^s	Shift Grating	T + 23 ^m 30 ^s
Shift Grating	T + 3 ^m 45 ^s		Shift Grating	T + 13 ^m 45 ^s	Shift Grating	T + 23 ^m 45 ^s
Close Shutter & Stop Drive	T + 4 ^m 00 ^s		Close Shutter & Stop Drive	T + 14 ^m 00 ^s	Close Shutter & Stop Drive	T + 24 ^m 00 ^s

Event	Time	EST	Event	Time	Event	Time
Start Drive	T + 5 ^m 00 ^s	x	Start Drive	T + 15 ^m 00 ^s	Start Drive	T + 25 ^m 00 ^s
Open Shutter	T + 5 ^m 59 ^s	x	Open Shutter	T + 15 ^m 59 ^s	Open Shutter	T + 25 ^m 59 ^s
Shift Grating	T + 6 ^m 15 ^s	x	Shift Grating	T + 16 ^m 15 ^s	Shift Grating	T + 26 ^m 15 ^s
Shift Grating	T + 6 ^m 30 ^s	x	Shift Grating	T + 16 ^m 30 ^s	Shift Grating	T + 26 ^m 30 ^s
Shift Grating	T + 6 ^m 45 ^s	x	Shift Grating	T + 16 ^m 45 ^s	Shift Grating	T + 26 ^m 45 ^s
Shift Grating	T + 7 ^m 00 ^s	x	Shift Grating	T + 17 ^m 00 ^s	Shift Grating	T + 27 ^m 00 ^s
Shift Grating	T + 7 ^m 15 ^s	x	Shift Grating	T + 17 ^m 15 ^s	Shift Grating	T + 27 ^m 15 ^s
Shift Grating	T + 7 ^m 30 ^s	x	Shift Grating	T + 17 ^m 30 ^s	Shift Grating	T + 27 ^m 30 ^s
Shift Grating	T + 7 ^m 45 ^s	x	Shift Grating	T + 17 ^m 45 ^s	Shift Grating	T + 27 ^m 45 ^s
Shift Grating	T + 8 ^m 00 ^s	x	Shift Grating	T + 18 ^m 00 ^s	Shift Grating	T + 28 ^m 00 ^s
Shift Grating	T + 8 ^m 15 ^s	x	Shift Grating	T + 18 ^m 15 ^s	Shift Grating	T + 28 ^m 15 ^s
Shift Grating	T + 8 ^m 30 ^s	x	Shift Grating	T + 18 ^m 30 ^s	Shift Grating	T + 28 ^m 30 ^s
Shift Grating	T + 8 ^m 45 ^s	x	Shift Grating	T + 18 ^m 45 ^s	Shift Grating	T + 28 ^m 45 ^s
Close Shutter & Stop Drive	T + 9 ^m 00 ^s	x	Close Shutter & Stop Drive	T + 19 ^m 00 ^s	Close Shutter & Stop Drive	T + 29 ^m 00 ^s

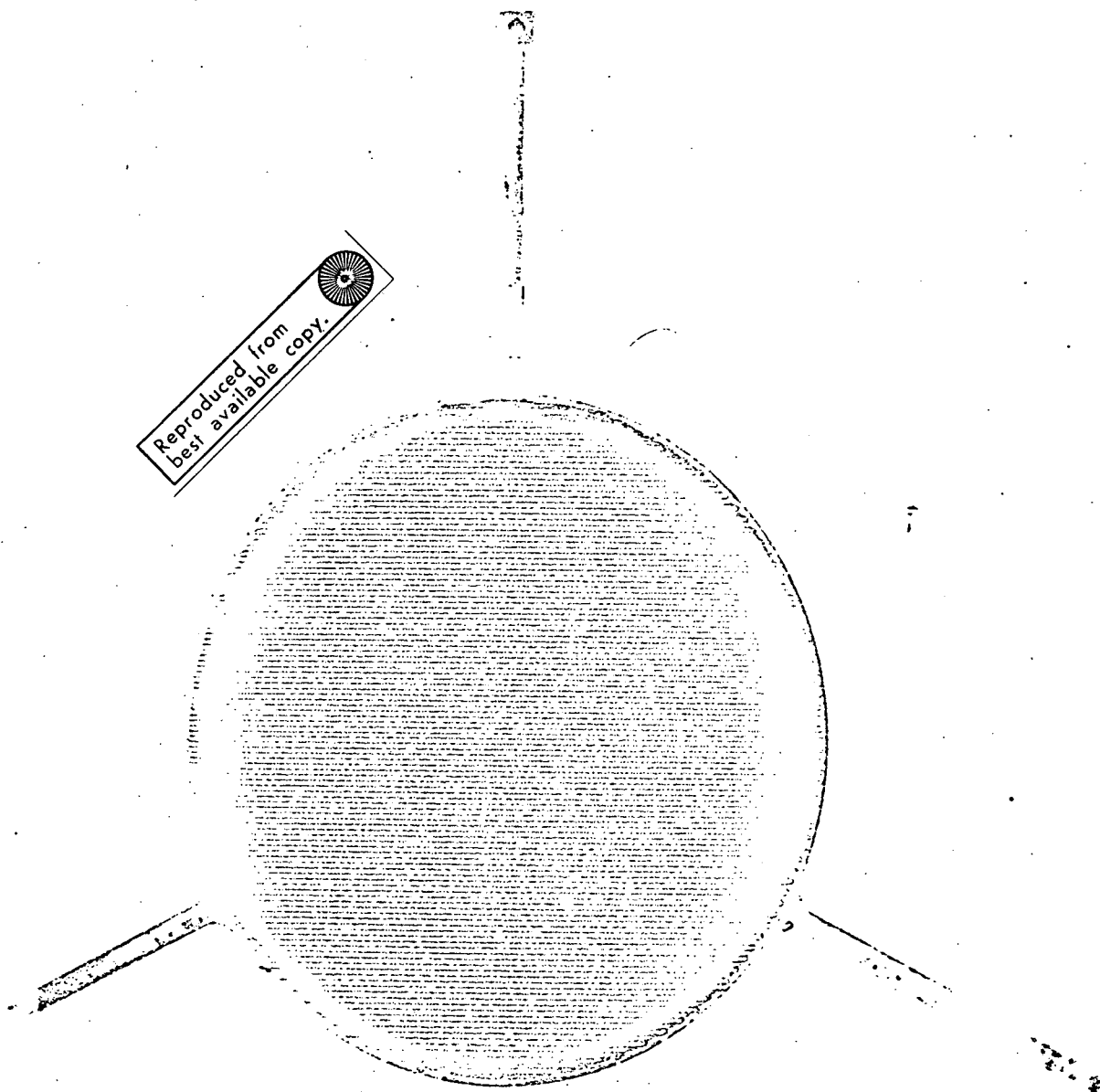


Figure 5. Direct Xerox print of diffraction grating employed in apparatus of Figure 4.

1.4 EXPERIMENTAL PROCEDURE

Short visits were made to the MOTS camera at the Ft. Myers STADAN station in April, September and November 1970 to gather data needed for the evolving design of the apparatus just described. Finally, on the night of December 2, a highly successful series of observations was made with the final version of the diffraction grating. In this section and the next we shall review the results of this test.

Because of other tests being conducted at the same time, the MOTS cameras had been refocussed for optimum imagery with blue light. For this reason, an orthochromatic emulsion (103 Ao) was employed for the diffraction grating experiment. For the data plate that was actually reduced, the MOTS was pointed toward the star β Persius, the drive was started at 01^h 55^m EST (December 3), and the initial exposure was started one minute later. Thereafter, exposures were made in accordance with the pre-established log reproduced on the next page. The total exposure for a complete set of 12 successive grating positions amounted to 180 seconds (or to two complete periods of the drive error), the grating being shifted at 15 second intervals throughout the exposure. Thus each central image of a star received the full 180 second exposure (not only from the grating but also from the unobscured aperture of the objective, as well), while each pair of diffraction images received a 15 second exposure (from the grating only). To simulate the taking of multiple plates, this process was repeated a total of six times, the drive being turned off for one minute between each sequence. Although all six sequences were recorded on a common plate, the practical end result was equivalent to what would have been obtained from the exposure of a single sequence on each of six separate plates. For this reason, we shall hereafter refer to the results from exposure sequences, 1 through 6 as being from plates 1 through 6.

The star β Persius toward which the camera was initially aimed, generated diffraction images that were too large for precise measurement. However, usable diffraction images were generated by eight other stars ranging in stellar magnitude from 2.5 to 4.0. Inasmuch as a set of diffraction images from a single star is sufficient for monitoring

stability, there was ample data from which to make a selection for reduction. In order to obtain a measure of redundancy, we selected two stars from each 'plate' for measurement and reduction. A 40X enlargement of the diffraction images generated by one of the two selected stars is provided in Figure 6. The total exposure of the central image is almost 600 times greater than the exposure of a given diffraction image. This explains the relatively large diameter of the central image. Although somewhat ragged because of their small size (about 20 to 30 microns on the plate), the diffraction images are, nonetheless, of a satisfactory quality for precise measurement.

1.5 EXPERIMENTAL RESULTS

On each of the 6 'plates', the 24 diffraction images (12 pairs) for each of the two selected stars were measured by an experienced operator on DBA's Mann comparator. The first phase of the data reduction consisted simply of determining the mean of the coordinates of each of the 12 pairs of diffraction images and then of subtracting from these the grand mean obtained by averaging the set of 12 means. If there were no drift of the camera and no measuring error, the departures from the grand mean would be precisely zero for each averaged pair of diffraction images. Significant, systematic departures were found to exist, and, within acceptable measuring tolerances, were found to be the same for the two stars measured on each plate. Accordingly, the departures for the two stars measured on each plate were themselves averaged for corresponding pairs of diffraction images.

The first stage in the analysis of the results consisted merely of plotting as functions of time the x (right ascension) and y (declination) departures obtained by the process just described. In addition, a program was written to perform a least squares regression based on functions of the form:

$$\delta x_j = a_0 + a_1 \tau_j + a_2 \sin \frac{2\pi}{90} \tau_j + a_3 \cos \frac{2\pi}{90} \tau_j$$

$$\delta y_j = b_0 + b_1 \tau_j + b_2 \sin \frac{2\pi}{90} \tau_j + b_3 \cos \frac{2\pi}{90} \tau_j$$

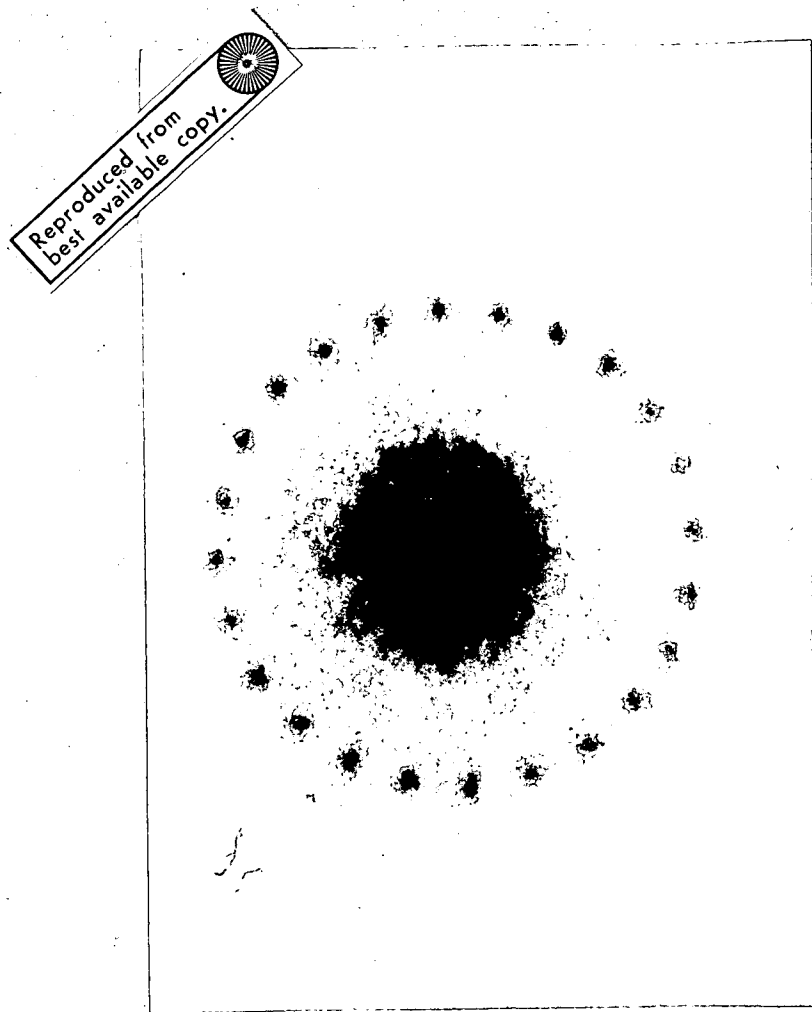


Figure 6. Enlargement (40X) of star exposed through diffraction grating apparatus mounted on MOTS (15 second exposure for each set of diffraction images and 180 second cumulative exposure for central image).

in which,

$\delta x_j, \delta y_j$ = observed departures in x and y from grand mean of averaged coordinates for j th pair of diffraction images,

τ_j = relative time of midpoint of exposure of j th pair of diffraction images

= 15 (j - 1) second (i.e., $\tau_1 = 0, \tau_2 = 15, \dots, \tau_{12} = 165$ seconds),

a_0, b_0 = zero set coefficients,

a_1, b_1 = linear drift coefficients,

a_2, a_3
 b_2, b_3 = periodic drift coefficients (90 second period assumed).

Values of the observed $\delta x_j, \delta y_j$ plotted against τ_j are presented in Figures 7 through 12. Also plotted in the same figures are corresponding values of $\delta x_j, \delta y_j$ as computed from the fitted functions.

In reviewing Figures 7 through 12, we find that the departures in right ascension and declination are not randomly distributed about zero, but rather, for the most part, display fairly well defined trends. However, with a few notable exceptions, the fit of the regression functions can be said to be only fair. This is especially clear from the results presented in Table 1 on the following page. These show that goodness of fit indicated by S_x and S_y is generally only modestly better than the dispersion about zero means as indicated by s_x and s_y . Indeed, in a few instances, values of S_x and S_y are slightly larger than their counterparts s_x and s_y , a result attributable to the fewer degrees of freedom associated with the residuals from the fitted functions (i.e., 8 degrees of freedom are associated with S_x, S_y , whereas 11 are associated with s_x, s_y).

It will be noted that the values of s_x and S_x for plate 6 are exceptionally large (9.1 and 7.8 μm , respectively). Referring to the plotted results in Figure 12, we see the presence of two pronounced jumps in the trends as indicated by the heavy arrows. To make sure that these jumps were actually real and not the result of a measuring or recording

Table 1. RMS values of x and y drifts before and after regression.

Plate	RMS Values Before Regression (μm)		RMS Values After Regression (μm)	
	s_x	s_y	S_x	S_y
1	3.4	2.5	2.4	1.8
2	3.5	2.3	3.4	1.8
3	4.0	1.7	3.7	1.9
4	5.3	2.3	4.3	1.1
5	3.2	2.1	3.3	1.9
6	9.1	2.3	7.8	2.2
$s_x = \left[\frac{\sum \delta x_j^2}{11} \right]^{\frac{1}{2}} \quad S_x = \left[\frac{\sum (\delta x_j - \delta x'_j)^2}{8} \right]^{\frac{1}{2}}$ $s_y = \left[\frac{\sum \delta y_j^2}{11} \right]^{\frac{1}{2}} \quad S_y = \left[\frac{\sum (\delta y_j - \delta y'_j)^2}{8} \right]^{\frac{1}{2}}$ <p>$\delta x_j, \delta y_j$ = observed values</p> <p>$\delta x'_j, \delta y'_j$ = values computed from regression</p>				

PLATE NO. 1

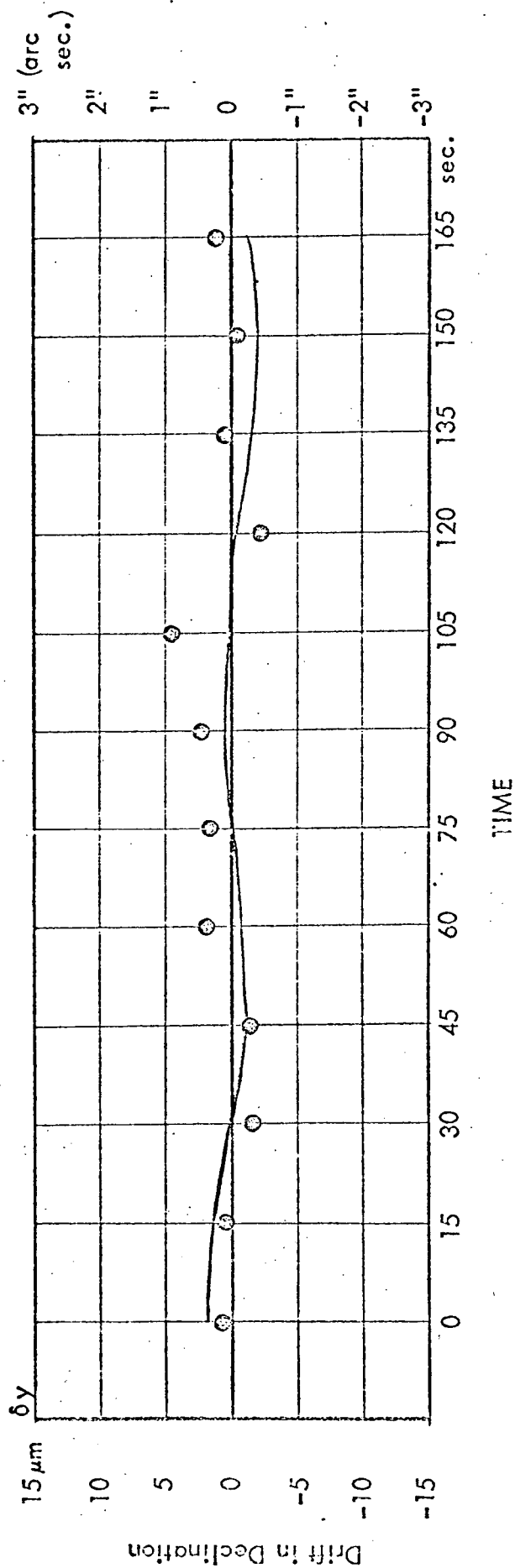
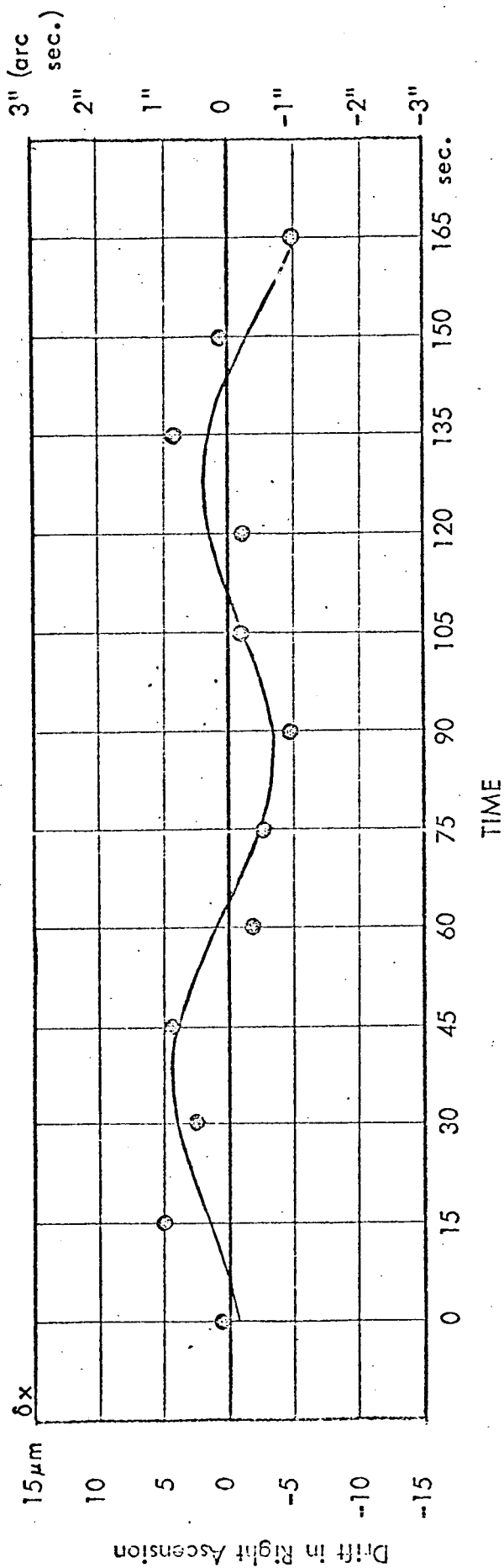


Figure 7 . MOTS drift as indicated by rotating diffraction grating, plate no. 1 .

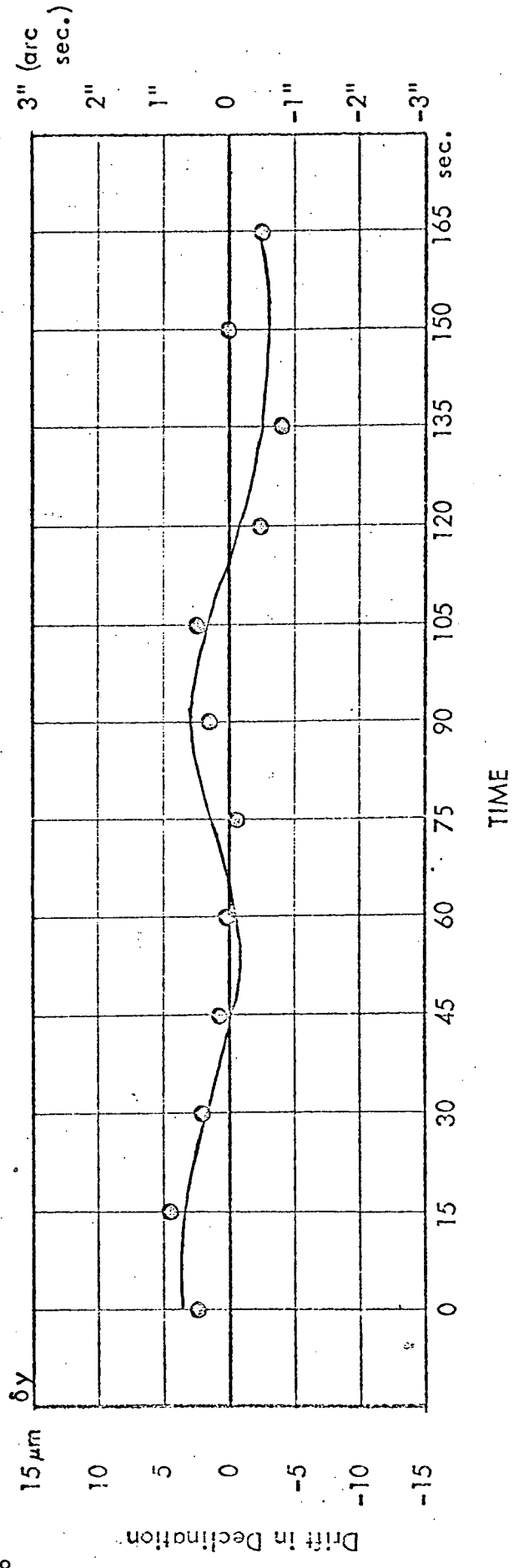
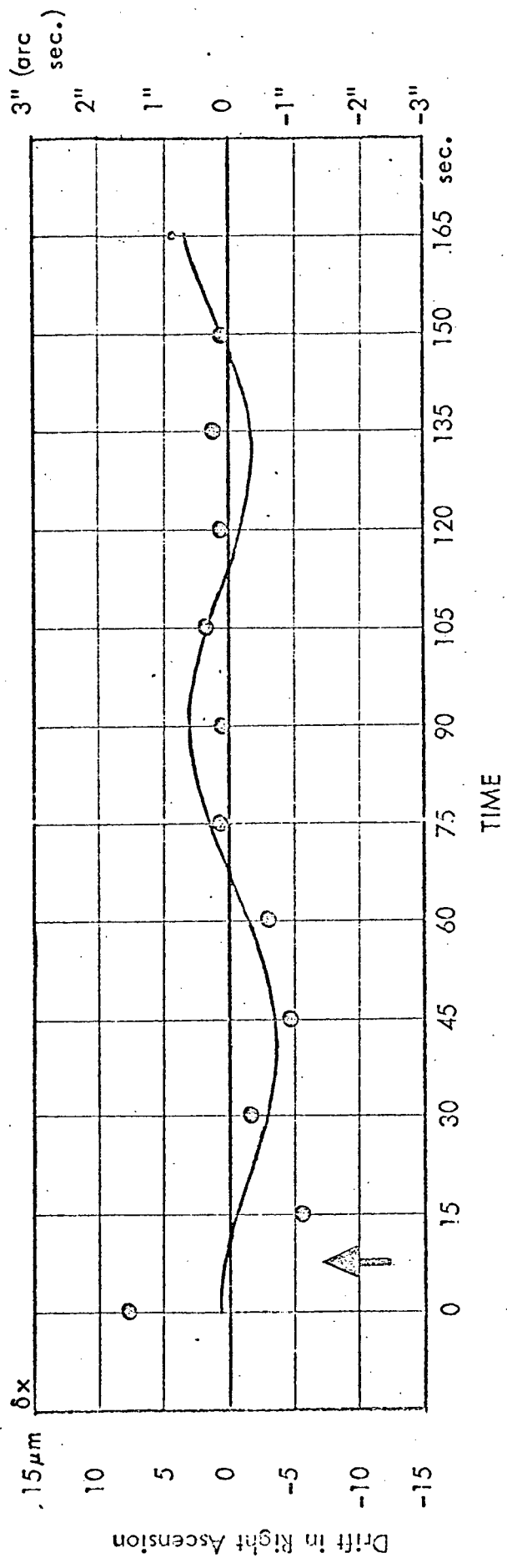


Figure 8 . MOTS drift as indicated by rotating diffraction grating, plate no. 2 .

PLATE NO. 3

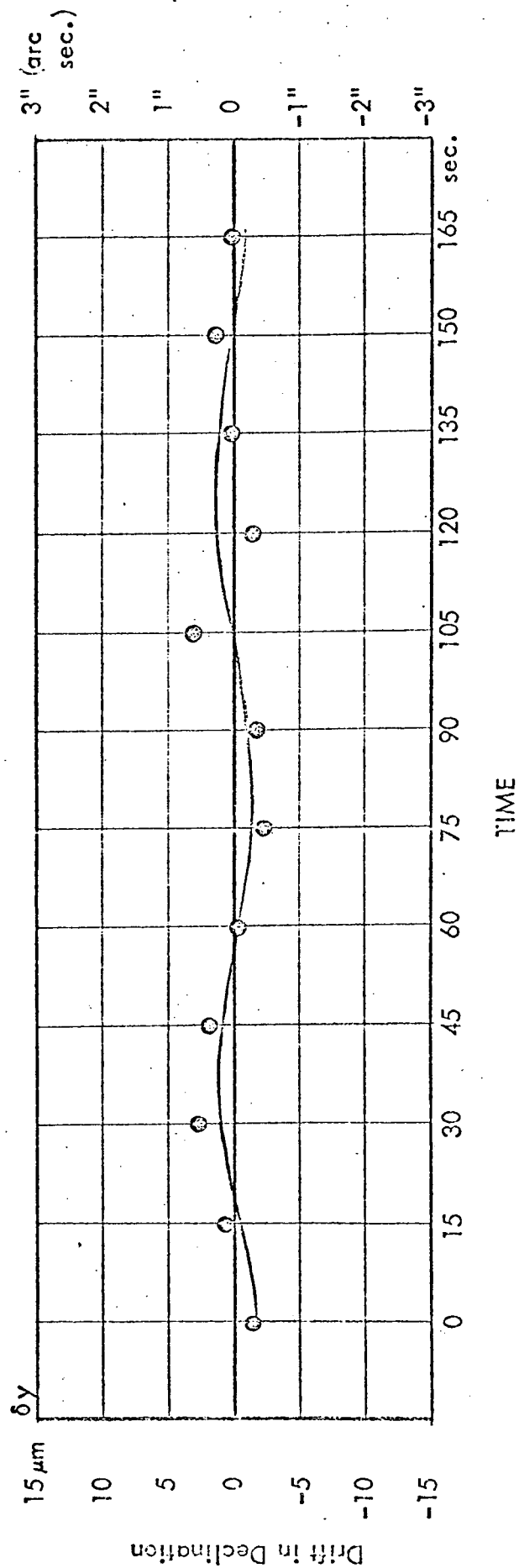
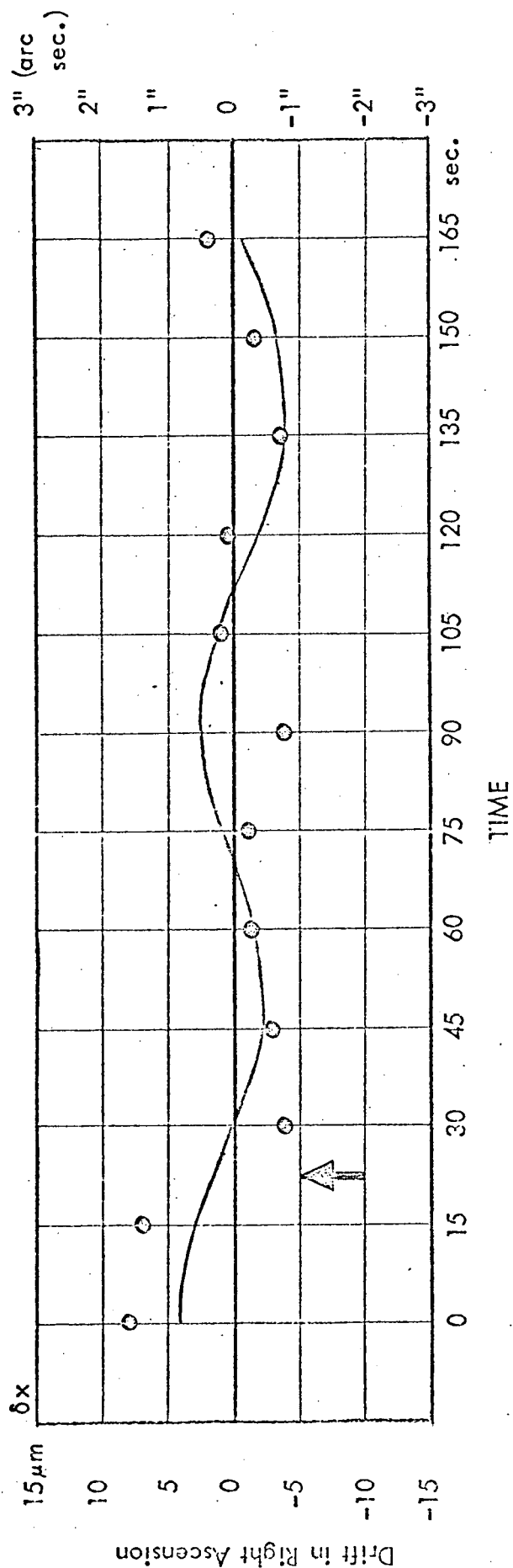


Figure 9 . MOTS drift as indicated by rotating diffraction grating, plate no. 3 .

PLATE NO. 4

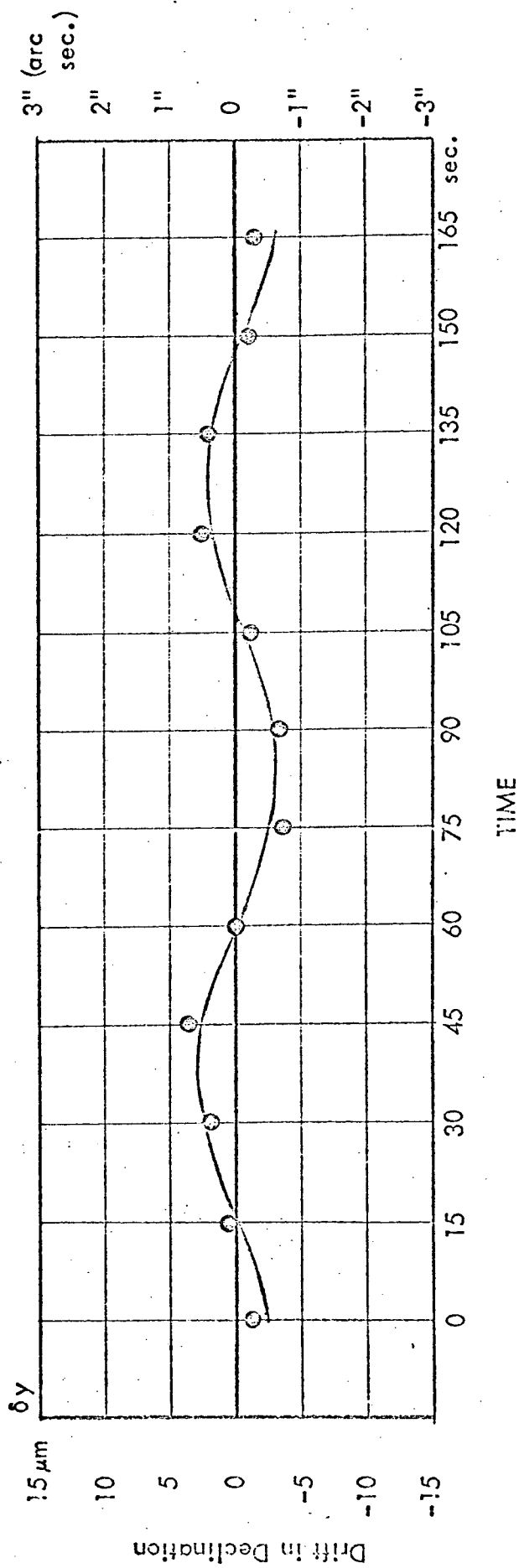
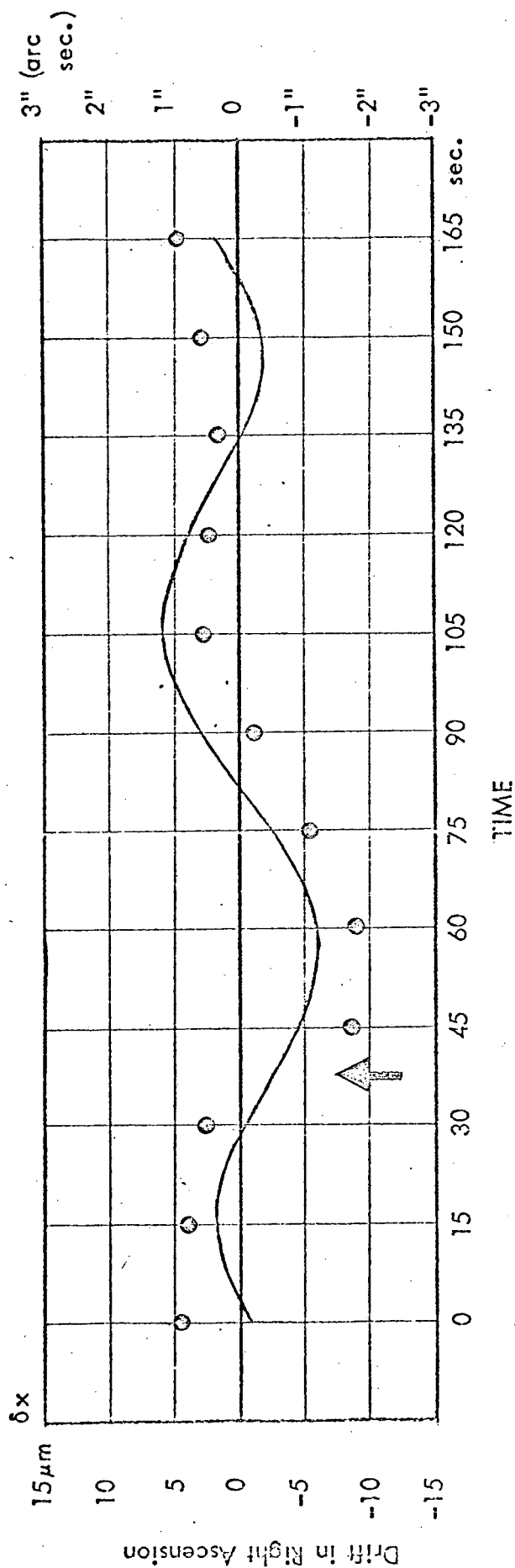


Figure 10. MOTS drift as indicated by rotating diffraction grating, plate no. 4 .

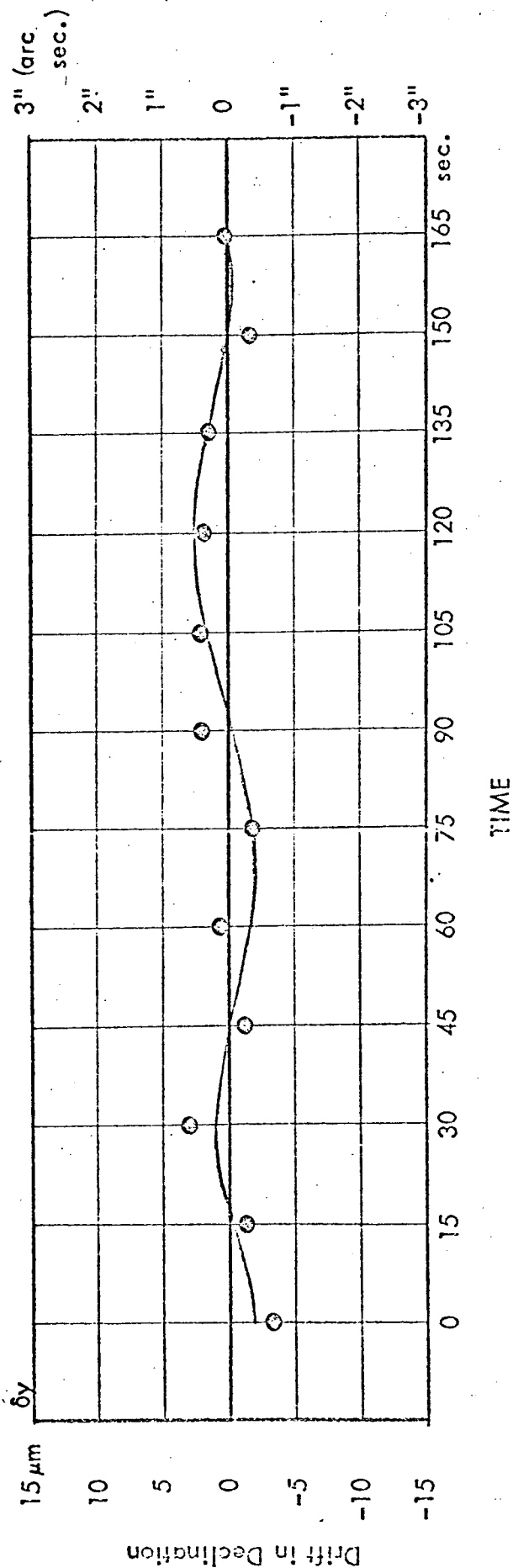
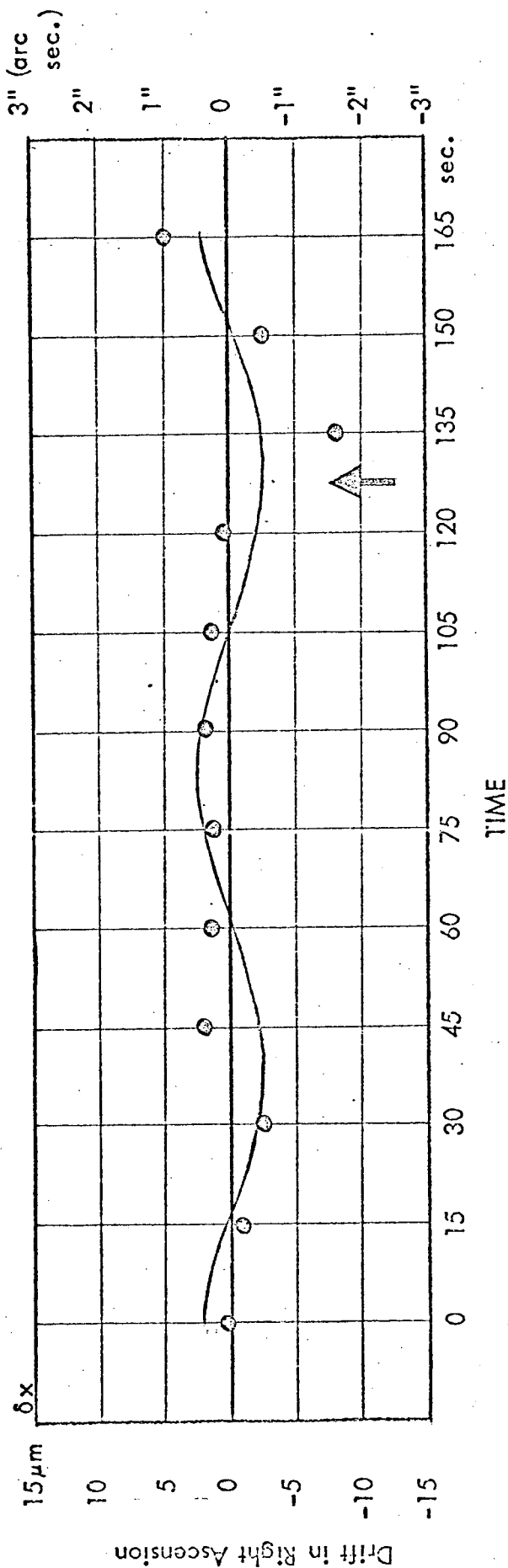


Figure 11 . MOTS drift as indicated by rotating diffraction grating, plate no. 5 .

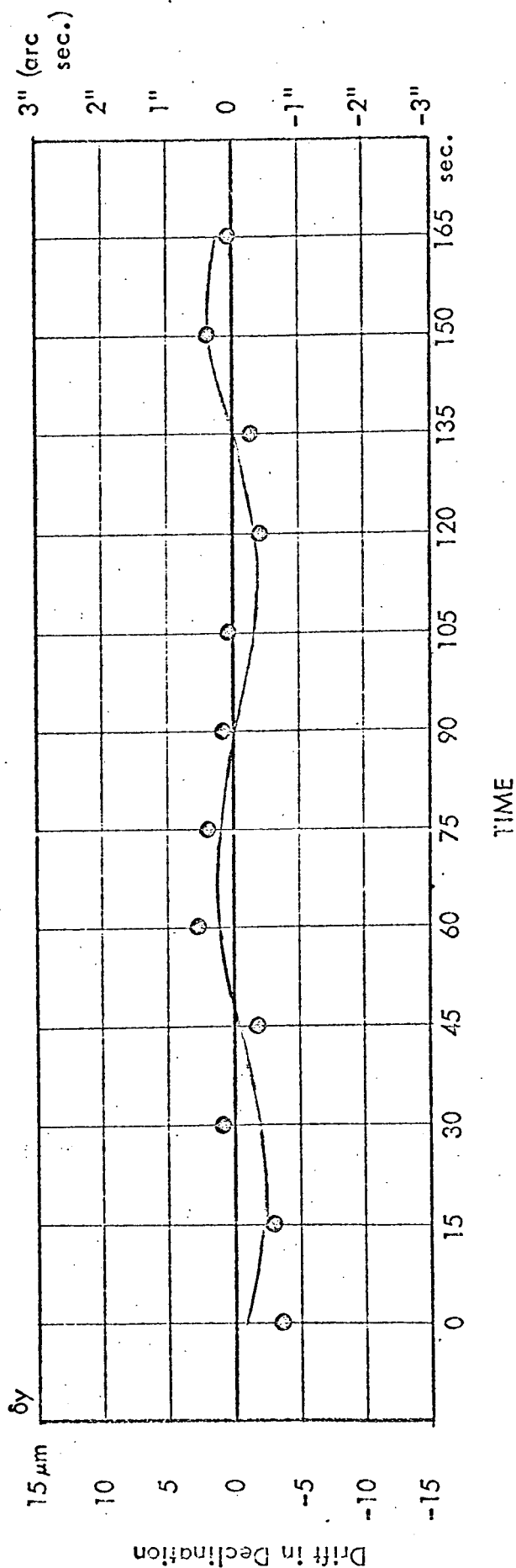
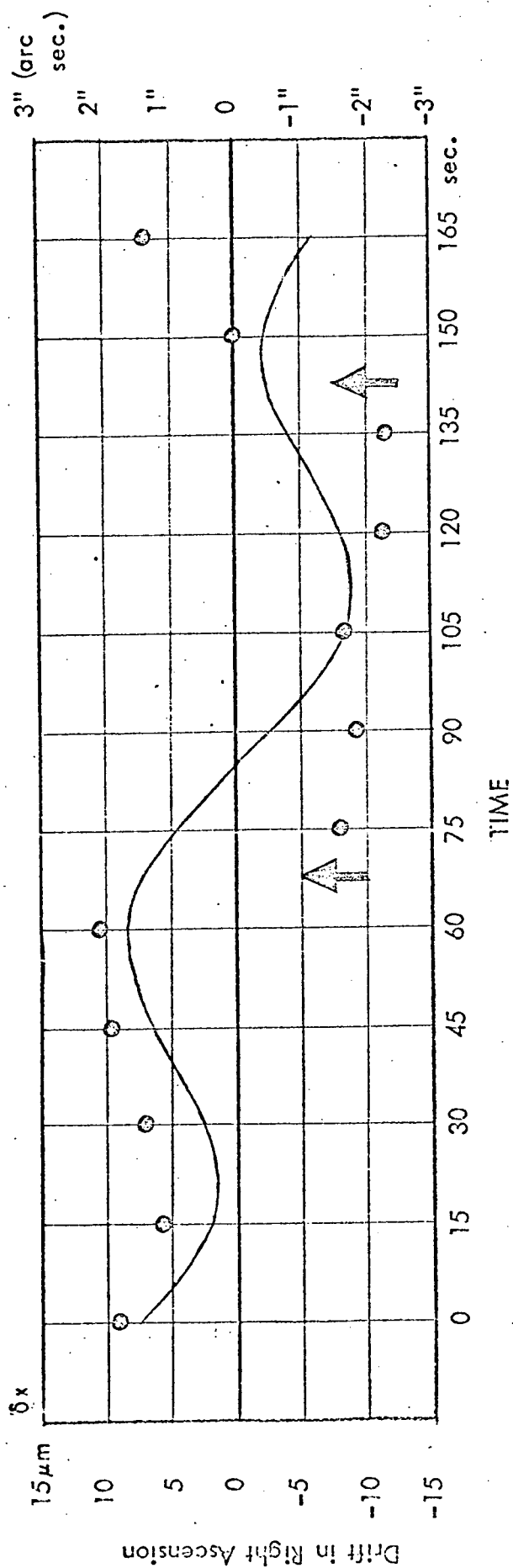


Figure 12. MOTS drift as indicated by rotating diffraction grating, plate no. 6 .

PLATE NO. 6

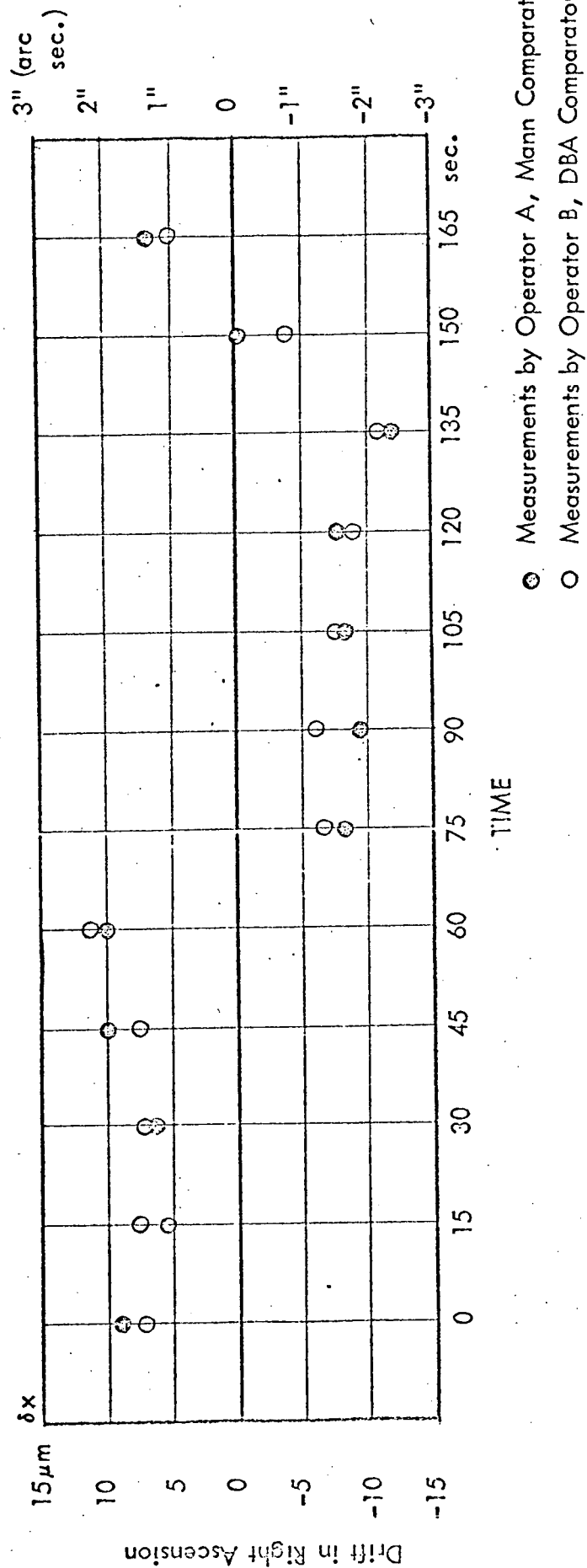


Figure 13. Comparison of original measurements of drift in right ascension for plate 6 with remeasurements made on different comparator by different operator.

blunder, we had plate 6 remeasured by another operator on another comparator (namely, the DBA multilaterative comparator). Comparative results presented in Figure 13 show good agreement between the two sets of measurements and verify that the jumps are indeed real. Reviewing the plots for the other plates, we find indications of similar jumps occurring on Plates 2, 3, 4 and 5 at the points indicated by the arrows in Figures 8, 9, 10 and 11. These suggest the presence of stiction in the drive train. Stiction being the occasional slight binding of the gears followed by sudden release. Whether or not this is the correct explanation for the abrupt changes remains to be determined. For convenience, we shall nonetheless refer to the abrupt changes as 'stiction jumps'.

It seemed that the generally mediocre fits obtained from the regressions performed on δx could well be attributable to the compromising effect of stiction jumps. To test this hypothesis we revised the regression model so that the single zero set term a_0 was replaced by the expression:

$$\xi_1 a_0 + \xi_2 a_0' + \xi_3 a_0''$$

in which,

$$\begin{aligned}\xi_1 &= 1 \text{ for } \tau_1 < T_1 \\ &= 0 \text{ for } \tau_1 > T_1 \\ \xi_2 &= 1 \text{ for } T_1 < \tau_1 < T_2 \\ &= 0 \text{ otherwise} \\ \xi_3 &= 1 \text{ for } \tau_1 > T_2 \\ &= 0 \text{ otherwise.}\end{aligned}$$

This artifice makes it possible to reinitialize the zero set term up to two times per plate. When no reinitializations are desired, we need merely set T_1 and T_2 to values greater than the maximum value of τ_1 (say to 180 seconds). The values of T_1 and T_2 adopted in the revised regressions for δx are as indicated in the following table.

Plate	Number of Stiction Jumps	T_1	T_2	Degrees of Freedom For Regression
1	0	180.	180	8
2	1	7.5	180	7
3	1	22.5	180	7
4	1	37.5	180	7
5	1	127.5	180	7
6	2	67.5	142.5	6

The results of the revised regressions are plotted in Figures 14 through 19. The results for Plate 1 are unchanged, which is as it should be, since no stiction jumps were exercised. Results for the remaining plates represent substantial improvements over those from the original regressions. The fitted functions now very closely follow the observed values. This is verified by Table 2 in which Table 1 is extended to reflect the results of the revised regressions. The grand rms value for the fit in δx for all six plates is $2.1 \mu m$, a value only insignificantly greater than the grand rms of $1.8 \mu m$ for y .

The amplitude of the periodic error from the revised regressions averages about 0.6 second of arc in right ascension and about 0.4 second of arc in declination. This is appreciably lower than the values considered typical (i.e. 2 to 3 arc seconds in right ascension) in Reference 2. However, specific results from the MOTS at Fort Myers were not reported in Reference 2.

1.6 GENERAL CONSIDERATIONS

When stiction jumps are duly taken into account whenever they occur, excellent fits are obtained from the simple regression model that was adopted. This demonstrates the effectiveness of the rotating diffraction grating as a means for monitoring the stability of the MOTS camera throughout routine operations.

Because of the exploratory nature of our investigation, we took the liberty of ignoring a few fine points that should be implemented when the diffraction data are actually to be used to generate corrections applicable to satellite observations. Because

Table 2. Extension of Table 1 to include results of revised regressions.

Plate	RMS Values Before Regression (μm)		RMS Values After Original Regression (μm)		RMS Values After Revised Regression (μm)	
	s_x	s_y	S_x	S_y	S'_x	S'_y
1	3.4	2.5	2.4	1.8	2.4	1.8
2	3.5	2.3	3.4	1.8	1.5	1.8
3	4.0	1.7	3.7	1.9	2.0	1.9
4	5.3	2.3	4.3	1.1	1.4	1.1
5	3.2	2.1	3.3	1.9	2.8	1.9
6	9.1	2.3	7.8	2.2	2.0	2.2

$$s_x = \left[\frac{\sum \delta x_j^2}{11} \right]^{\frac{1}{2}}$$

$$S_x = \left[\frac{\sum (\delta x_j - \delta x_j')^2}{8} \right]^{\frac{1}{2}}$$

$$S'_x = \left[\frac{\sum (\delta x_j - \delta x_j'')^2}{f} \right]^{\frac{1}{2}}$$

$$s_y = \left[\frac{\sum \delta y_j^2}{11} \right]^{\frac{1}{2}}$$

$$S_y = \left[\frac{\sum (\delta y_j - \delta y_j')^2}{8} \right]^{\frac{1}{2}}$$

$$S'_y = \text{same as } S_y$$

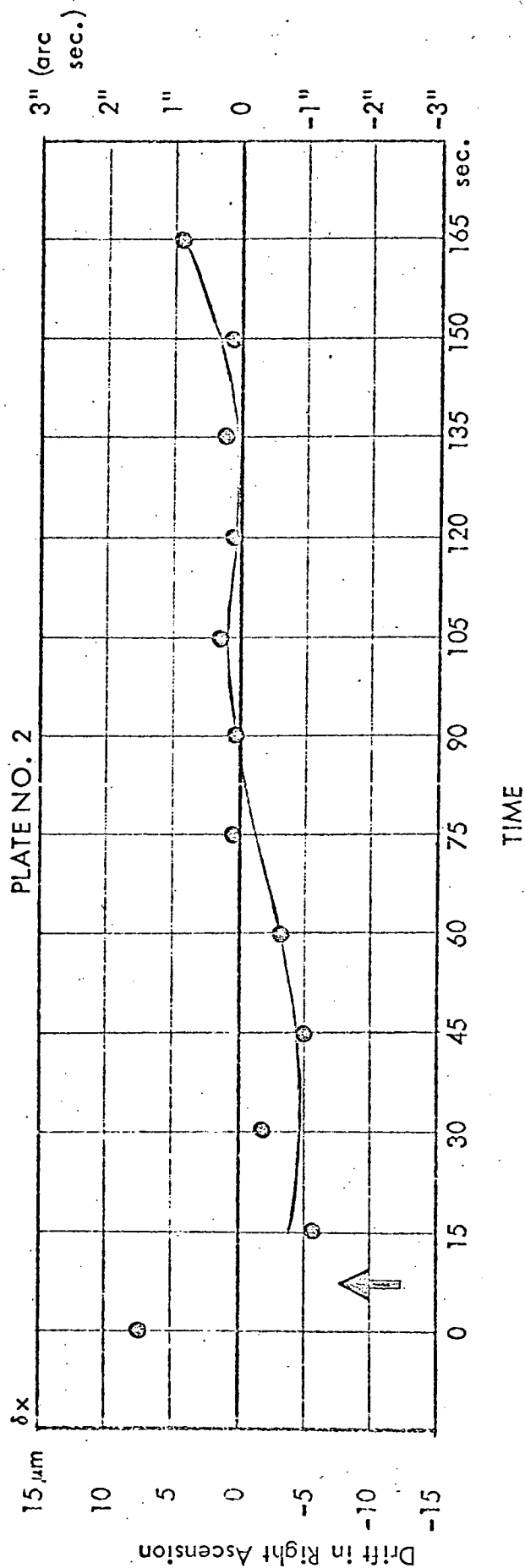
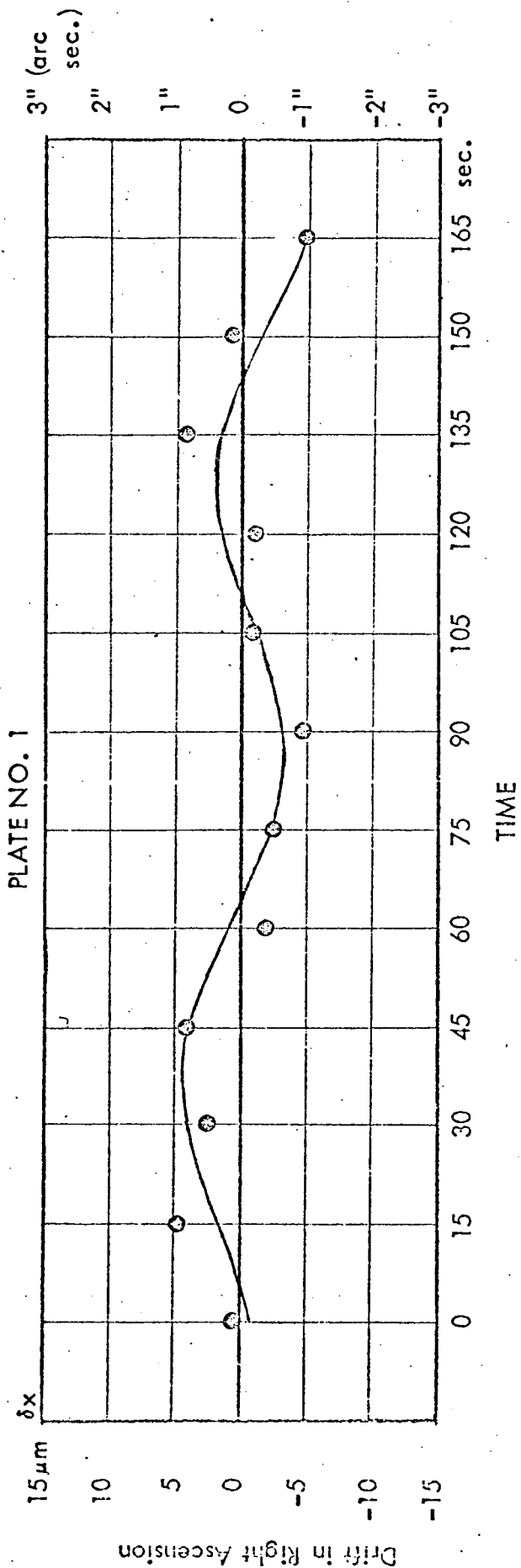
$\delta x_j, \delta y_j$ = observed values

$\delta x_j', \delta y_j'$ = values computed from original regression

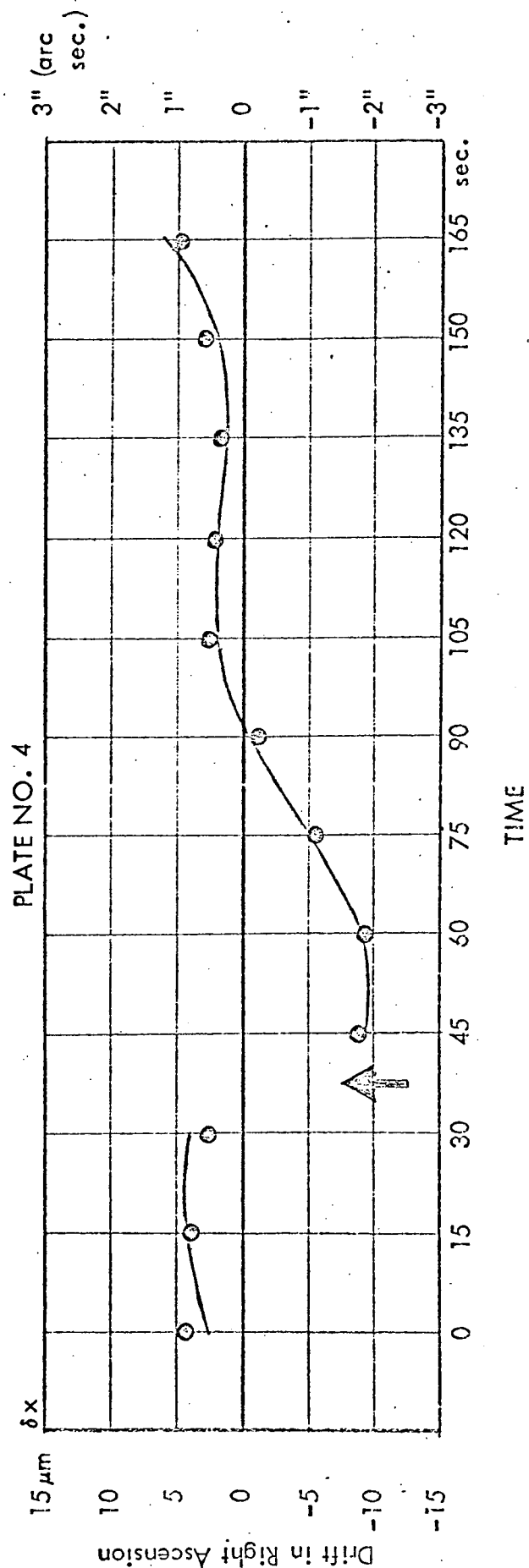
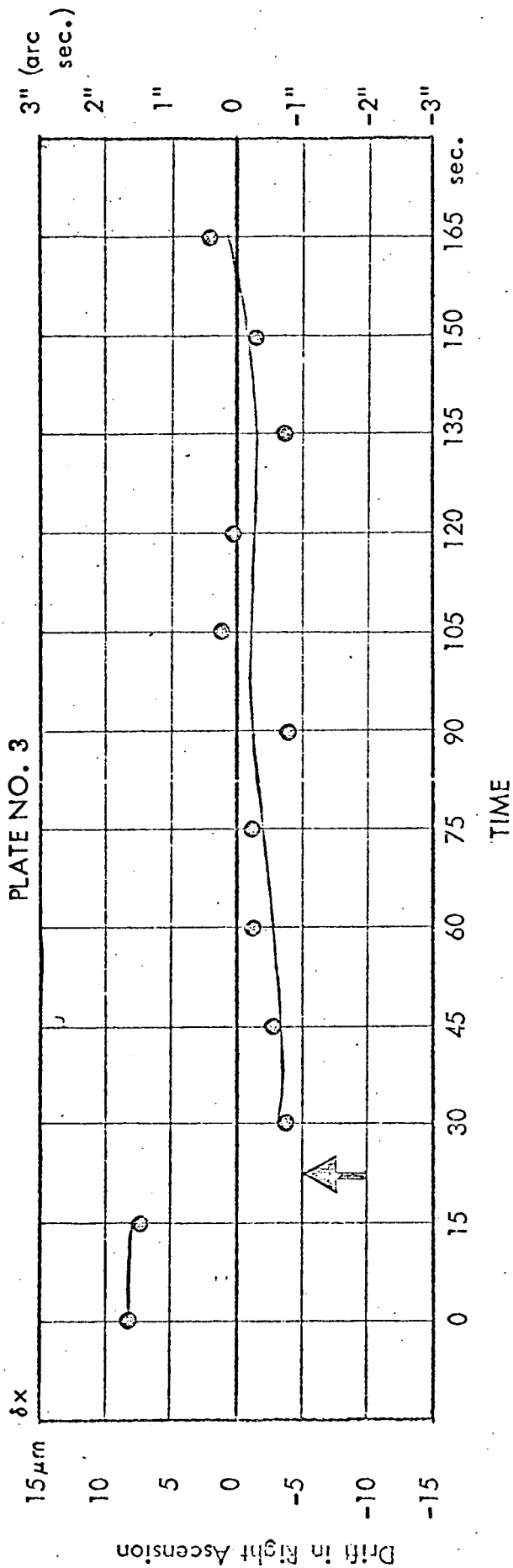
$\delta x_j'', \delta y_j''$ = values computed from revised regression

f = degrees of freedom

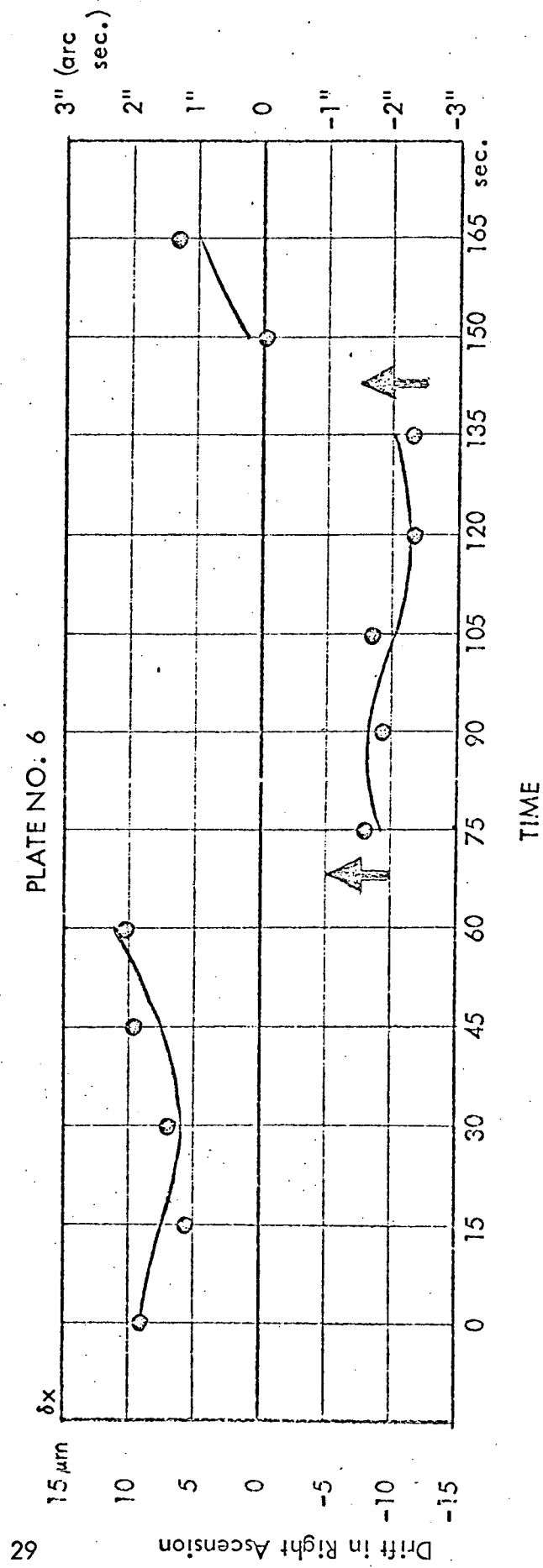
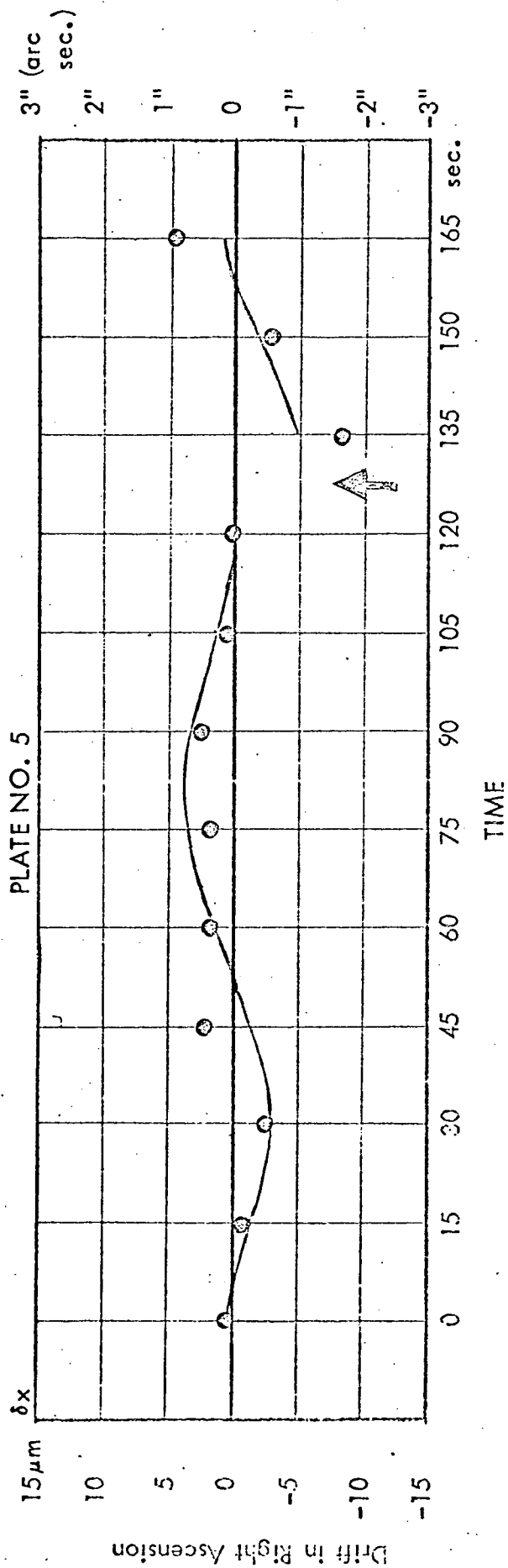
= 8, 7 or 6 depending on number of stiction jumps



Figures 14 and 15. Plots showing fit from revised regressions in right ascension, plates 1 and 2.



Figures 18 and 19. Plots showing fit from revised regressions in declination, plates 3 and 4.



Figures 16 and 17. Plots showing fit from revised regressions in right ascension, plates 5 and 6.

the length of each exposure through the grating may be a significant fraction of the 90 second period of the drive, the integrated effect of the drift over exposure increments should be recognized as being what is actually observed. Accordingly, if 2Δ denotes the length of each exposure through the grating, the expression

$$a_2 \sin \frac{2\pi}{90} \tau_1 + a_3 \cos \frac{2\pi}{90} \tau_1$$

in the formula for δx_1 , for example, should more properly be replaced by the expression

$$\frac{1}{2\Delta} \int_{\tau_1 - \Delta}^{\tau_1 + \Delta} [a_2 \sin \frac{2\pi}{90} t + a_3 \cos \frac{2\pi}{90} t] dt.$$

However, this reduces to the form

$$a'_2 \sin \frac{2\pi}{90} \tau_1 + a'_3 \cos \frac{2\pi}{90} \tau_1$$

in which

$$a'_2 = K a_2$$

$$a'_3 = K a_3$$

where

$$K = \left(\sin \frac{2\pi}{90} \Delta \right) / \left(\frac{2\pi}{90} \Delta \right).$$

Thus, while a'_2 and a'_3 are the values actually obtained from the least squares regression, the values to be used in the correction formulas should be a_2, a_3 which will, of course, be slightly larger. For $2\Delta = 15$ seconds (the value used in our experimental investigation), the value of K is $(\sin \pi/6)/(\pi/6) = 0.956$, which means that the amplitudes obtained from the regressions should be increased by a factor of $1/0.956 = 1.044$.

The second fine point to be considered in operational applications of the diffraction grating concerns effects induced by changes in atmospheric refraction resulting from the gradual changes in zenith distance occurring throughout the operation. Even if the MOTS were perfectly stable in the right ascension-declination frame, the gradual change in refraction with change in zenith distance would be manifested as a secular drift if appropriate corrections were not applied. In Reference 3 we showed that the correction for this effect is given by:

$$d(\Delta\zeta) = 4.5 \times 10^{-3} t_i \sin A_i \cos \Phi \sec^2 \zeta_i$$

(arc sec)

in which, for the present application,

$d(\Delta\zeta)$ = angular correction to be applied zenith distance of mean of pair of diffraction images

t_i = time of exposure of i th set of diffraction images relative to mean time of total exposure

A_i = azimuth of star at t_i

ζ_i = zenith distance of star at t_i

Φ = latitude of station.

By means of standard astronomical formulas, this correction for zenith distance can be propagated into right ascension and declination and thence into x, y plate coordinates. It is the corrected x, y coordinates that properly should be employed in the diffraction grating regressions.

1.7 CONCLUSIONS AND RECOMMENDATIONS

The diffraction grating apparatus evolved from this study has proven to provide a simple, inexpensive, effective, and operationally unobtrusive means for monitoring the stability of the MOTS camera to a precision of a few tenths of a second of arc.

We recommend that NASA employ the breadboard apparatus developed by DBA in further tests on other MOTS cameras, particularly those that are known to be affected by larger drift errors than the MOTS at Ft. Myers. Should these tests confirm the promise of the approach, NASA should undertake the procurement of operationally optimized units to be used routinely in future operations at all MOTS stations. Such units should preferably be controlled by an automatic programmer with a suitable range of selectable exposure rates.

While the diffraction grating method provides a way of correcting for drift in future MOTS operations, the question naturally arises as to whether anything can be done about the many hundreds of plates gathered on past operations, particularly on GEOS I and GEOS II. We believe that quite possibly something effective can be done. Because a formal standardized procedure was followed in the exposure of GEOS plates, a fairly high level of repeatability of drive error may well exist. In any event, whether or not this is the case can be determined experimentally by employing the grating in repeated trials simulating GEOS operations. If acceptably repetitive results are obtained for a given camera, a pooled result can be used to derive corrections to be applied to directions obtained from previous plates taken by the camera. The validity of such corrections can be tested by determining whether or not improved residuals are generally obtained from short arc reductions based on revised directions.

1.8 REFERENCES

- [1] Brown, D., "Advanced Methods for the Calibration of Metric Cameras," final report, Contract No.: DA-44-009-AMC-1457(X), U.S. Army Engineering Topographic Laboratories, Fort Belvoir, Virginia, 9 December 1968.
- [2] Harris, D., Cartwright, M., Oosterhaut, J., "Analysis of the MOTS Camera Drive," GSFC Report X-514-69-482, November 1969.
- [3] Brown, D., Hartwell, J., Stephenson, J., "Geodetic Data Analysis for GEOS A, An Experimental Design," final report prepared for NASA Goddard under Contract No. NAS5-9860, November 1965.

SECTION 2

MINITRACK DATA REDUCTION

2.1 INTRODUCTION

This section covers work done by DBA Systems, Inc., over a 2-year period. Work for the contract was initially being performed by the DBA Florida Office. In order to provide better liaison between NASA and DBA, it was decided to transfer the project to the DBA Washington Office. This was done nine months after the start of the contract. The section dealing with the Minitrack geometrical error model, contributed by James B. Willmann, was written prior to the transfer of the project to Washington. Several thousand NAP (Network Analysis Program-II) control cards for processing optical orbits had also been prepared, but this work became largely redundant after the development of a new optical preprocessing program.

After the project was transferred to Washington, work was concentrated on calibrating Minitrack using short optically determined reference arcs. This was done in order to demonstrate the feasibility of using the NAP program for the purpose of calibrating Minitrack. At this time too, the magnitude of the Doppler effect was being investigated, and the relevant equations were implemented into the NAP program.

Concurrently, the new optical preprocessing program, already mentioned, was developed. The reason for writing a new optical preprocessing program was that the old program could not process data for SAO stations and required an enormous amount of data preparation. The new program in addition would punch out most of the NAP control cards.

Twelve months after the start of the contract, work began on the calibration of Minitrack using Minitrack data only. Initially, little progress was made. At this time the Minitrack extract and sort programs were developed. The Minitrack preprocessor was modified to punch out most of the NAP control cards. After three months, it was found that the NAP program had been requested to compute and apply the effect of the earth's precession and nutation. Unfortunately, an error was known

to exist in these computations. After the NAP control cards were changed, so as not to request these computations, progress was again made. (To the order of the accuracy of the Minitrack system, it would not appear to be necessary to consider precession and nutation. However, because of the surprisingly good agreement between orbits determined from Minitrack and optical data, this point of view may have to be modified).

Definite but slow progress was now being made. A post NAP program -- later extensively modified -- was written to summarize the results of the NAP program. This also involved modifications to NAP subroutines RESID and FINALP.

About 17 months after the start of the contract, the contract Technical Monitor (W. M. Rice) proposed an analysis of the NAP program by Boole & Babbage, Inc., to determine the feasibility (within the time scale of the contract) of increasing the computational speed of NAP and hence the overall rate of progress. The analysis showed that the majority of the computing time was being spent in a few relatively short subroutines. A new algorithm was then developed for the computation of spherical harmonics and this was implemented into NAP. The modifications to the NAP program doubled its overall computational speed.

Advantage was now taken of the faster NAP program, the length of arc considered was increased from 2.5 to 5 days; however, this led to further problems. A meeting was called by E. P. Damon of the Computer Systems Branch to call attention to the amount of computer disk space being required by the NAP program. (As the length of arc had been doubled, so had the amount of data being stored on disk memory). We had, however, become aware of the problem before the above mentioned meeting because of the frequently aborted runs due to non-availability of enough disk space. To overcome this problem, the special subroutines PRTIAL and RESID were written and the NAP disk space requirements were substantially reduced. The post-NAP program was modified to be consistent with the latest NAP program.

With the increasing amount of data being processed on each run, the number of NAP control cards became very large and it was decided to write them on tape. To handle modifications to individual NAP "cards" the pre-NAP card updater program was written.

In checking out the new special subroutine PRTIAL a discrepancy was discerned in the printed out time. This was traced back to the Minitrack preprocessing program, which was corrected. All Minitrack data used in the data processing now had to be reprocessed.

At about 21 months from the start of the contract it was decided to investigate the puzzlingly slow rate of convergence of the solutions computed by NAP. The investigation revealed that the NAP matrix inversion was not being handled as described in the NAP documentation but in an iterative manner, which was extremely time consuming for the long arcs being considered. The complete equations as given in the existing NAP documentation were incorporated into NAP by R. Garza-Robles of Goddard Space Flight Center (Code 551). The rate of convergence was at least doubled.

With the help of the support programs already described and with the modified NAP program a four-arc run was now made on the 360/95. The total time span covered was 25 days and the computer time taken was 20 minutes. (At the start of this program, one 2.5 day arc was processed in 24 minutes and then the convergence rate of the solution was half of its present rate). "Optical" reference arcs were computed for the same time spans and a comparison of results was made. Advantage was taken of the current DBA contract (NAS5-11730) to develop an ionospheric error model for incorporation in the NAP program and one run was made using ionospheric corrections.

It should also be mentioned that the NAP-II program was successfully overlaid reducing its core requirements from 700,000 to 500,000 bytes.

This section is devoted to discussion of the reduction of Minitrack data using the NAP-II program and auxiliary programs written specifically for this task. Included in this section are discussions of the Minitrack error model and the Doppler effect and wave-propagation time delay as applied to predicted Minitrack measurements.

The second and third parts of this section discuss the handling and preprocessing of the Minitrack and Optical data respectively. The fourth part is devoted to the reduction of the data using the NAP-II program.

Results for a reduction effort are given in the fifth part. Results are given for the station at Ft. Myers and then a multi-station network which includes all of the Minitrack stations.

The last part of this section is a recommended procedure for reducing Minitrack data on a production basis.

As of special note: Appendix A-4 should be continuously referenced in the data processing cycle, as it contains restrictions on the programs and assumptions pertaining to the data.

2.1.1 The Minitrack Geometrical Error Model

This discussion will consider some of the general geometric properties of the Minitrack system. As with any interferometer system, the basic measurement mode is that of the phase path difference between the target and two antennas located some distance apart. The line between the antennas is referred to as the base line. The geometry for two cases is depicted below; 'A' for a target at a close range, and 'B' for a target at infinity.

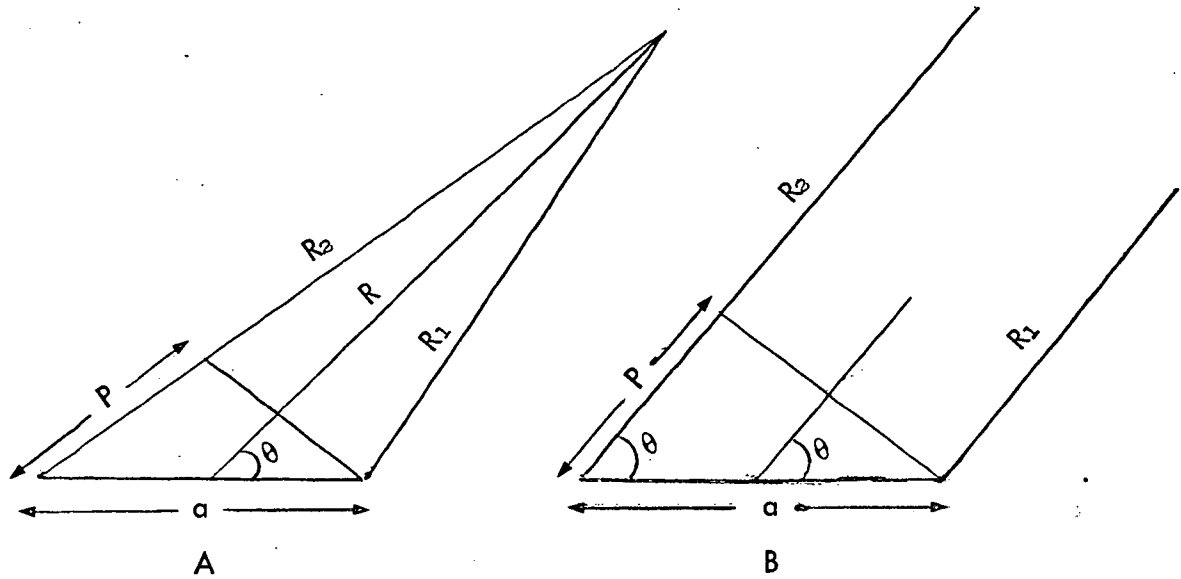


Figure 1

In Figure (1), A and B, the antennas are at the end of the base line a . The measurement made by the system can be interpreted as being proportional to the distance P . In both cases, P is defined as

$$P = R_2 - R_1.$$

Generally, we say that the system measures the cosine of the angle θ since

$$\cos \theta \approx \frac{P}{a}.$$

For the case of a point at infinity, the above expression is exact. For the case depicted in Figure 1A, it is only approximately true and $\cos \theta$ depends upon R as well as P and a .

For the Minitrack system, there are four antennas located at the ends of two perpendicular base lines. These base lines are usually located to intersect each other at their centers. However, since exact location of the phase centers of the antennas is not possible, there will be errors in the resulting data if they are interpreted as a true measurement of the cosine of the direction to the target. Therefore, the discussion which follows will investigate two areas. First, we will derive the relationship between the angle θ and the measurement P . Then, we will investigate errors in the antenna locations and how they effect the interpretation of the data.

To derive the desired expression, we can refer to Figure 1A. From this figure, the following relationships can be written.

$$\begin{aligned} P &= R_2 - R_1 \\ R_1^2 &= R^2 + \left(\frac{a}{2}\right)^2 - R a \cos \theta \\ R_2^2 &= R^2 + \left(\frac{a}{2}\right)^2 + R a \cos \theta \end{aligned}$$

We will redefine the measurement as

$$\ell_0 = \frac{P}{a} = \frac{R_2 - R_1}{a}$$

Then ℓ_0 approximates the cosine of θ . Proceeding with the algebra, give

$$\begin{aligned} P^2 + 2PR_1 + R_1^2 &= R_2^2 \\ P^2 + 2PR_1 - 2Ra \cos \theta &= 0 \\ (P^2 - 2Ra \cos \theta)^2 &= 4P^2 R_1^2 = 4P^2 \left(R^2 + \frac{a^2}{4} - Ra \cos \theta\right) \\ P^4 + 4R^2 a^2 \cos^2 \theta &= 4P^2 R^2 + P^2 a^2 \end{aligned}$$

solving for $\cos \theta$ give

$$\cos \theta = \ell_0 \sqrt{1 + \frac{a^2}{4R^2} (1 - \ell_0^2)}$$

the desired result. Note that as $R \rightarrow \infty$ then $l_0 \rightarrow \cos \theta$. Expanding gives

$$\cos \theta = l_0 + \frac{a^2}{8R^2} l_0 (1 - l_0^2) \dots$$

The maximum error in assuming $\cos \theta = l_0$ occurs when l_0 is approximately $1/\sqrt{3}$. This leads to a maximum error of about

$$\cos \theta - l_0 \approx \frac{a^2}{20R^2}.$$

For this analysis, we will consider the three dimensional case pictured in Figure (2). The antennas are located along the x and y base lines which are approximately a and b in length. We will then relate the path difference measurements to the desired cosines as a function of a , b and the errors in antenna location. This is pictured below.

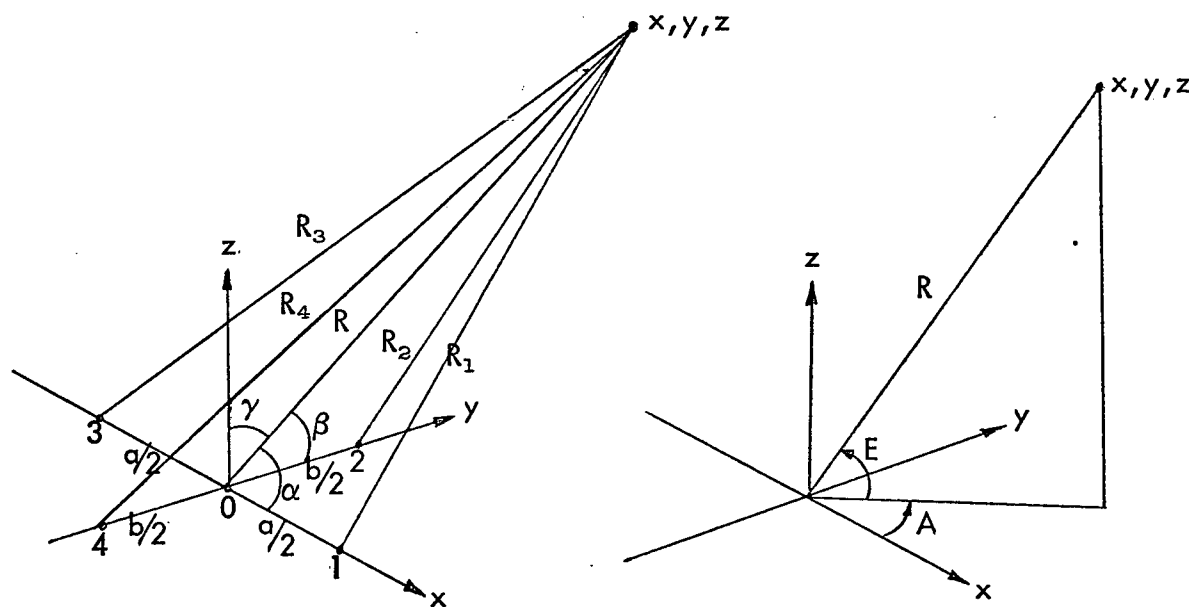


Figure 2

We have also included a figure which defines the measurements of azimuth and elevation. First a few definitions.

$$\ell = \cos \alpha$$

$$m = \cos \beta$$

$$n = \cos \gamma = \sqrt{1 - \cos^2 \alpha - \cos^2 \beta} = \sqrt{1 - \ell^2 - m^2}$$

$$x = R \cdot \ell = R \cdot \cos A \cos E$$

$$y = R \cdot m = R \cdot \sin A \cos E$$

$$z = R \cdot n = R \cdot \sin E$$

Thus,

$$\tan A = m/\ell ; \quad \cos E = \sqrt{\ell^2 + m^2}.$$

The measurements made by the system are given by

$$P = R_3 - R_1 = \sqrt{(x + \frac{a}{2} - x_3)^2 + (y - y_3)^2 + (z - z_3)^2} \\ - \sqrt{(x - \frac{a}{2} - x_1)^2 + (y - y_1)^2 + (z - z_1)^2}$$

$$Q = R_4 - R_1 = \sqrt{(x - x_4)^2 + (y + \frac{b}{2} - y_4)^2 + (z - z_4)^2} \\ - \sqrt{(x - x_2)^2 + (y - \frac{b}{2} - y_2)^2 + (z - z_2)^2}.$$

In the above, we have chosen the coordinates of the antennas to be

$$1 \quad x_1 + a/2, y_1, z_1$$

$$2 \quad x_2, y_2 + b/2, z_2$$

$$3 \quad x_3 - a/2, y_3, z_3$$

$$4 \quad x_4, y_4 - b/2, z_4.$$

In the case where there are no errors, then $x_1, y_1, \dots, y_4, z_4$ would all be zero. In that case, if P_0 is the value of P when all survey errors are zero, then

$$P_0 = \sqrt{(x + a/2)^2 + y^2 + z^2} - \sqrt{(x - a/2)^2 + y^2 + z^2} \\ = \sqrt{R^2 + ax + a^2/4} - \sqrt{R^2 - ax + a^2/4}$$

and

$$Q_0 = \sqrt{R^2 + by + b^2/4} = \sqrt{R^2 - by + b^2/4}$$

The solution to these two equations is the same as that presented in Section II. That is

$$\begin{aligned} \ell &= \frac{P_0}{a} \sqrt{1 + \frac{a^2}{4R^2} \left(1 - \frac{P_0^2}{a^2}\right)} = \frac{P_0}{a} + \frac{a^2}{8R^2} \frac{P_0}{a} \left(1 - \frac{P_0^2}{a^2}\right) + \dots \\ m &= \frac{Q_0}{b} \sqrt{1 + \frac{b^2}{4R^2} \left(1 - \frac{Q_0^2}{b^2}\right)} = \frac{Q_0}{b} + \frac{b^2}{8R^2} \frac{Q_0}{b} \left(1 - \frac{Q_0^2}{b^2}\right) + \dots \end{aligned}$$

However, of more importance is the effect on ℓ and m when the errors in antenna location are not zero. To explore this, we can expand the equations for P and Q about $x_1 \dots z_4 = 0$. This gives

$$P = P_0 - \frac{(x + a/2)x_3 + yy_3 + zz_3}{R_3} + \frac{(x - a/2)x_1 + yy_1 + zz_1}{R_1}$$

For purposes of this expansion, we can let $R_3 = R_1 = R$, giving

$$P = P_0 + \frac{x}{R}(x_1 - x_3) + \frac{y}{R}(y_1 - y_3) + \frac{z}{R}(z_1 - z_3) - \frac{a}{2R}(x_1 + x_3)$$

but

$$\ell = \frac{x}{R}, \quad m = \frac{y}{R}, \quad n = \frac{z}{R}$$

thus,

$$P = P_0 + \ell(x_1 - x_3) + m(y_1 - y_3) + n(z_1 - z_3) - \frac{a}{2R}(x_1 + x_3)$$

The actual measurement is given by

$$\ell_0 = \frac{P}{a},$$

and from before

$$\frac{P_0}{a} \approx \ell - \frac{a^2}{8R^2} \ell(1 - \ell^2) \approx \ell$$

Therefore, we finally have

$$\ell = \ell_0 - \ell_0 \frac{(x_1 - x_3)}{a} - m_0 \frac{(y_1 - y_3)}{a} - n_0 \frac{(z_1 - z_3)}{a} + \frac{(x_1 + x_3)}{2R}$$

Proceeding in the same manner, we have for m

$$m = m_0 - \ell_0 \frac{(x_2 - x_4)}{b} - m_0 \frac{(y_2 - y_4)}{b} - n_0 \frac{(z_2 - z_4)}{b} + \frac{y_2 + y_4}{2R} .$$

Normally, the last term of both expressions can be neglected. Alternately, if a and b are chosen so that $x_1 + x_3$ and $y_2 + y_4$ are zero, then it can be dropped from consideration.

For close-in ranges when the approximation

$$\ell = \frac{P_0}{a}$$

cannot be made, then the value of ℓ and m above can be used to compute the exact cosine value through the solution of

$$\ell = \frac{P_0}{a} + \frac{a^2}{8R^2} \frac{P_0^2}{a^2} \left(1 - \frac{P_0^2}{a^2} \right) .$$

2.1.2 The Doppler Effect and Wave-Propagation Time-Delay as Applied to Predicted Minitrack Measurements

Consider a satellite at position $\underline{r}(t)$ at time t transmitting an unmodulated signal at a constant frequency ν . The signal is received by two MINITRACK antennas situated at $\frac{a}{2}\underline{i}$ and $-\frac{a}{2}\underline{i}$, respectively, where a is the baseline length and \underline{i} is a unit vector in the x-direction. The phase difference between two signals arriving at the two antennas at the same time t is measured. If the two signals left the satellite at times t_A and t_B , respectively, then the phase-difference between the two signals is $2\pi\nu(t_A - t_B)$. The actual measurement, $\Delta\phi$, is the phase-difference divided by 2π . Hence,

$$\Delta\phi = \nu (t_A - t_B) . \quad (1)$$

or equivalently,

$$\Delta\phi = \frac{c (t_A - t_B)}{\lambda} . \quad (2)$$

where c is the velocity of light and λ the wavelength. We must also have,

$$|\underline{r}_A - \frac{a}{2}\underline{i}| = c(t - t_A) , \quad (3)$$

and

$$|\underline{r}_B + \frac{a}{2}\underline{i}| = c(t - t_B) , \quad (4)$$

where, in general, $\underline{r}_i = \underline{r}(t_i)$

Writing,

$$\tau = t_A - t_B , \quad (5)$$

we have by the mean-value theorem

$$\underline{r}_B = \underline{r}_A - \tau \dot{\underline{r}}_A + \frac{1}{2} \tau^2 \ddot{\underline{r}}_M , \quad (6)$$

where t_M is a time between t_A and t_B .

Writing

$$r_A = |\underline{r}_A| \text{ and } \underline{p}_A = \underline{r}_A / r_A, \quad (7)$$

we obtain from (6),

$$\underline{r}_B + \frac{1}{2} a \underline{i} = r_A \left[\underline{p}_A - \left(\frac{a}{r_A} \right) \left(\frac{c\tau}{a} \right) \frac{\dot{\underline{r}}_A}{c} + \frac{1}{2} \left(\frac{c\tau}{a} \right)^2 \left(\frac{a}{r_A} \right) \frac{a \ddot{\underline{r}}_M}{c^2} + \frac{1}{2} \left(\frac{a}{r_A} \right) \underline{i} \right] \quad (8)$$

Since $\underline{p}_A^2 = 1$, $\underline{p}_A \cdot \dot{\underline{r}}_A = \dot{r}_A$, and $\underline{i} \cdot \underline{p}_A = l_A$,

the direction cosine at time t_A , we obtain from (8),

$$\begin{aligned} |\underline{r}_B + \frac{1}{2} a \underline{i}| = r_A \left\{ 1 + \left(\frac{a}{r_A} \right) \left[l_A - 2 l_0 \frac{\dot{r}_A}{c} + l_0^2 \frac{a \underline{p}_A \cdot \ddot{\underline{r}}_M}{c^2} \right] \right. \\ \left. + \left(\frac{a}{r_A} \right)^2 \left[\frac{1}{2} \underline{i} - l_0 \frac{\dot{\underline{r}}_A}{c} + \frac{1}{2} l_0^2 \frac{a \ddot{\underline{r}}_M}{c^2} \right]^2 \right\}^{\frac{1}{2}} \quad (9) \end{aligned}$$

$$\text{where } l_0 = \frac{c\tau}{a} \quad (10)$$

Next we make some assumptions regarding the magnitude of the terms in (9).

We assume that,

$$|l_0| \leq 1 \quad (11)$$

(This will be justified later on when we shall show that l_0 is a first approximation to the direction cosine l_A)

$$\text{Write, } \frac{a}{r_A} = a_3, \quad (12)$$

and assume that $a_3 < 10^{-3}$, i.e. that the satellite is always more than 1000 baseline lengths from the station.

$$\text{Write } \frac{\dot{\underline{r}}_A}{c} = u_4 \quad (13)$$

and assume that $|\dot{\underline{r}}_A|/c < 10^{-4}$, i.e. that the satellite velocity is less than 10^{-4} times the velocity of light. Since $|\dot{\underline{r}}_A| \leq |\dot{\underline{r}}_A|$ it follows that $|u_4| < 10^{-4}$.

Next assume that, $\frac{r}{c^2} |\ddot{r}| < 10^{-7}$ (14)

Hence by the assumption made in (12) ,

$$\frac{a}{c^2} |\ddot{r}_M| < 10^{-10} \quad (15)$$

With the above assumptions equation (9) may be rewritten as,

$$|r_B + \frac{1}{2} a \underline{i}| = r_A \left\{ 1 + a_3 \left[l_A - 2l_0 u_4 + \frac{1}{4} a_3 + 0(10^{-7}) \right] \right\}^{\frac{1}{2}} \quad (16)$$

where $0(10^{-n})$ denotes terms of order 10^{-n} or less.

Equation (16) may be rewritten in the form:

$$\begin{aligned} |r_B + \frac{1}{2} a \underline{i}| &= r_A \left\{ 1 + a_3 l_A + \frac{1}{4} a_3^2 l_A^2 + a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) - 2l_0 u_4 + 0(10^{-7}) \right] \right\}^{\frac{1}{2}} \\ &= r_A \left(1 + \frac{1}{2} a_3 l_A \right) \left\{ 1 + a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) - 2l_0 u_4 + 0(10^{-7}) \right] \left[1 - a_3 l_A + 0(10^{-6}) \right] \right\}^{\frac{1}{2}} \\ &= r_A \left(1 + \frac{1}{2} a_3 l_A \right) \left\{ 1 + \frac{1}{2} a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) - 2l_0 u_4 + 0(10^{-7}) \right] \left[1 - a_3 l_A \right] \right\} \\ &= r_A \left\{ 1 + \frac{1}{2} a_3 l_A + \frac{1}{2} a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) (1 - \frac{1}{2} a_3 l_A) - 2l_0 u_4 + 0(10^{-7}) \right] \right\} \quad (16)' \end{aligned}$$

We obtain a similar expression for $|r_1 - \frac{1}{2} a \underline{i}|$ with a_3 replaced by $-a_3$ and $u_4 = 0$.

Hence:

$$|r_A - \frac{1}{2} a \underline{i}| = r_A \left\{ 1 - \frac{1}{2} a_3 l_A + \frac{1}{2} a_3 \left[\frac{1}{4} a_3 (1 - l_A^2) (1 + \frac{1}{2} a_3 l_A + 0(10^{-7})) \right] \right\} \quad (17)$$

Hence from (3), (4), (5), (16)', and (17),

$$c\tau = r_A a_3 \left\{ l_A - \frac{1}{8} a_3^2 (1 - l_A^2) l_A - l_0 u_4 + 0(10^{-7}) \right\} \quad (18)$$

It is easy to show that $\frac{1}{8} a_3^2 (1 - l_A^2) l_A = O(10^{-7})$. Hence from (10), (12), and (18)

$$l_0 = l_A - l_0 u_4 + O(10^{-7}).$$

Whence, by (13)

$$l_A = l_0 \left(1 + \frac{\dot{r}_A}{c}\right) + O(10^{-7}) \quad (19)$$

Hence we have shown that l_0 is a first approximation to the direction cosine l_A .

From (2), (5), and (10)

$$l_0 = \frac{\lambda \Delta \varphi}{a}, \quad (20)$$

and hence

$$l_A = \frac{\Delta \varphi}{a} \left[\lambda \left(1 + \frac{\dot{r}_A}{c}\right) \right] + O(10^{-7}) \quad (21)$$

From expression (21) it is easy to see that the term in (\dot{r}_A/c) represents the Doppler effect. We shall show that expression (21) may be further simplified.

From (3) and (17) we have

$$c(t - t_A) = r_A \left[1 + O(10^{-3}) \right] \quad (22)$$

Hence denoting the direction cosine at time t by l , we have by the mean value theorem

$$l = l_A + \frac{r_A}{c} \left[1 + O(10^{-3}) \right] l_A + \frac{1}{2} \frac{r_A^2}{c^2} \left[1 + O(10^{-3}) \right] l_N'' \quad (23)$$

where l_N is the direction cosine at some time t_N between t and t_A . Writing

$\underline{p} = \underline{r}/r$ we obtain

$$\begin{aligned} r \underline{\dot{p}} &= \underline{\dot{r}} - \dot{r} \underline{p} \\ &= \underline{p} \times (\underline{\dot{r}} \times \underline{p}) \end{aligned} \quad (24)$$

since $\underline{p}^2 = 1$ and $\underline{p} \cdot \underline{\dot{r}} = \dot{r}$. Differentiating (24) gives,

$$r \underline{\ddot{p}} = \underline{\dot{p}} \times (\underline{\dot{r}} \times \underline{p}) + \underline{p} \times (\underline{\ddot{r}} \times \underline{p}) + \underline{p} \times (\underline{\dot{r}} \times \underline{\dot{p}}) - \dot{r} \underline{\dot{p}} \quad (25)$$

Since $l = \underline{p} \cdot \underline{i}$ it follows that,

$$l \leq |\underline{p}|, \quad \dot{l} \leq |\dot{\underline{p}}| \quad \text{and} \quad \ddot{l} \leq |\ddot{\underline{p}}| \quad (26)$$

By (24),

$$r |\dot{\underline{p}}| \leq |\dot{\underline{r}}| \quad (27)$$

From (25) and (27)

$$\begin{aligned} r^2 |\ddot{\underline{p}}| &\leq |\dot{\underline{r}}|^2 + r |\ddot{\underline{r}}| + |\dot{\underline{r}}|^2 + \dot{r} |\dot{\underline{r}}| \\ &\leq 3 |\dot{\underline{r}}|^2 + r |\ddot{\underline{r}}| \end{aligned} \quad (28)$$

From (26) and (27) we have

$$\begin{aligned} \frac{r \dot{l}}{c} &\leq \frac{|\dot{\underline{r}}|}{c} \\ &= 0(10^{-4}) \end{aligned} \quad (29)$$

by our previous assumptions. From (26) and (28) we obtain

$$\begin{aligned} \frac{1}{2} \frac{r^2 \ddot{l}}{c^2} &\leq \frac{1}{2} \left[3 \frac{|\dot{\underline{r}}|^2}{c^2} + r \frac{|\ddot{\underline{r}}|}{c^2} \right] \\ &= 0(10^{-7}), \end{aligned} \quad (30)$$

by the assumptions made in (13) and (14) above.

We then have from (23), (29), and (30),

$$l = l_A + \frac{r_A}{c} \dot{l}_A + 0(10^{-7}) + \frac{r_A^2}{r_N^2} 0(10^{-7}) \quad (31)$$

By the mean value theorem

$$r_N = r_A + (t_N - t_A) \dot{r}_K$$

But $t_N - t_A \leq t - t_A = \frac{r_A}{c} [1 + 0(10^{-3})]$, Hence

$$\begin{aligned} |t_N - t_A| |\dot{r}_K| &\leq r_A |\dot{r}_K| / c [1 + 0(10^{-3})] \\ &= r_A 0(10^{-4}), \text{ where} \end{aligned}$$

$$r_N > r_A - r_A 0(10^{-4}), \text{ and } (r_A/r_N) \leq 1 + 0(10^{-4})$$

$$\text{Hence } l = l_A + \frac{r_A}{c} \dot{l}_A + 0(10^{-7}) \quad (32)$$

$$\text{But } r_A \dot{\underline{i}}_A = \dot{\underline{x}}_A - \dot{\underline{i}}_A \underline{l}_A, \quad (33)$$

$$\text{where } \dot{\underline{x}}_A = \underline{\dot{i}}_A \cdot \underline{i}$$

$$\text{Hence } \underline{l} = \underline{l}_A + \frac{\dot{\underline{x}}_A}{c} - \underline{l}_A \left(\frac{\dot{\underline{i}}_A}{c} \right) + 0(10^{-7}) \quad (34)$$

From (19) we obtain

$$\underline{l}_0 = \underline{l}_A \left(1 - \frac{\dot{\underline{i}}_A}{c} \right) + 0(10^{-7}),$$

Hence from the above and (36)

$$\underline{l} = \underline{l}_0 + \frac{\dot{\underline{x}}_A}{c} + 0(10^{-7}) \quad (35)$$

By the mean value theorem and (22)

$$\begin{aligned} \frac{\dot{\underline{x}}}{c} &= \frac{\dot{\underline{x}}_A}{c} + \frac{r_A}{c} \frac{\ddot{\underline{x}}_D}{c} \left[1 + 0(10^{-3}) \right] \\ &= \frac{\dot{\underline{x}}_A}{c} + 0(10^{-7}), \text{ by (14), where } \dot{\underline{x}} \text{ is the x-component of the} \\ &\quad \text{velocity at time } t. \end{aligned}$$

Hence,

$$\underline{l}_0 = \underline{l} - \frac{\dot{\underline{x}}}{c} + 0(10^{-7}).$$

Finally from the above and (20),

$$\boxed{\frac{\lambda \Delta \varphi}{a} = \underline{l} - \frac{\dot{\underline{x}}}{c} + 0(10^{-7})} \quad (38)$$

The following assumptions were made in deriving (38)

$$(a/r) < 10^{-3}, \quad (|\dot{\underline{i}}|/c) < 10^{-4},$$

and $r |\ddot{\underline{r}}|/c^2 < 10^{-7}$. If the only forces acting on the satellite are due to the Earth's gravity field then $|\ddot{\underline{r}}| = g R_E^2/R^2$, where g is the acceleration due to gravity at the Earth's surface, R_E is the radius of the Earth and R is the radius vector from the center of the Earth to the satellite. Since $r \leq 2R$ it then follows that $r |\ddot{\underline{r}}|/c^2 \leq [2g R_E/c^2][R_E/R]$ which is always less than 10^{-7} .

For the m direction cosine a formula similar to (38) holds true:

$$\boxed{\frac{\lambda \Delta\phi_m}{a} = m - \frac{\dot{y}}{c} + 0(10^{-7}) ,} \quad (39)$$

where in this case $\Delta\phi_m$ represents the phase difference of the North-South antenna pair.

2.2 MINITRACK DATA

2.2.1 Standard Minitrack Data Format

The following is the Standard Minitrack data message that is stored on magnetic tapes by satellite and by station. The message appears on teletype output as in the following sample.

Satellite ID
and date → &6406401 1 690103

Data → 4350.2639114.3580.2639114.1230.2639114.00380.2639114.215.2639114.
1456.3071750.4503.3231736.1217.3121830.00334.3251831.215.3391904.
1662.3591152.4505.3581199.1222.3761243.00335.3771280.215.3751324.
1861.4081559.4504.4241597.1217.4221636.00339.4252685.215.4321729.
2061.4741972.4505.4672022.1220.4761060.00342.4812083.215.4881142.
2263.5342388.4506.5391436.1222.5301463.00347.5411519.215.5472546.
2463.5911798.4507.5912840.1227.6082386.00348.6062920.215.6102969.
2664.6502208.4507.6491255.1228.6522305.00350.6721342.215.6792385.
2863.7162633.4505.7212679.1232.7312717.00351.7372762.215.7452802.
3064.7882057.4508.7992104.1236.8062143.00354.8202186.215.8192239.
3265.8572483.4507.8672528.1238.8342574.00358.8842604.215.8961652.
3467.9482918.4507.9431950.1238.9612006.00359.9592031.215.9802078.
3668.0162345.4508.0281380.1241.0372431.00366.0482459.215.0582517.
3867.1022771.4509.1162812.1247.1242870.00365.1312904.215.1412946.
4068.1892200.4507.2011247.1249.2102297.00366.2152342.215.2252384.
4269.2831634.4510.2992684.1251.2932731.00371.3131768.215.3051830.
4469.3721086.4511.3871115.1256.3921171.00370.4031207.215.4121258.
4670.4741514.4511.4821560.1259.4921607.00376.4941661.215.5021704.
4870.5701966.4511.5801993.1261.5871055.00376.5981087.215.6031146.
5071.6691395.4513.6841450.1265.6931503.00379.6941544.215.7081598.
5271.7781848.4512.7841909.1268.7951947.00383.8001990.215.8281045.
5472.8891289.4514.8961351.1271.9131397.00385.9151439.215.9310481.
5672.9841751.4515.0030801.1273.0231826.00387.0161901.215.0611942.
5874.1140218.4516.1190238.1278.1370292.00390.1691338.215.1500394.
0074.2341658.4615.2440702.1281.2700759.00393.2860777.215.2850835.
0274.3590109.4616.3740175.1283.3990211.00397.3930246.215.4070299.
0475.4750568.4619.5000613.1287.5170665.00300.4830695.215.5330745.
0676.6200003.4619.6460072.1290.6330121.00302.6540176.215.6470231.
0879.7680522.4620.7230527.1294.7930567.00305.7900650.215.3420678.
1078.8850954.4620.8280014.1298.9310025.00308.9620126.215.9890143.
1280.1020389.4621.0980426.1200.0230478.00309.0300507.215.0990595.

Satellite ID → 6406401
Terminating
Message 03/1321Z JAN LWNK

The format for the message is as follows:

MESSAGE FORMAT

<u>Character(s)</u>	<u>Contents</u>
1, 2	second (time) of frame start
3, 4	hundreds and tens digits of east-west medium phase
5	period "." separator
6 to 8	first east-west fine phase
9	signal strength indicator (AGC)
10 to 12	first north-south fine phase
13	period "." separator
14, 15	minute of frame start
16, 17	hundreds and tens digits of east-west coarse phase
18	period "." separator
19 to 21	second east-west fine phase
22	signal strength indicator (AGC)
23 to 25	second north-south fine phase
26	period "." separator
27, 28	hour of frame start
29, 30	hundreds and tens digits of north-south medium phase
31	period "." separator
32 to 34	third east-west fine phase
35	signal strength indicator (AGC)
36 to 38	third north-south fine phase
39	period "." separator
40 to 42	day of year for frame start
43, 44	hundreds and tens digits of north-south coarse phase
45	period "." separator
46 to 48	fourth east-west fine phase

MESSAGE FORMAT (Cont'd)

<u>Character(s)</u>	<u>Contents</u>
49	signal strength indicator (AGC)
50 to 52	fourth north-sound fine phase
53	period "." separator
54	equatorial/polar antenna indicator 1 = equatorial 2 = polar
55, 56	station number 03 = FTM YRS 15 = WNKFLD 01 = BPOINT 05 = QUITOE 16 = JOBURG 13 = COLEGE 06 = LIMAPU 19 = ALASKA 17 = MOJAVE 08 = SNTAGO 21 = ORORAL 14 = GRDFKS 12 = NEWFLD 23 = MADGAR 18 = WOOMER
57	period "." separator
58 to 60	fifth east-west fine phase
61	signal strength indicator (AGC)
62 to 64	fifth north-south fine phase'
65	period "." separator

2.2.2 Extracting and Sorting Minitrack Data

The GEOS-A Minitrack data extracting program and the sorting program are special purpose programs each with a single function. The extracting program reads a Master Minitrack data storage tape and extracts only data taken on the GEOS-A satellite. This data is copied to another magnetic tape in the same format (same as given in the example in 2.2.1). This results in a data tape of GEOS-A Minitrack data grouped by station in chronological order. The FORTRAN listing of the extracting program is given in Appendix A-2.1. The requirements for the program operation are:

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Card Input	Card Reader	Program Source Deck
Tape Input	Data Set 9 (FT09F001)	Minitrack messages for several satellites
Tape Output	Data Set 11 (FT11F001)	Minitrack messages for GEOS-A (Satellite ID 65891)
Printed Output	Data Set 6	Total number of messages Number of GEOS-A messages First 100 messages from output tape

The tape output (Data Set 11) from the extract program is the input data tape for the sort program. This program sorts messages in time-sequence. It also eliminates duplicate messages. Messages for the same station and antenna configuration are assumed to be duplicates if they commence within 30 seconds of each other. If two duplicate messages are of unequal length, then the shorter message is discarded. If they are of the same length, then the last received message is discarded.

The length of a message is determined by the number of good records it contains. The characters in each record are checked for numeric characters and periods in the appropriate places. A record with an error is discarded. The first "proper" record of a message is the calibration line. If this contains an error, the whole message is discarded. It has been found that in some messages the calibration line and subsequent records are repeated within the same message. For this reason, every record is compared with the calibration line. If a record is found to be identical to the calibration line, then this is regarded as the first "proper" record of the message. All previous "proper" records are ignored.

Messages containing fewer than 5 records are discarded. The output tape from the sort program is in the same format as the input tape.

The FORTRAN listing of the sort program is given in Appendix A-2.2.

The requirements for running the sort program are as follows.

<u>Function</u>	<u>Unit</u>	<u>Description</u>																				
Card Input	Card Reader	Source Program																				
Data Cards	Data Set 5	17 Cards Required (See Appendix A-2.2) Cards 1-16 (One card for each Station)																				
		<table><tr><th><u>Card Column</u></th><th><u>Word</u></th><th><u>Definition</u></th><th><u>Format</u></th></tr><tr><td>1-5</td><td>KSTA</td><td>Station ID</td><td>I5</td></tr><tr><td>6-10</td><td></td><td>Blank</td><td></td></tr><tr><td>11-16</td><td>STATIO</td><td>Station Name</td><td>A6</td></tr></table>	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>	1-5	KSTA	Station ID	I5	6-10		Blank		11-16	STATIO	Station Name	A6				
<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>																			
1-5	KSTA	Station ID	I5																			
6-10		Blank																				
11-16	STATIO	Station Name	A6																			
		Card 17																				
		<table><tr><th><u>Card Column</u></th><th><u>Word</u></th><th><u>Definition</u></th><th><u>Format</u></th></tr><tr><td>1-8</td><td>INTAPE</td><td>Input tape No.</td><td>A8</td></tr><tr><td>9-13</td><td>INFILE</td><td>File No.</td><td>I5</td></tr><tr><td>14-21</td><td>NDTAPE</td><td>Output tape No.</td><td>A8</td></tr><tr><td>22-26</td><td>NDFILE</td><td>File No.</td><td>I5</td></tr></table>	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>	1-8	INTAPE	Input tape No.	A8	9-13	INFILE	File No.	I5	14-21	NDTAPE	Output tape No.	A8	22-26	NDFILE	File No.	I5
<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>																			
1-8	INTAPE	Input tape No.	A8																			
9-13	INFILE	File No.	I5																			
14-21	NDTAPE	Output tape No.	A8																			
22-26	NDFILE	File No.	I5																			
Tape Input	Data Set 9 (FT09F001)	Input tape containing Minitrack messages (Output tape from Extract program)																				
Tape Output	Data Set 10 (FT10F001)	Output tape containing sorted Minitrack messages																				
Printer Output	Data Set 6	A list of message numbers (as sequenced on input tape) of rejected messages together with reasons for rejection A list of output information giving the following. (The actual data message is not printed out): Sequence number on output tape Sequence number on input tape Station ID (KSTA) Station Name (STATIO) Day Number (1 to 366) Month Day of Month (not correct for leap year) Seconds of day Hours Minutes } (of day) Seconds } Number of lines in message																				

2.2.3 The Minitrack Preprocessor

The purpose of the Minitrack preprocessor is to make known corrections to the Minitrack data and output a magnetic tape containing corrected data in a format acceptable to the NAP-II program. Basically, the preprocessor reads the raw phase data message, computes phase differences, makes corrections and then converts the corrected phase differences to direction cosines. This process is explained in detail in references 1 and 2.

The Minitrack preprocessor used was based on that developed by the Goddard Space Flight Center Network Computation Section (references 1 and 2). The program was extensively modified by W. M. Rice (GSFC, Code 551). A few minor modifications were then made by DBA Systems, Inc. under this contract. A complete listing of the preprocessor program is given in Appendix A-2.3. Sample JCL for running the program is also given.

Changes Made by W. M. Rice. A Minitrack message contains, in general, 155 measurements of phase differences between two antenna pairs. The preprocessor converts these to 155 pairs of direction cosines. A quadratic fit is then made to each set of 155 direction cosines. The resultant output is a single pair of direction cosines (the fitted midpoint values). The program is made more complicated by the fact that the ambiguity of the direction cosines must be resolved using additional information in the Minitrack message (Reference 2). However, this is only done to the fitted midpoint values. In the Rice version of the program the ambiguity is resolved for all direction cosines. The output consists of all direction cosines and is in a format that can be used as an input to the NAP program. The time associated with each measurement is given at the instant that the signal being analyzed arrived at the relevant antenna pair.

Changes Made by DBA Systems, Inc. To facilitate the data preparation for the NAP program, the Minitrack preprocessor was modified to punch out the three control cards (Categories 201, 202, and 999) required for each data message. (For a description of the required control cards, see reference 4).

Although nominally there is a single time associated with each pair of direction cosines, this is not so in practice. Differences arise due to different filter delays associated with each direction cosine and also due to different counter delays (reference 3). As the volume of printed output from the NAP program is proportional to the total number of different time points, the output volume could be reduced by one half, if each pair of direction cosines were adjusted to the same time point. This was done. The adjusted time point was chosen as the average time of the two measurements. For a typical NAP run, this reduced the output volume by half.

A modification was also made to output on tape in a NAP input format, the fitted midpoint values of the original program. The idea behind this was that the fitted midpoint values could be used initially as an input to NAP, the "all data points" input being reserved for the final iterations through NAP. This in theory should have reduced the total computer time required. In practice, however, it was found that the "all data points" input when processed through NAP, provided the user with an extremely useful criterion for determining the quality of the data in a Minitrack message -- the standard deviation of the error of all measurements within a message. For this reason, little use was made of the "fitted midpoint" input.

To help in the analysis of the results of the NAP program, a modification was made to print out a summary of the results of the preprocessing. This summary contained the following information for each station: For each data message the midpoint time, the three midpoint direction cosines and their rates of change, plus the prepass calibration constants.

Finally, an error in the way the 2 Hz filter delay was being applied was corrected.

A Program Error. Messages spanning midnight are not handled correctly by the program. A Minitrack message typically spaces a time interval of one minute or one half of a minute, so that this occurs very infrequently, but the program error should be corrected.

The Minitrack preprocessor exists as a modified version of the original program developed by GSFC. Some of the information used in the original program is not used in its present form. The input cards to the program, however, are the same as with the original program. Consequently, a large number of cards containing little information are required.

The following information is required for operation of the program.

<u>Function</u>	<u>Unit</u>	<u>Description</u>		
Card Input	Data Set 5	Station Calibration Constants		
		Card 1 Blank		
		Card 2 Station Constants		
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u> <u>Format</u>
		1-6	STATIO	Any 6 alpha-numeric characters A6
		7		Blank

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		8, 9	KSTA	Station number	I2
		10-13	KFA	Time adjustment EW-channel	I4
		14-17	KFB	Time adjustment NS-channel	I4
		18-20		Blank	
		21-24	EWM	Phase bias medium antenna, EW-channel	F4.3
		25-27	CLEWM	Cable length in- equality, EW- medium channel	F3.3
		28-31	EWC	Phase bias coarse antenna, EW-channel	F4.3
		32-34	CLEWC	Cable length in- equality, EW- coarse channel	F3.3
		35		Blank	
		36-39	EWFEQ	Phase bias equatorial fine antenna, EW-channel	F4.3
		40-43	EWFPO	Phase bias polar fine antenna, EW-channel	F4.3
		44-46		Blank	
		47-50	NSM	Phase bias medium antenna, NS-channel	F4.3
		51-53	CLNSM	Cable length in- equality NS-medium channel	F3.3
		54-57	NSC	Phase bias coarse antenna, NS-channel	F4.3
		58-60	CLNSC	Cable length in- equality NS-coarse channel	F3.3
		61		Blank	

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		62-65	NSFEQ	Phase bias equatorial fine antenna, NS-channel	F4.3
		66-69	NSFPO	Phase bias polar fine antenna, NS-channel	F4.3
		70-74		Blank	
		75-79	DATE	Date of calibration	I6
		Cards 3 thru 10		Blank	
		Cards 11-135		15 sets of cards 2 thru 10 are required. One set for each of the Minitrack stations	
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		1-5	KSAID	Satellite ID	I5
		6-24		Blank	
		25-32	FREQ	Satellite transmitter frequency (MHZ)	F8.3
		Card 137		Blank card terminates data set.	

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
Card Input	Data Set 8	Data Selection Control Cards			
		Card 1	80 alphanumeric characters used to write a message in the pre-processed printout		
		Card 2	(more than one card can be used)		
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		1-10	ILOW, IHIGH	Program will process messages between ILOW and IHIGH	2I5

<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
11-15	IYEAR	2-digit integer for year of measurements e.g. 1966 = 66	I5
16-20	NEWARC	Arc number assigned to measurements. If several ILOW, IHIGH cards define some arc, NEWARC should be blank on all but first card.	I5
21-25	NAPEND	Normally left blank -1 = more data tape to follow 0 = normal termination 1 = no terminal record written (for tape addition)	

According to Ref. 4, the input tape to NAP should terminate with a negative number in the last record. However, with current versions of NAP this is no longer necessary. If NAPEND is left blank, this terminal record is written on the tape. If on the last "ILOW, IHIGH" card NAPEND is set equal to a positive non-zero integer, then the terminal record is not written. (The reason for this option is to facilitate combination of two or more data tapes into a single tape).

If the messages being processed are contained on more than one tape, then NAPEND should be set to a negative integer on the last "ILOW, IHIGH" card referring

<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
--------------------	-------------	-------------------	---------------

to a tape that is to be followed by another tape. e.g., if data messages to be processed are contained on three tapes such that

FT09F001 defines tape 1,
FT09F002 defines tape 2,
FT09F003 defines tape 3,

then the last "ILOW,IHIGH" card of tape 1 should have a negative NAPEND, the last "ILOW,IHIGH" card of tape 2 should have a negative NAPEND, the last "ILOW,IHIGH" card of tape 3 should have either a blank or a positive NAPEND.

Card 3, 4

Blank

Each "ILOW,IHIGH" card should be followed by two blank cards. The program actually has a restart capability. The blank cards must be inserted if the user does not wish to avail himself of the restart facility. For use of the restart facility the user is referred to the program listing, Appendix 2.3

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Tape Input	Data Set 9	Data tape(s) containing Minitrack messages to be processed
Tape Output	Data Set 12	Preprocessed output of "all data points" in a NAP-II input format
Tape Output	Data Set 19	Preprocessed output of "fitted midpoint" in NAP-II input format

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Punched Card Output	Data Set 7	NAP-II control cards for each data message. These are the start-stop times for that station data set (NAP-II cards group 201, 202, 999)
Printed Output	Data Set 6	Raw Minitrack messages with each message followed by the computed direction cosines for each data point. (Direction cosines are also given in terms of Minitrack counts.)
	Data Set 11	Printout of intermediate results obtained in pre-processing
	Data Set 13	Input station constants (See data set 5) List of all messages that have not been preprocessed and reasons why. Pass summary information (number of messages per station, time of last message for each station) Information required for restart.
	Data Set 14	Summary of preprocessed results arranged in time sequence (station, time, direction cosines, direction cosine rates)
	Data Sets 20 thru 51	32 data sets -- 1 per station. Although there are only 16 stations the program treats a station operating in the equatorial mode as one station with station number KSTA (See data set 5) and the same station operating in the polar mode as a different station with station numbers KSTA+100. Each data set contains preprocessed results (for each station) arranged in time sequence (time, direction cosines, direction cosine rates, prepass calibration constants.)

Suggested Running Time

For the 360/91	CPU time	11 minutes per 1000 messages
For the 360/95	CPU time	14 minutes per 1000 messages

2.3 Optical Data

2.3.1 Standard Optical Data Format

The optical data used in this study was obtained from the NASA Space Sciences Data Center (NSSDC) at Goddard Space Flight Center. The data was on magnetic tape in the "GEOS format." A complete description of the data format is available from the NSSDC. The "GEOS format" for optical data is basically 80 column card images stored on magnetic tape. Each card image contains the following.

<u>Card Column</u>	<u>Description</u>
1-6	Satellite identification
7	Type of coordinates (RA and DEC)
8	Observation identifier
9-11	Timing standard deviation
12-13	Time identifier
14-18	Station number
19-34	GMT of observation
35-53	Observation data
54-59	Date of plate reduction
60-71	Code information as to processing
72-80	Description of random error

A separate data tape for each tracking network is normally obtained from the NSSDC. For example, in this study optical data from the STADAN network and the SAO network was to be used. Two data tapes were obtained, one for STADAN and one for SAO. In order to simplify the optical preprocessing, it was necessary to merge the two tapes. A special program was written to this task. The program listing is given in Appendix A-2.4. The program merges two time sequenced optical data tapes into a single tape which will be the input data tape for the optical pre-processor. Data for each month is written on a separate file numbered sequentially on the same tape.

The following is required to execute the merge program:

<u>Function</u>	<u>Unit</u>	<u>Description</u>																
Card Input	Data Set 5	Tape and file number of output tape used for printout.																
		<table><tr><th><u>Card Column</u></th><th><u>Word</u></th><th><u>Definition</u></th><th><u>Format</u></th></tr><tr><td>1-8</td><td>TAPE</td><td>8-character tape number</td><td>A8</td></tr><tr><td>9-10</td><td></td><td>Blank</td><td></td></tr><tr><td>11-15</td><td>IFILE</td><td>File number of first month of the combined tape</td><td>15</td></tr></table>	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>	1-8	TAPE	8-character tape number	A8	9-10		Blank		11-15	IFILE	File number of first month of the combined tape	15
<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>															
1-8	TAPE	8-character tape number	A8															
9-10		Blank																
11-15	IFILE	File number of first month of the combined tape	15															
Tape Input	Data Set 1	Data tape with STADAN stations.																
Tape Input	Data Set 2	Data tape with SAO station.																
NOTE: The user should examine the printed output of the input data tapes to determine if there are dummy or non-essential data records on the tapes.																		
Tape Output	Data Set 3	Merged data output (Input tape to Optical Preprocessor) JCL cards required for each month there is data. FT03F001 should have tape and file no. corresponding to card input, data set 5. The reason for writing a separate file for each month is to minimize tape search required in the optical preprocessor.																
Printed Output	Data Set 6	Printed output of the merged output data tape (data set 3). Each page has a heading giving the year and month of the data and the tape and file number on which the data may be found on tape.																

2.3.2 Optical Data Preprocessing

The program assumes that the data on the input tape (data set 1) is arranged in time sequence. The program resequences the data such that the data for each station/orbit combination is sequential. An orbit is defined as consisting of TORBT seconds (45 minutes). Furthermore, each "station/orbit" is subdivided into passes (photographic plates) where each pass may be TPASS seconds (45 seconds) long. The data itself is converted to radians and output on data set 2 in the NAP input format. NAP control cards are punched (data set 7) for each pass.

For SAO stations (station ID 29XXX), the input data is given in the 1950.0 coordinate system. This is converted to the "true of date" coordinate system. The precession and nutation formulae used are based on those given in the Explanatory Supplement to the Astronomical Ephemeris and the American Ephemeris and Nautical Almanac (Her Majesty's Stationary Office, London, 1961). Also, the time of the SAO stations is given as Atomic time. This is converted to UTC using information provided by the user (data set 4). A further complication arises in the case of the SAO stations because, for those stations, the time associated with the data is the time of observation rather than the time that the signal left the satellite. An " r/c " correction should thus be applied to the timing of the orbit determination program. Unfortunately, NAP-II does not possess this capability. A temporary fix has, therefore, been made (subroutine SAOCOR) utilizing the fact that, nominally, the GEOS satellite always flashes on the even second. Since this is not exactly true, it is recommended that the user compare the output time for the SAO stations with those of other stations and make the appropriate adjustments on NAP "704" cards (see reference 4).

The following cards are required for running the optical preprocessor.

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Card Input	Data Set 5	Station and data set control cards.

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
		<u>Station Cards:</u> Up to 30 observing stations may be used. One card for each station.			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		1-5	KSTA	Station No. given on NAP 201/202 cards.	I5
		6-10		Blank	
		11-18	STNAM	8-alphanumeric character station name.	A8
		19-20		Blank	
		21-25	ISTA	Station ID	I5
		26-30	IEND	Blank except for last "station" card where a negative integer is used to indicate last station card.	I5
		<u>Data Set Cards:</u> One card for each arc of data.			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		7-5	NARC	Arc number required for NAP control cards.	I5
		6-10		Blank	
		11-16	IYMDB	Year, month and day of beginning of arc (e.g. 660312).	I6
		17-19	IHB	Hour of beginning of arc.	I3
		20-22	IMB	Minute of beginning of arc.	I3
		23-32	SECB	Seconds of beginning of arc.	D10.0
		33-38	IYMDE	Year, month and day of end of arc.	I6

<u>Function</u>	<u>Unit</u>	<u>Description</u>			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		39-41	IHE	Hour of end of arc.	I3
		42-44	IME	Minutes of end of arc.	I3
		45-54	SECE	Seconds of end of arc.	D10.0
Card Input	Data Set 4	Correction from A.I to UTC time. Required only if SAO stations are to be processed. Any number of these cards may be used and the program will use a linear interpolation to any required time. At least two cards required.			
		<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	<u>Format</u>
		1-2	IYR	Year	I2
		3-4	IMO	Month	I2
		5-6	IDA	Day	I2
		7-10		Blank	
		11-20	COR	A.I minus UTC on year, month, day (IYR,IMO,IDA)	F10.5
Tape Input	Data Set 1	Data tapes to be processed (output from Merge or GEOS formatted data tape). If more than one data tape is used, then JCL will be modified to accommodate (e.g. FT01F001 for first tape, FT01F002 for second tape, etc.).			
Tape Output	Data Set 2	Preprocessed data tape to be input to NAP-II.			
Printed Output	Data Set 6	Print of preprocessed data.			
	Data Set 3	Printed output of input (data sets 4 and 5).			
	Data Set 12	Summary of data.			
Punched Output	Data Set 7	NAP Control Cards for timing/station information, NAP Cards 201, 202, 999 (see Reference 4).			

2.4 REDUCTION OF MINITRACK DATA

2.4.1 PRENAP Program

The processing of 20 days of Minitrack data requires about 5000 input cards. In order to reduce the number of cards that must be handled for a NAP-II run, the NAP-II control cards are written on magnetic tape. This "control card" tape is then updated and communicated to the NAP-II program via the PRENAP program. In this mode of operation, execution of the PRENAP program becomes the first step of a complete NAP-II run.

The following is a listing of the program to copy the NAP-II control cards onto magnetic tape.

Job Card

```
// EXEC FORTRAN
```

```
//SOURCE.SYSIN DD*
```

```
    IMPLICIT REAL * 8 (A-H,0-7)
```

```
    DIMENSION KAT(2),KEY(10),DATA(2)
```

```
100  FORMAT (13,12,A8, 10I3,D22.8,D15.8)
```

```
    DO 300 I=1, 10000
```

```
    READ (5, 100,END=400) KAT,XLABEL,KEY,DATA
```

```
    WRITE (9) KAT,XLABEL,KEY,DATA,I
```

```
300  CONTINUE
```

```
400  ENDFILE 9
```

```
    REWIND 9
```

```
200  FORMAT (1X,3I8,A8, 10I3,2D19.8)
```

```
    DO 330 J=1, 10000
```

```
    READ(9,END=500) KAT,XLABEL,KEY,DATA,I
```

```
    WRITE(6,200) I,KAT,XLABEL,KEY,DATA
```

```
330  CONTINUE
```

```
500  STOP
```

```
    END
```

```

/*
// EXEC LOADER, PARM='MAP,CALL,SIZE=100K',REGION.GO=110K
//GO.FT09=001 DD UNIT=9TRACK,LABEL=(4,BLP),DSN=MRGDAP,DISP=(NEW,KEEP),
// DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3204) VOL=SER=34517C
//GO.DATA5 DD*

```

Once the NAP-II cards are written on tape, the function of the PRENAP program is to update the "cards" on tape and to convert the binary "cards" tape to a format acceptable to the NAP-II program. The PRENAP program is listed in Appendix A-2.6. At the end of the program listing is an example of the JCL cards needed and a sample set of update cards.

The program is normally loaded as a binary object deck (Appendix A-2.6 JCL cards). The function of the peripheral equipment needed to execute the PRENAP program are:

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Input Tape	Data Set 9	NAP-II control cards on magnetic tape. (Output from program given above).
Disk File	Data Set 10	Used as an intermediate scratch tape.
Disk File	Data Set 12	Used to pass "updated" NAP-II control cards to NAP-II program for execution.
Card Input	Data Set 5	Updater cards for NAP-II control cards. If no update is required, data set 5 should be left empty. There would probably be no update the first time NAP-II is run for a particular job. The program prints out instructions on how to update "cards".

2.4.2 Use of NAP-II Program

The NAP-II program is a very flexible analysis tool providing the user with considerable freedom for designing and executing data reductions. Consequently, the user must have a good understanding of the program uses to attain efficient

utilization. This can only be done through use of the program and its various options. The functions of the program are discussed in reference 4.

The type of information required to execute NAP-II is given as follows:

<u>Type of Information</u>	<u>Categories</u>
General and planetary information	101, 102, 103, 151
Comments	150
Station survey	301, 302, 303
Totally stable parameters	601, 602
Measurement definitions	701, 702, 703, 704 (Sets 0 only)
General arc information	104, 205, 206
Arc stable parameters	601, 602
General pass information	201, 202, 203, 204
Pass stable parameters	601, 602
Pass comments	152
Overrides for measurement definitions for a pass	701, 702, 703, 704 (Sets 1 only)
End of pass, arc, or all control data	999

The station numbers (category 300) are preassigned by the Minitrack and the optical data preprocessors, depending on the order of the Minitrack Station Calibration Cards and the Optical Stations Control Cards. This controls both the station ID numbers and the user assigned station numbers. These two programs also provide the timing information cards (category 200 and 999) as part of their output. The other cards must be set up by the user. The information required by the various groups of cards is given in reference 4.

Once a "master" set of cards has been set-up, subsequent runs can be made with new data sets by changing the following quantities,

- State vectors - Category 601, 205
- Greenwich Hour Angle - Category 206

- Lunar and Solar Coordinates - Category 104
- Timing information - Output from data preprocessors.

These cards can be changed via the PRENAP program.

To run the NAP program, it is essential to have a reasonably good estimate of the state vector at the initial epoch. Before the user tries to solve for any parameters, he should make an initial run, which will allow the POSTNAP program to edit out obviously bad data and correct the lobe assignments made by the Minitrack preprocessor. Once this has been done, the user can go ahead and solve for any parameters he wishes. As the user improves his estimate of the initial state vector, he may wish to modify his definition as to what constitutes bad data.

The NAP-II program outputs the following information on disk or tape:

- measurement discrepancies (FT37F001)
- current estimates of error model parameters (FT37F002)
- data tape with the mid-data point for each pass (FT37F003) .

For multi-arc data processing, it is recommended that the user switch from using the data tape output from the Minitrack preprocessor to the "single data point per pass" data tape. When using the single data point prepass, the Category 704 cards have to be deleted, because the biases have already been applied. The run time advantage of using one data point instead of all data points (which may be as many as 155) is considerable. The loss of accuracy is negligible.

The recommended procedure for reducing Minitrack data is summarized in Section 2.6.

There were changes made to the NAP-II program to effect the procedure for reducing Minitrack data. The need for some of these changes was discussed in the preface of this report. Without going into great detail, the changes to the particular subroutines are as follows:

- Changes to Subroutine ENEXPS

This subroutine computes two sets of series: (1) the power series expansions of n -heavenly bodies, and (2) the power series expansion defining whether or not the satellite is exposed to solar radiation. The subroutine was completely reprogrammed, making the new version seven times faster than the old. One of the factors contributing to the increased computational speed of the new program is that it computes the $n(n-1)/2$ different distances between n bodies, and no more. The old program somehow managed to compute more distances than this so that some distances had to be identical. The old program had a programming error in the computation of the "shadow" series so that the two programs do not agree as far as shadow series expansion is concerned. The FORTRAN listing of the subroutine is given in Appendix A-3.1.

- Changes to Subroutine EXPAND

Subroutine EXPAND computes two sets of series: (1) the power series expansion of the acceleration due to the full gravity field, expressed as a sum of spherical harmonics, of the main attacking body, and (2) the power series expansion of the acceleration due to atmospheric drag. The part dealing with the gravity field was completely rewritten. The mathematical analysis for this is given in reference 5. The FORTRAN listing of the subroutine is given in Appendix A-3.2.

- Changes to Subroutine VARIEQ

Subroutine VARIEQ computes the two sets of series: (1) the power series expansion of the variational matrix due to the full gravity field of the main attracting body, and (2) the power series expansion of the variational matrix due to atmospheric drag. The FORTRAN listing of the subroutine is given in Appendix A-3.3.

- Changes to Subroutine FINALP

A small change was made in this subroutine to output on disk (data set 10) the computed values for the error model terms. Note that the call to this routine precedes the final call to subroutine RESID so that the quantities output by this routine on data set 10 precede those output by RESID. The FORTRAN listing is given in Appendix A-3.4.

- Special Subroutine PRTIAL

The standard subroutine PRTIAL computes the discrepancies between observed and predicted measurements and also the partial derivatives of the predicted measurements with respect to those error model terms that affect the predicted measurements. The computed values are then stored on a disk file (ISFILE). Later in the program subroutine SOLVER forms the normal equations from this disk file and solves the equations to give the computed values for the error model terms. The quantities on the disk file are also used by subroutine RESID which prints the measurement residuals. (The residuals are updated discrepancies between observed and predicted measurements, where the predicted measurements reflect the latest values (from SOLVER) of computed error model terms. The quantities involved in this computation are the discrepancies and partial derivatives from subroutine PRTIAL, which are stored on disk file, and the difference between the computed values for the error model terms and the values used by subroutine PRTIAL for the predicted measurements).

Obviously, the more data points that are stored on ISFILE the longer it will be. For a one-week long arc of Minitrack data, ISFILE is about 3,000,000 bytes long (20 cylinders of disk space).

To print the final residuals would require a further 9,000,000 bytes (60 cylinders of disk space). Together with the remaining disk requirements of the NAP program this puts a severe strain on the total 360 system.

To make it practicable to use the NAP program for multi-arc cases, several changes were made to subroutine PRTIAL.

Changes to Subroutine PRTIAL. For each measurement all discrepancies for a pass (Minitrack message) are averaged to give the mean measurement discrepancy. The standard deviations are also computed and any discrepancies differing from the mean by more than three standard deviations are rejected. (The process is iterative, since as soon as a discrepancy is rejected a new mean and standard must be computed). The mean discrepancies are then output on ISFILE together with the appropriate partial derivatives. The time associated with the mean discrepancies is also computed. These measurements are written on the same tape on disk file as the discrepancies (FT37F001). They are also written on disk (FT35F001) in a NAP observation tape format. The standard deviations and the number of measurement points (not rejected) are written on disk (FT36F001).

The FORTRAN listing of the subroutine is given in Appendix A-3.6.

• Changes to Subroutine RESID

- There are two subroutines RESID that can be used in NAP-II. These are identified as STANDARD Subroutine RESID and SPECIAL Subroutine RESID. The Special subroutine was written to make multi-arc runs practical in terms of run time.

Standard Subroutine RESID. Three sets of changes were made to this subroutine. The new subroutine will work only if there are two or fewer kinds of measurements per station-pass. The first change involved writing the printed (as on data set 6) pass summary on disk (data set 10) for use by some postNAP program, and also on data set 34, which is a printed pass summary. The second change involved plotting the measurement residuals in addition to giving the numerical values. The third change involved the computation of the correlation coefficient between the errors of the two measurements. The reason for computing the correlation coefficient was that when the plotting facility was added to this subroutine, it looked as if there was some correlation between the two measurement errors. However, in most cases the correlation coefficient is very small. The FORTRAN listing of the subroutine is given in Appendix A-3.5.1.

Special Subroutine RESID. The computed values of the error model terms are copied from disk (FT10F001) and written on tape (FT37F002). The measurement residuals are computed as before. However, since there now is only one measurement time point per pass, the standard deviation cannot be computed. Instead, the standard deviation computed in subroutine PRTIAL is copied from disk (FT36F001) as is the number of measurement points. This information is written on the same tape as the new values for the error model terms. Finally, the new observation tape is copied from disk (FT35F001) to tape (FT37F003). The FORTRAN listing is given in Appendix A-3.5.2.

- Changes to Subroutine MESOLD

Terms were added to Subroutine MESOLD to reflect the complete Minitrack geometrical error model. The following should be added to the NAP-II User's Guide (Reference 4) to be consistent with these changes (Appendix IV, Page IV-2).

ERROR MODEL TERM NO MEASUREMENT CODE		12	15	16
6			RE	RM
7		TM	RP	RL

where measurement code 6 corresponds to direction cosine alpha (or ℓ), and measurement code 7 corresponds to direction cosine beta (or m), and $n = \sqrt{1 - (\ell^2 + m^2)}$

The 12th error model term (TM) is not part of the geometrical error model but corresponds to a timing bias.

RE and RP are rotation terms about the local vertical of the equatorial and polar m measurements, respectively. RL and RM are rotations or tilt about the ℓ or m measurements.

2.4.3 The NAP-II Minitrack Post-Processing Program

The post-processing program summarizes the results of a NAP-II Minitrack run and prepares the NAP-II "input cards" for the next iteration. Any lobe assignment errors of the Minitrack preprocessor can also be corrected through the NAP-II "input cards".

In order to execute the post-processing program, the NAP-II program must be a version employing the special subroutine PRTIAL and RESID given in Appendix A-3.6 and 3.5.2, respectively.

The program assumes that the station numbers assigned by NAP are odd for equatorial stations and even for polar stations and that measurement numbers are odd for "L" measurements and even for "M" measurements. (See Appendix A-4.)

The NAP-II control cards must be in a particular order required by the POSTNAP program. In general, error model terms should be setup in order of totally stable, arc stable and pass stable. The error model parameter numbers (Category 601, Key 7), must be in ascending and consecutive order. Cards must not be repeated.

This is not a restriction on the NAP-II program but a restriction imposed by POSTNAP.

<u>Function</u>	<u>Unit</u>	<u>Description</u>		
Card Input	Data Set 5	Only one card required.		
	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>	
	1-5	IOPT	<p>Determines which NAP "701" (continuation 1) cards are to be output. If measurements were previously edited out of the solution and no value for the pass standard deviation is available, the measurements are edited out again. IOPT can assume values of 0, -1 and +1. In all three cases the above applies. In all cases key 7 of 701 card is set to "1".</p> <p>= 0, measurements are edited out if mean pass measurement error exceeds MAXERR or if pass standard deviation exceeds SDMAX. If measurements are edited out, DATA 2 of 701 card is set to 1.D15.</p> <p>= -1, measurements are edited out if mean pass measurement exceeds MAXERR or if no pass standard deviation is available or if pass standard deviation exceeds SDMAX. If measurements are edited, DATA 2 is set to 1.D15.</p> <p>= +1, same as -1 case except if measurements are not edited out, they are assigned "a priori" sigma of 10 times pass standard deviation. If measurements are edited out, DATA 2 is set to 1.D7 times the pass standard deviation.</p>	

<u>Function</u>	<u>Unit</u>	<u>Description</u>	
	<u>Card Column</u>	<u>Word</u>	<u>Definition</u>
	6-10	MAXERR	Maximum mean measurement error in Minitrack counts.
	11-20	SDMAX	Maximum pass standard deviation (unscaled).
	21-30	FREQCY	Satellite transmitter frequency in MHz.

Note on the availability of a Pass Standard Deviation.

A pass standard deviation can only be computed if there is more than one measurement per pass. If IOPT = 1, the pass standard deviation is saved on a "701" card. (If key 7 = 0, it is equal to DATA 2 times 1.D-1; if Key 7 = 1, it is equal to DATA 2 times 1.D-7). Use is made of this facility when the data processing switches from using all measurements for a pass to the single new measurement computed in special subroutine PRTIAL.

Note on data editing.

A bad pass is defined as one whose mean error exceeds MAXERR or whose standard deviation exceeds SDMAX. Bad passes are edited out of the solution in all cases. If no standard deviation is available, then in the case of Iopt = -1 the pass will be edited out of the solution. (It is recommended that Iopt = -1 only be used if there are more than one data point per pass. The non-availability of a pass standard deviation may in that case be the result of the pass not meeting the elevation requirements. NAP in that case would output a zero mean pass error).

Iopt = 1 should be used if the user wishes to weight the measurements of a pass in inverse proportion to their standard deviation, in other words, a noisy pass would be given less weight than one that is less noisy.

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Disk Input (on tape)	Data Set 27	NAP input cards used in making NAP run. This would normally be on a disk file created by the PRENAP card updating program.
Disk input (on tape)	Data Set 10, File 1 (FT10F001)	Output from NAP data set 37 (FT37F002). The computed values of error model parameters.
Disk input (on tape)	Data Set 10, File 2 (FT10F002)	Output from NAP data set 37 (FT37F001). Current measurement discrepancies.
Disk output (on tape)	Data Set 10, File 3 (FT10F003)	Output of sequenced NAP "input cards" for use by the PRENAP card updater program on the next iteration.
Printed output	Data Set 6	Prints the following <ul style="list-style-type: none"> • Some instructions on the use of the program. • Printout of input cards (data set 5). • Printout of NAP "output cards" (FT10F003) for the next iteration. The first column of this list are the sequence numbers.
Printed output	Data Set 20	The following is printed out for each station/pass. <ul style="list-style-type: none"> • Time of midpoint of pass. • Mean measurement error (This is the mean discrepancy computed in special subroutine PRTIAL and equals the mean residual error computed in subroutine RESID when the solution converges). • Standard deviation of the measurements for a pass. For only one measurement the standard deviation is equal to zero. • For each measurement, the time relative to midpoint and the error relative to mean pass error. This error is also plotted.
Printed Output	Data Set 31	Printout of the bias values used in the Minitrack preprocessor (built into the program) and the new bias. New biases are obtained by converting the bias obtained by NAP to Minitrack counts and adding the result to the preprocessor bias.

<u>Function</u>	<u>Unit</u>	<u>Description</u>
Printed output	Data Set 31-60	<p>A summary for each station is written on a different data set. Each pass contains</p> <ul style="list-style-type: none"> • Time of midpoint measurement • Arc number • Pass number • Mean error in Minitrack counts • Whether () or not (*) the measurement met elevation requirement given on NAP "702" card • Whether () or not (*) measurement contributed to present solution • Measurement standard deviation in Minitrack counts • Bias correction made to the measurement for the next iteration expressed in Minitrack lobes (in 1000 Minitrack counts). The errors being corrected are due to wrong lobe assignments in the Minitrack preprocessor and are corrected via NAP "704" cards • Number of measurement points per pass on the data tape • Number of measurement points deleted by special subroutine PRTIAL • The mean error rate • The reduction in standard deviation, expressed as a percentage, that would result if the standard deviation were computed about the line defined by the mean error and mean error rate and not the mean error alone • The computed measurement. The predicted (NAP) measurement plus the mean pass measurement error, (computed in special subroutine PRTIAL). • Whether () or not (*) the measurement will contribute to the solution of the next iteration.

2.5 RESULTS OF MINITRACK DATA REDUCTIONS USING NAP-II

2.5.1 Estimation of Calibration Parameters for the Fort Myers Minitrack Station Using the GEOS-I Satellite and Optically Determined Reference Arcs

A number of GEOS-A arcs determined from optical observations were used as reference arcs. These arcs had previously been obtained by DBA Systems, Inc. for work on another contract. Since optical observations are considerably more accurate than Minitrack, the optical reference arcs could be considered perfect. The NAP program was then used to recover measurement biases and measurement scale factor errors. The Minitrack measurements for each pass were weighted in inverse proportion to the variance of the measurement error for each pass (Minitrack message).

The results are shown in Tables 2 and 4. Tables 1 and 3 give the actual measurements. Table 5 is a comparison of calibration results. Table 6 tabulates some observed frequencies. It shows that the fluctuation in the GEOS-A transmitter frequency is very small. Table 7 shows the effect of including the Doppler effect and wave propagation time delay in the computations. The total effect can be seen to be of the order of 1 Minitrack count.

TABLE 1

POLAR ARRAY. Observed values of direction cosines, direction cosines rates and prepass internal bias (KS2).

ARC Number	ORBIT Number	DATE(1966)			GMT	Direction Cosines			Direction Cosine Rates			KS2 (l) - 067	KS2 (m) - 560
		MTH	DAY	HRS.		l	m	n	\dot{l}	\dot{m}	\dot{n}		
1	700	1	4	6	23	.84	.00	.55	.0009	-.0030	-.0014	0	0
2	712	1	5	6	27	.63	.01	.73	.0017	-.0037	-.0015	0	2
3	784	1	11	6	50	-.87	.00	.49	.0004	-.0031	.0007	2	14
5	831	1	15	5	4	-.21	.00	.98	.0026	-.0047	.0006	2	0
7	843	1	16	5	7	-.52	.00	.85	.0017	-.0043	.0010	2	4
9	855	1	17	5	11	-.72	.00	.69	.0009	-.0037	.0010	0	1
10	866	1	18	3	14	.86	.07	.51	.0010	-.0027	-.0013	2	2
11	867	1	18	5	16	-.84	.00	.54	.0005	-.0032	.0008	3	2
12	914	1	22	3	30	-.10	.00	.99	.0027	-.0046	.0003	2	8
15	938	1	24	3	37	-.67	.00	.74	.0011	-.0038	.0010	2	0
16	949	1	25	1	40	.90	.00	.44	.0006	-.0024	-.0013	3	0
17	961	1	26	1	44	.80	.01	.61	.0011	-.0029	-.0014	1	-1
18	1080	2	5	0	20	.11	.00	.99	.0027	-.0043	-.0003	2	10
19	1092	2	6	0	25	-.25	.00	.97	.0023	-.0043	.0006	4	3
20	1408	3	4	9	19	-.43	.00	.90	.0012	.0022	.0006	6	-41
21	1479	3	10	7	40	-.13	.00	.99	.0014	.0024	.0002	4	-51
22	1680	3	27	2	40	.76	-.12	.64	.0005	.0021	-.0003	16	14
23	1681	3	27	4	41	-.63	.00	.77	.0010	.0020	.0008	16	14
24	1740	4	1	3	0	-.15	.00	.99	.0015	.0025	.0002	18	15
25	1752	4	2	3	3	-.38	.02	.93	.0014	-.0023	.0005	18	15

TABLE 2

POLAR ARRAY. Measurement Errors.

ARC No.	Standard Deviation Of Measurement Error About Mean For Pass		Mean Measurement Error For Pass		MINITRACK COUNTS	
	σ_l	σ_m	Δl	Δm	Δl	Δm
1	.000072	.000147	-.000001	-.000135	0	-8
2	.000036	.000034	-.000038	-.000097	-2	-6
3	.000749	.000660	-.000164	-.000034	-9	-2
5	.000068	.000072	.000027	.000085	2	5
7	.000040	.000063	.000009	.000033	1	2
9	.000044	.000056	.000116	-.000005	7	0
10	.000239	.000141	-.000042	-.000023	-2	-1
11	.000261	.000353	.000033	-.000057	2	-3
12	.000044	.000032	.000155	-.000068	9	-4
15	.000071	.000081	.000048	.000125	3	7
16	.000133	.000173	.000112	.000029	6	2
17	.000042	.000048	.000011	.000005	1	0
18	.000035	.000034	.000003	.000098	0	6
19	.000044	.000057	-.000057	.000136	-3	8
20	*	.000038	*	.000036	*	2
21	.000052	.000048	.000087	.000047	5	3
22	.000085	.000092	.000130	.000118	7	7
23	.000029	.000032	.000003	.000018	0	1
24	.000039	.000034	-.000046	-.000005	-3	0
25	.000021	.000028	-.000062	-.000066	-4	-4

EW - BIAS: 137 MINICTS - .000021 = 136 MINICTS

NS - BIAS: 431 MINICTS + .000071 = 435 MINICTS

EW - SCALE FACTOR: -.00022

(Base Line is Shorter Than Assumed.)

TABLE 3

EQUATORIAL ARRAY. Observed values of direction cosines,
direction cosine rates and prepass internal bias (KS2).

ARC Number	ORBIT No.	DATE(1966)		GMT		Direction Cosines			Direction Cosine Rates			KS2 (l) - 067	KS2 (m) - 560
		MTH	DAY	HRS.	MIN.	l	m	n	\dot{l}	\dot{m}	\dot{n}		
1	700	1	4	6	18	.00	.88	.48	.0020	-.0007	.0013	-1	0
2	712	1	5	6	23	.00	.78	.62	.0022	-.0013	.0017	-1	2
4	819	1	14	4	59	.00	.26	.97	.0028	-.0042	.0011	-2	11
13	926	1	23	3	36	-.04	-.65	.76	.0023	-.0027	-.0022	4	-1
15	938	1	24	3	43	-.03	-.90	.43	.0016	-.0009	-.0018	2	0
17	961	1	26	1	38	.00	.85	.53	.0019	-.0008	.0013	1	-1
20	1408	3	4	9	23	.00	.57	.82	.0014	.0014	-.0010	6	-42
21	1479	3	10	7	42	.01	.21	.98	.0014	.0022	-.0005	5	-51
23	1681	3	27	4	48	.00	.73	.68	.0013	.0009	-.0010	16	14
25	1752	4	2	3	7	.00	.52	.85	.0014	.0016	-.0010	18	15

TABLE 4

EQUATORIAL ARRAY. Measurement Errors.

ARC No.	Standard Deviation Of Measurement Error About Mean For Pass		Mean Measurement Error For Pass		MINITRACK COUNTS	
	σl	σm	Δl	Δm	Δl	Δm
1	.000191	.000213	.000151	-.000080	7	-4
2	.000081	.000053	-.000013	-.000050	-1	-2
4	.000033	.000040	.000062	.000025	3	1
13	.000189	*	.000157	*	7	*
15	.000657	.000757	.000192	-.000397	9	-18
17	.000088	.000076	.000056	.000006	3	0
20	*	.000041	*	-.000007	*	0
21	.000031	.000041	-.000054	-.000040	-2	-2
23	.000071	.000043	.000113	.000012	5	1
25	.000034	.000039	-.000045	.000038	-2	2

EW - BIAS: 957 MINICTS + .000026 = 958 MINICTS

NS - BIAS: 988 MINICTS - .000544 = 988 MINICTS

NS - SCALE FACTOR: -.00049

(Base line is shorter than assumed.)

TABLE 5
COMPARISON OF CALIBRATION RESULTS

Source	DBA*	RCA**	Aircraft Calibration			Actual Values Used	
			July 1965	5 Nov 1965	3 Mar. 1966	5 Nov 1965	3 Mar. 1966
Equatorial Array							
EW - BIAS	958	956	956	957	969	954	959
NS - BIAS	988	985	988	992	988	988	988
Polar Array							
EW - BIAS	136	136	137	140	153	138	143
NS - BIAS	435	437	431	435	433	435	433
Equatorial Array NS - Scale Factor	-.00049	-.00015					
Polar Array EW - Scale Factor	-.00022	-.00022					

* The DBA computed calibration values are the ones shown in Tables I and II. They are based on observations from 4 January to 2 April 1966.

** The RCA results have been verbally communicated by Mr. Jerry Casto and are based on satellite observations covering approximately the same time period as those used by DBA.

TABLE 6

OBSERVED GEOS - A FREQUENCIES

(Source: Harry Pritchard, GSFC)

Date (1966)	Value (MHz)	Scale Error Relative To Nominal Value (136.83 MHz)
1 January	136.830360	26×10^{-7}
5 January	136.830350	26×10^{-7}
3 February	136.830038	3×10^{-7}
8 February	136.829675	-24×10^{-7}
17 March	136.830540	40×10^{-7}

TABLE 7

CHANGE IN PREDICTED MEASUREMENTS DUE TO INCLUSION OF
THE DOPPLER EFFECT AND WAVE PROPAGATION TIME DELAY

POLAR ARRAY			EQUATORIAL ARRAY		
ARC No.	$10^5 \Delta I$	$10^6 \Delta m$	ARC No.	$10^5 \Delta I$	$10^6 \Delta m$
1	-14	19	1	-15	17
2	-14	20	2	-15	18
3	-10	21	4	-13	20
5	-12	21	13	-11	x
7	-11	21	15	-11	21
9	-11	21	17	-14	18
10	-14	18	20	x	-17
11	-10	21	21	-11	-18
12	-12	20	23	-13	-16
15	-11	21	25	-12	-17
16	-14	18			
17	-14	19			
18	-13	20			
19	-11	20			
20	x	-18			
21	-11	-18			
22	- 8	-20			
23	-12	-17			
24	-11	-18			
25	-11	-17			

POLAR ARRAY: 1 MINITRACK Count = .0000175

EQUATORIAL ARRAY: 1 MINITRACK Count = .0000216

2.5.2 The Calibration of all Minitrack Stations Using GEOS-A Minitrack Measurements

The procedures followed in processing the Minitrack data are described in Section 2.6 of this report. The four arcs described in Table 15 were at first processed separately. A new data tape was created for each of the four arcs (see special subroutines PRTIAL and RESID). The arcs were then combined in pairs to give two, two-arc runs, and finally all the data were combined into a single four-arc run. Three sets of runs were made under slightly varying conditions (see Table 15): In the first run scale factors and antenna rotation terms were recovered in addition to measurement biases and the four state vectors. The second run was similar to the first except that no rotation terms were considered. This resulted in very slight differences in the solutions. The third run was similar to the first but in this run ionospheric corrections were made using the ionospheric model developed by DBA under Contract NAS511730. In all runs, data were edited out of the solution using the criteria listed in Tables 12 and 13. It should be mentioned that when the runs were made, no ionospheric data could be obtained for 1966. The 1971 values were therefore substituted. This may account for the relatively bad results obtained for run 3. Tables 8 through 14 refer to run 1. Table 8 is a comparison of calibration results. Table 9 lists the scale factor errors and antenna alignment errors. It can be seen that the scale errors are predominantly negative. This is the kind of effect that would be expected if no ionospheric corrections were made, i.e., it seems likely that the scale factors have absorbed some of the effect of ionospheric refraction. When ionospheric corrections were made (run 3), the recovered scale factors were indeed reduced in magnitude (the actual numbers are not included in this report).

Table 10 is a listing of the number of observations for each station. Table 11 gives the RMS values of the observed residuals. It is interesting to note that the Polar Array, which has a larger baseline, shows a larger RMS error than the Equatorial Array when the errors are expressed in Minitrack counts, but more or less the same RMS error in terms of angular error. From this, it could be inferred that the errors are caused less by the electronics of the observing stations, which measures Minitrack counts, than

by general uncertainties in conditions outside the observing station. This, in general, is probably true. However, it has been observed that large variations in the pre-calibration biases, which is part of the Minitrack message, have been accompanied by large residuals in the orbital fit. The Woomera Polar Station was particularly bad in this report. The measurement residuals and precalibration constants for that station are listed in Table 14 for illustrative purposes. Tables 12 and 13 are self-explanatory, as are Tables 15.1 through 15.4. It should be emphasized that the results given in Tables 15 are the most important results of this report.

In all orbital computations the Earth model used was that given in Appendix A-1. The affect of solar radiation pressure was not taken into account, and neither was the effect of the Earth's precession and nutation.

In all three runs the measurements were weighted proportionately to the standard deviation of the measurements within each message.

TABLE 8
Comparison of Calibration Results for
Equatorial and Polar Station Biases

Station	This Program *		Aircraft 65.12.31		Aircraft 66.02.25	
	EW	NS	EW	NS	EW	NS
Fort Myers (E)	956	981	954	988	953	984
Fort Myers (P)	135	435	138	435	137	435
Quito (E)	817	036	812	036	837	030
Quito (P)	756	000	760	002	763	006
Lima (E)	949	252	955	263	955	259
Lima (P)	023	881	028	882	028	882
Santiago (E)	078	057	073	060	076	059
Santiago (P)	950	972	943	967	943	963
New Foundland (E)	930	937	934	935	934	935
New Foundland (P)	170	920	171	919	171	919
Winkfield (E)	071	973	067	976	067	976
Winkfield (P)	868	001	870	011	870	011
Johannesburg (E)	048	937	054	932	054	932
Johannesburg (P)	084	876	090	871	090	871
Blossom Point (E)	948	094	948	096	948	096
Blossom Point (P)	081	887	082	889	082	889
College (E)	955	807	961	804	960	804
College (P)	846	932	854	916	859	919
Mojave (E)	030	576	017	579	029	575
Mojave (P)	079	123	062	129	079	121
Grand Forks (E)	068	951	060	954	061	951
Grand Forks (P)	602	001	598	990	598	990
Woomera (E)	020	944	031	938	031	938
Woomera (P)	934	118	948	118	948	118

* Time span covered was 66.1.1 - 66.2.3 and 66.3.12 - 66.3.19.

Table 9

Scale Factor Errors and Antenna Alignment Errors in Minitrack Counts

1000 Equatorial Minitrack Counts = .0216 radians

1000 Polar Minitrack Counts = .0174 radians

	<u>Equatorial Array</u>		<u>Polar Array</u>	
	<u>Scale Error</u>	<u>Antenna Rotation</u>	<u>Scale Error</u>	<u>Antenna Rotation</u>
Fort Myers	-14	4	-15	2
Quito	9	-4	- 6	-2
Lima	-24	-4	30	-3
Santiago	- 2	-8	- 8	-2
New Foundland	- 8	0	-13	-2
Winkfield	- 4	-3	- 8	5
Johannesburg	- 6	-1	-14	-4
Blossom Point	-11	6	- 1	0
College	-10	8	- 4	0
Mojave	- 3	-3	- 7	4
Grand Forks	8	-5	- 8	-9
Woomera	-11	-3	- 8	-4

Scale Error

The predicted measurement is in error by an amount equal to the "scale error" multiplied by the actual measurement.

Antenna Rotation

The predicted measurement is in error because the antenna baselines are rotated anti-clockwise by the "antenna rotation".

In the equatorial mode the scale error only affects the m measurement and the antenna rotation only the l measurement.

In the polar mode the scale error only affects the l measurement and the antenna rotation only the m measurement.

Table 10

The Number of Minitrack Messages Used in the Orbit Determination
and the Determination of Biases, Scale Factors and Antenna Rotations

<u>Equatorial</u> <u>Array</u>	<u>Direction Cosine l</u>					<u>Direction Cosine m</u>				
	<u>Arc 1</u>	<u>Arc 2</u>	<u>Arc 3</u>	<u>Arc 4</u>	<u>Total</u>	<u>Arc 1</u>	<u>Arc 2</u>	<u>Arc 3</u>	<u>Arc 4</u>	<u>Total</u>
Fort Myers	4	4	11	12	31	4	4	11	12	31
Quito	1	-	2	4	7	1	-	-	3	4
Lima	-	3	-	2	5	-	3	2	-	5
Santiago	1	1	3	3	8	1	1	3	3	8
New Foundland	17	19	26	31	93	16	19	26	31	92
Winkfield	12	-	9	11	32	12	-	15	11	38
Johannesburg	-	1	3	2	6	-	1	3	2	6
Blossom Point	12	9	20	16	57	12	9	21	16	58
College	12	12	18	17	59	13	12	17	17	59
Mojave	12	11	17	14	54	12	11	17	14	54
Grand Forks	11	14	22	7	54	12	14	22	7	55
Woomera	<u>1</u>	<u>-</u>	<u>1</u>	<u>3</u>	<u>5</u>	<u>-</u>	<u>-</u>	<u>2</u>	<u>3</u>	<u>5</u>
Total	83	74	132	122	411	83	74	139	119	415

Table 10 (Continued)

The Number of Minitrack Messages Used in the Orbit Determination
and the Determination of Biases, Scale Factors and Antenna Rotations

<u>Polar Array</u>	<u>Direction Cosine l</u>					<u>Direction Cosine m</u>				
	<u>Arc 1</u>	<u>Arc 2</u>	<u>Arc 3</u>	<u>Arc 4</u>	<u>Total</u>	<u>Arc 1</u>	<u>Arc 2</u>	<u>Arc 3</u>	<u>Arc 4</u>	<u>Total</u>
Fort Myers	11	9	14	19	53	10	9	14	19	52
Quito	4	3	5	5	17	4	4	5	5	18
Lima	5	5	5	4	19	5	6	6	6	21
Santiago	4	2	5	5	16	4	3	5	4	16
New Foundland	9	14	14	17	54	9	14	14	18	55
Winkfield	3	-	2	3	8	3	-	2	2	7
Johannesburg	2	3	7	7	19	2	3	7	8	20
Blossom Point	13	9	15	20	57	12	9	15	20	58
College	7	5	9	8	29	7	6	9	7	29
Mojave	14	11	13	20	58	14	11	13	20	58
Grand Forks	4	7	18	10	39	4	7	18	10	39
Woomera	<u>4</u>	<u>2</u>	<u>3</u>	<u>7</u>	<u>16</u>	<u>3</u>	<u>3</u>	<u>5</u>	<u>7</u>	<u>18</u>
Total	80	71	110	125	385	77	75	112	124	389

Table 11
RMS Value of Residuals* in Minitrack Counts

<u>Station</u>	<u>Equatorial Array</u>		<u>Polar Array</u>	
	<u>l</u>	<u>m</u>	<u>l</u>	<u>m</u>
Fort Myers	2.7	5.6	5.1	4.5
Quito	3.2	8.9	7.4	5.2
Lima	3.7	9.3	6.6	5.7
Santiago	4.7	3.8	7.2	7.0
New Foundland	4.9	3.3	7.1	5.3
Winkfield	7.3	3.5	4.5	5.4
Johannesburg	3.6	2.8	4.5	4.0
Blossom Point	4.8	3.4	4.8	3.2
College	3.7	5.9	5.8	8.4
Mojave	3.1	5.3	5.2	5.1
Grand Forks	4.9	4.2	6.0	7.1
Woomera	<u>4.1</u>	<u>11.8</u>	<u>7.2</u>	<u>8.1</u>
All **	4.3	4.7	5.9	5.6

*The residuals are the differences between observed and predicted values.
The predicted values are based on the computed orbit.

**It is of interest to note that the four RMS residuals for all stations expressed as unscaled quantities assume the values:

.000093, .000102, .000102, .00097.

The same residuals expressed as equivalent angular discrepancies at zenith assume the values: 19", 21", 21", 20", i.e., values around the quoted Minitrack accuracy of 20".

Table 12

Total Number of Minitrack Messages
and the Number of Rejected Messages

<u>Equatorial Array</u>	<u>Total</u>	<u>Rejected</u>	<u>Direction Cosine l</u>		<u>Direction Cosine m</u>	
	<u>Number</u>		<u>Rejected</u>	<u>Rejected</u>	<u>Rejected</u>	<u>Rejected</u>
	<u>Messages</u>	<u>(Elevation)</u>	<u>(Discrepancy)</u>	<u>(S.D.)</u>	<u>(Discrepancy)</u>	<u>(S.D.)</u>
Fort Myers	52	20		1		1
Quito	7				3	
Lima	5					
Santiago	9		1			1
New Foundland	99	5	1		3	
Winkfield	41		9		3	
Johannesburg	6					
Blossom Point	73	15	1			
College	69	6	3	1	3	1
Mojave	79	25				
Grand Forks	59	4	1			
Woomera	<u>6</u>	<u> </u>	<u>1</u>	<u> </u>	<u>1</u>	<u> </u>
Total	505	75	17	2	12	3

Rejection Criteria

Elevation. All messages the mean elevation of which was below 25° .

Discrepancy. All direction cosines having a residual error in excess of 20 Minitrack Counts.

S.D. All direction cosines having an error with a standard deviation in excess of 0.00050, the computed standard deviation being based on all measurements within a Minitrack message.

Rejected measurements are only listed under one heading even if they should have been rejected for more than one reason. Thus, the total number of measurements less the number of rejected measurements equals the number of measurements used in the computations (Table 3).

Table 12 (Continued)

Total Number of Minitrack Messages
and the Number of Rejected Messages

<u>Polar Array</u>	<u>Total Number Messages</u>	<u>Rejected Elevation</u>	<u>Direction Cosine l Rejected Discrepancy</u>	<u>Direction Cosine l Rejected (S.D.)</u>	<u>Direction Cosine m Rejected Discrepancy</u>	<u>Direction Cosine m Rejected (S.D.)</u>
Fort Myers	72	18		1		2
Quito	19		1	1	1	
Lima	21			2		
Santiago	22	1	4	1	3	2
New Foundland	74	19	1			
Winkfield	8				1	
Johannesburg	20		1			
Blossom Point	82	24	1		2	
College	76	40	1	6	1	6
Mojave	70	10	1	1	1	1
Grand Forks	51	11	1			1
Woomera	<u>20</u>	<u>—</u>	<u>4</u>	<u>—</u>	<u>2</u>	<u>—</u>
Total	535	123	15	12	11	12

Rejection Criteria

Elevation. All messages the mean elevation of which was below 25° .

Discrepancy. All direction cosines having a residual error in excess of 20 Minitrack Counts.

S.D. All direction cosines having an error with a standard deviation in excess of 0.00050, the computed standard deviation being based on all measurements within a Minitrack message.

Rejected measurements are only listed under one heading even if they should have been rejected for more than one reason. Thus, the total number of measurements less the number of rejected measurements equals the number of measurements used in the computations (Table 3).

Table 13

Total Number of Measurements and Number of Rejected Messages

	Total Measurements	Rejected (Elevation)	Rejected (Discrepancy)	Rejected (S.D.)	Used In Computation
Number	2080	396	55	29	1600
Percent	100	19.0	2.6	1.4	77.0

Rejection Criteria

Elevation. All measurements at a mean elevation below 25° .

Discrepancy All measurements having a residual error in excess of 20
Minitrack Counts

S.D. All measurements having an error with a standard deviation in
excess of 0.00050, the computed standard deviation being based
on all measurements within a Minitrack message.

Rejected measurements are only listed under one heading even if
they should have been rejected for more than one reason.

Table 14
Residual Measurement Errors and Prepass Calibration Constants
for the Woomera Polar Station

<u>Arc</u>	<u>Date</u>	<u>Time (hrs)</u>	<u>Residual Measurement</u>		<u>KC-KS1 + KS2</u>	
			<u>l</u>	<u>Error</u> <u>m</u>	<u>l</u>	<u>m</u>
1	1.2.66	5.2	11	3	345	557
1	1.3.66	18.7	-10	5	344	545
1	1.4.66	18.8	- 2	30	343	551
1	1.5.66	18.8	0	5	342	570
2	1.11.66	17.2	- 9	-14	345	584
2	1.12.66	17.2	5	- 8	343	584
2	1.13.66	17.3	31	-16	305	576
3	1.28.66	14.2	65	7	152	546
3	1.28.66	22.8	98	- 2	124	544
3	1.29.66	14.3	-34	65	224	545
3	1.29.66	22.9	-16	12	222	541
3	1.30.66	22.9	3	4	221	540
3	2.3.66	12.6	14	10	160	541
4	3.12.66	4.8	1	-11	561	719
4	3.12.66	13.4	- 4	0	561	717
4	3.13.66	4.9	0	- 1	560	717
4	3.13.66	13.5	4	- 5	560	717
4	3.15.66	13.6	0	- 1	560	717
4	3.16.66	13.7	- 2	1	561	713
4	3.19.66	3.3	2	-12	563	716

Table 15.1

Comparison of a GEOS-A Arc Determined from Minitrack Data with an Orbit
Determined from Optical Data

Start Time 1.1.66 6 hours
 Stop Time 1.5.66 19 hours
 Length of Arc 4.5 days

	Run 1	Run 2	Run 3
RMS Position Difference (m)	67	69	149
RMS Velocity Difference (m/sec)	.044	.046	0.100
Maximum Position Difference (m)	103	122	237
Maximum Velocity Difference (m/sec)	.063	.074	0.140

- Run 1. Minitrack orbit with measurement bias, scale factor, and rotation recovery. No ionospheric corrections.
- Run 2. Minitrack orbit with measurement bias and scale factor recovery. No ionospheric corrections.
- Run 3. Minitrack orbit with measurement bias, scale factor, and rotation recovery. Ionospheric corrections.

It is of interest to compare the above results with those quoted in "Intercomparison of the Minitrack and Optical Tracking Networks using GEOS-I Long Arc Orbital Solutions" (by J.G. Marsh, C.E. Doll, R.J. Sandifer and W.A. Taylor, NASA-TND-5337, February 1970). For an arc covering almost the identical period, they obtained an RMS position difference of 165 meters in a similar comparison. However, they did not attempt to recover any station calibration parameters. They made no ionospheric corrections.

Table 15.2

Comparison of a GEOS-A Arc Determined from Minitrack Data with an Orbit

Determined from Optical Data

Start Time 1.8.66 0 hours

Stop Time 1.14.66 5 hours

Length of Arc 6.2 days

	Run 1	Run 2	Run 3
RMS Position Difference (m)	86	116	160
RMS Velocity Difference (m/sec)	.075	.099	.127
Maximum Position Difference (m)	127	180	262
Maximum Velocity Difference (m/sec)	.120	.158	.180

Run 1. Minitrack orbit with measurement bias, scale factor, and rotation recovery. No ionospheric corrections.

Run 2. Minitrack orbit with measurement bias and scale factor recovery. No ionospheric corrections.

Run 3. Minitrack orbit with measurement bias, scale factor, and rotation recovery. Ionospheric corrections.

Table 15.3

Comparison of a GEOS-A Arc Determined from Minitrack Data with an OrbitDetermined from Optical Data

Start Time 1.28.66 2 hours
 Stop Time 2.4.66 0 hours
 Length of Arc 6.9 days

	Run 1	Run 2	Run 3
RMS Position Difference (m)	124	114	182
RMS Velocity Difference (m/sec)	.103	.099	.155
Maximum Position Difference (m)	194	181	272
Maximum Velocity Difference (m/sec)	.155	.153	.231

- Run 1. Minitrack orbit with measurement bias, scale factor, and rotation recovery. No ionospheric corrections.
- Run 2. Minitrack orbit with measurement bias and scale factor recovery. No ionospheric corrections.
- Run 3. Minitrack orbit with measurement bias, scale factor, and rotation recovery. Ionospheric corrections.

Table 15.4

Comparison of a GEOS-A Arc Determined from Minitrack Data with an Orbit
Determined from Optical Data

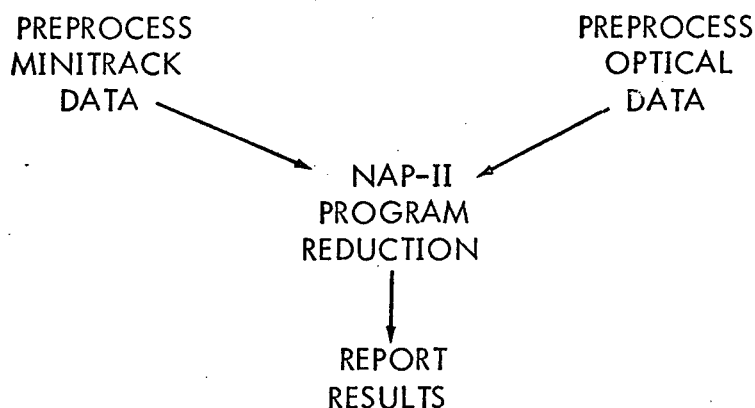
Start Time	3.12.66	3 hours			
Stop Time	3.19.66	20 hours			
Length of Arc	7.6 days				
			Run 1	Run 2	Run 3
RMS Position Difference (m)			168	179	249
RMS Velocity Difference (m/sec)			.142	.152	.207
Maximum Position Difference (m)			251	250	406
Maximum Velocity Difference (m /sec)			.207	.215	.315

- Run 1. Minitrack orbit with measurement bias, scale factor, and rotation recovery. No ionospheric corrections.
- Run 2. Minitrack orbit with measurement bias and scale factor recovery. No ionospheric corrections.
- Run 3. Minitrack orbit with measurement bias, scale factor, and rotation recovery. Ionospheric corrections.

2.6 RECOMMENDED PROCEDURE FOR REDUCING MINITRACK DATA

2.6.1 Reduction Procedure

The purpose of this section is to provide a step-by-step procedure to be followed for the reduction of Minitrack data and optical data. This procedure can be simplified into three or four parts.



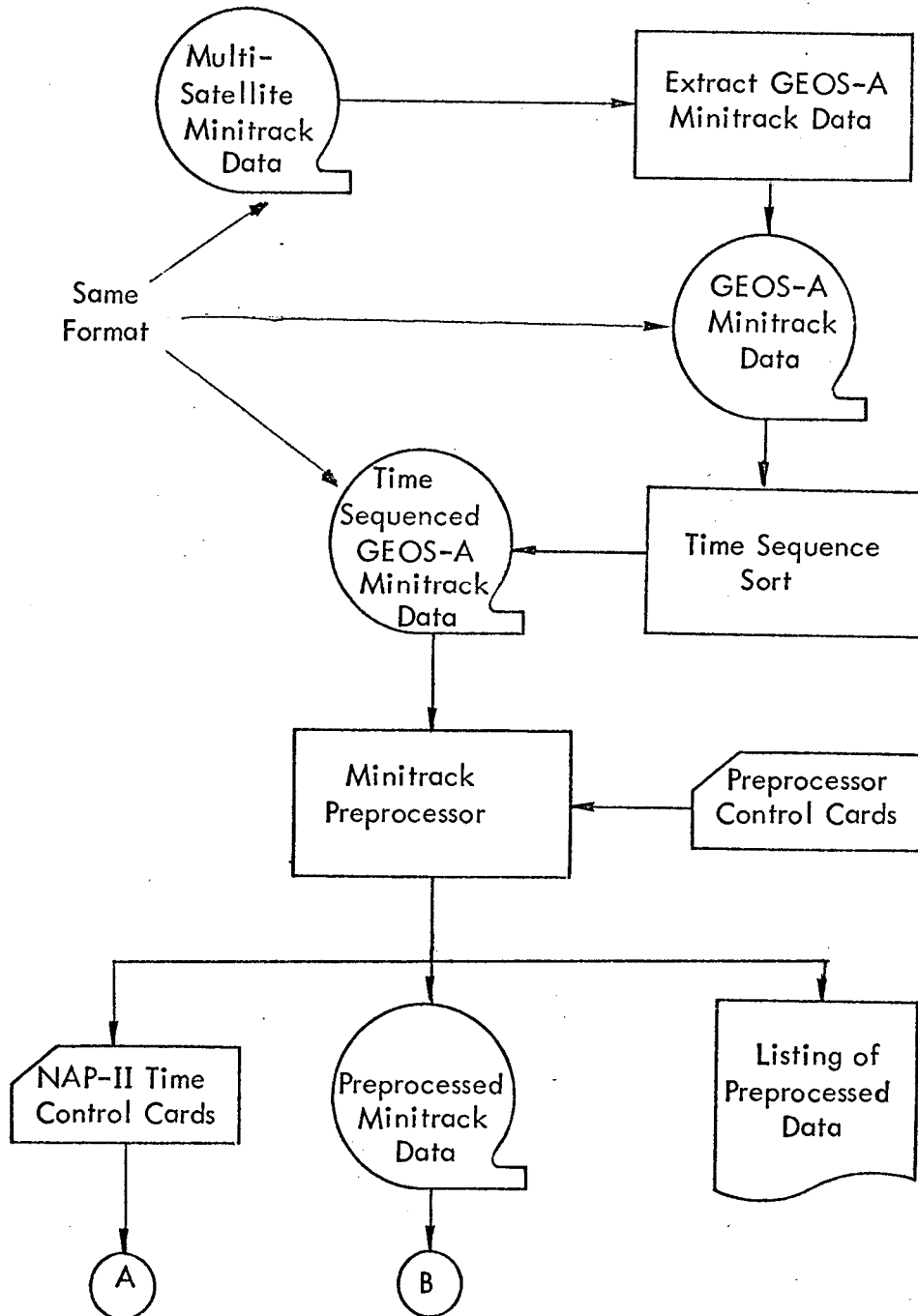
The preprocessing of the Minitrack data and the Optical data can be done as a series or parallel effort. The same applies to the NAP-II reduction of the data.

The steps to a complete reduction of the Minitrack data are:

1. Extract desired data from Minitrack and/or Optical data tapes.
 2. Sort Minitrack messages in time sequence (not required for Optical data when GEOS formatted data tapes are used).
 3. Preprocess Minitrack and/or Optical data.
 4. Set up NAP-II control cards and write cards on magnetic tape.
 5. Make PRENAP card updater run.
 6. NAP-II program execution.
 7. POSTNAP program execution.
 8. Report results after reduction has converged.
- } Iterate on these 3 steps until convergence achieved

A flow diagram for the preprocessing of the Minitrack data is given in Figure 1. Note: In setting up these runs, refer to Appendix A-4 for restriction place on card set-up.

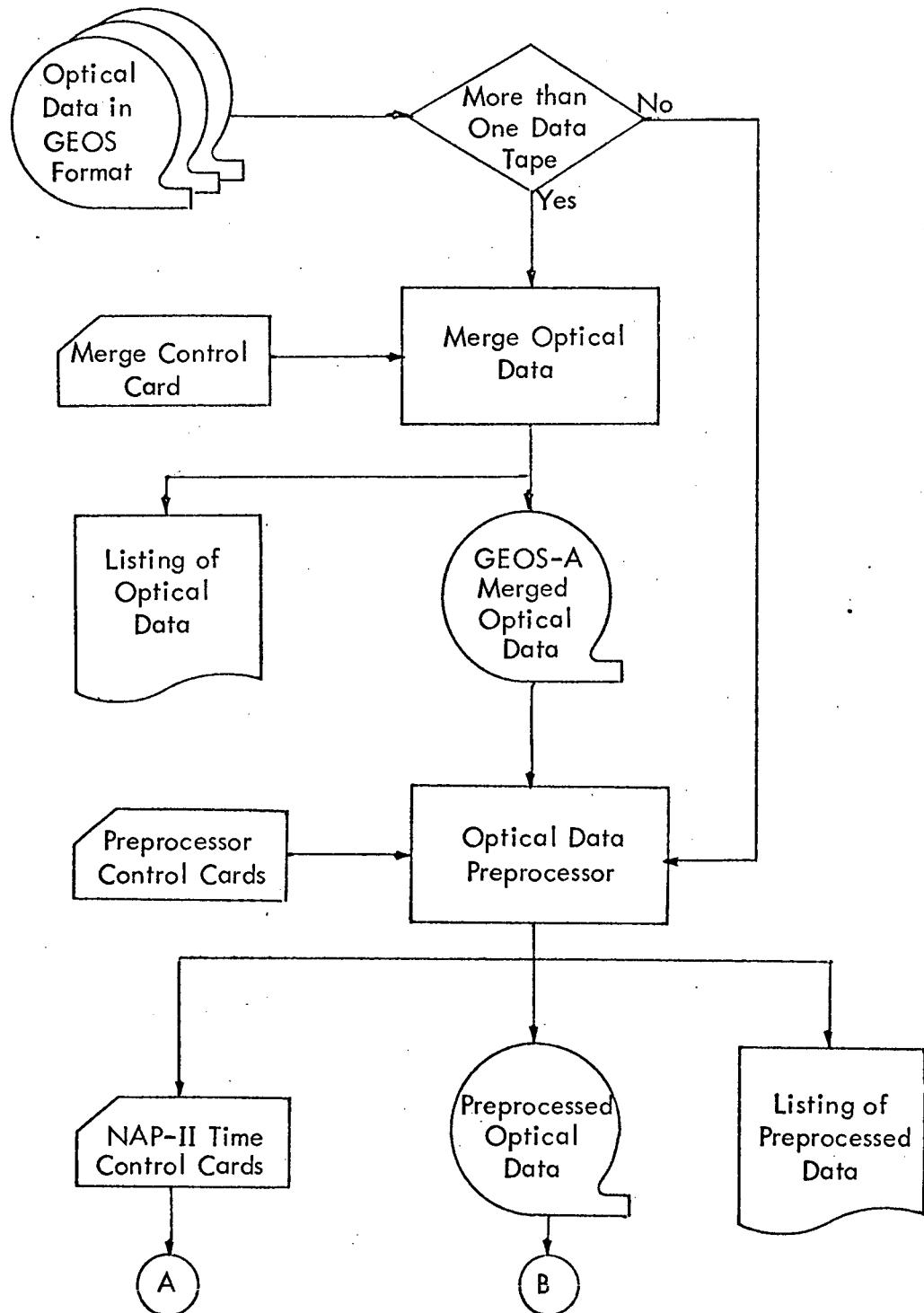
FIGURE 1
MINITRACK PREPROCESSING



The process starts with a magnetic tape containing Minitrack messages from several satellites. This tape is input to a program to extract just the messages from GEOS-1 satellite and writes them on another magnetic tape in the same format. This tape is then input to a program that sorts the messages, and also edits duplicate messages and puts them in time sequence on magnetic tape. This tape is now in the right form for the preprocessor program. The time-sequenced data tape, along with preprocessor control cards, are now input to the Minitrack preprocessor program. The preprocessor makes known corrections to the data and converts the corrected phase differences to direction cosines. The program outputs a data tape in a format acceptable to NAP-II and also a listing of the corrected data. The preprocessor also outputs a bulk of the NAP-II control cards dealing with the station times for the data (Category 201, 202, and 999). These are used in selection of data to be processed. This ends the pre-processing phase of the procedure. The preprocessing of Minitrack data is discussed in Section 2.2 of this report.

Figure 2 is a flow diagram of the preprocessing of optical data. The data input to the Optical preprocessing program must be in time sequence. If there are more than one tracking systems data to be processed, the data tapes must be "merged" onto one data tape. The output from the merge program is a data tape, in GEOS format, and a listing of the data. This data tape is input to the Optical preprocessor with control cards that specify the stations and times of the data to be processed. In the case of the SAO stations, these cards are also used to correct the observation times from A.1 to UTC. The Optical preprocessor outputs a data tape in a format acceptable to NAP-II and punched cards used in NAP-II to control data times. There is also a printed output of the reformatted and corrected data. The optical data preprocessing is discussed in Section 2.3 of this report.

FIGURE 2
OPTICAL PREPROCESSING



Once the data has been preprocessed, it is ready to be reduced using the NAP-II program. This process is flowed in Figure 3. The first step is to set up the NAP-II control cards as specified by the NAP-II User's Guide. The timing cards (Category 201, 202, and 999) are output as a result of the preprocessor. After the cards are set up, they are written on magnetic tape, for ease of handling. The cards on tape can be changed via the PRENAP card updater. This program is discussed in Section 2.4.1 of this report.

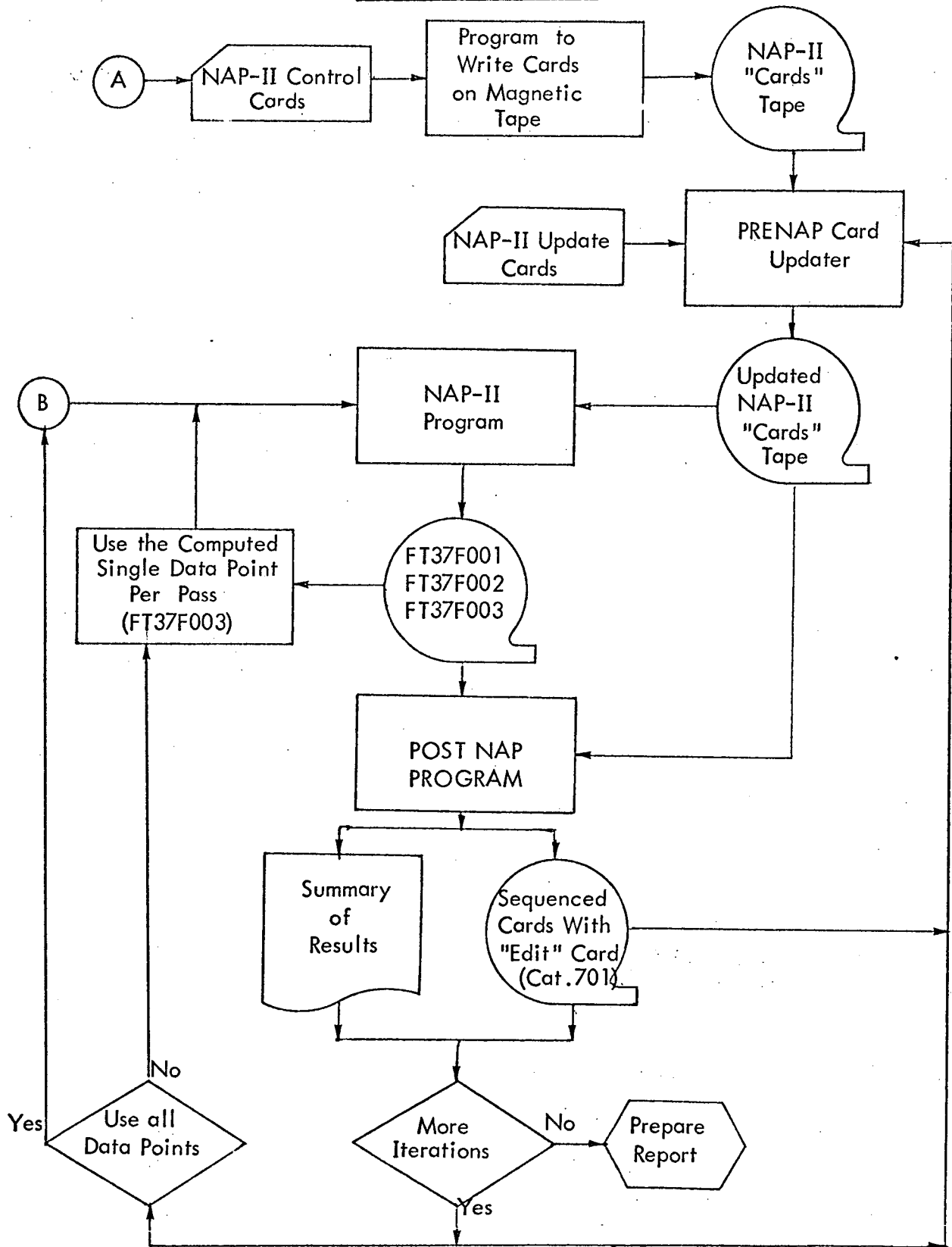
The NAP-II control cards (now on tape) and the data tape output from the preprocessor are now input to the NAP-II program. At the end of each iteration, NAP-II outputs a disk file (on tape) with the current values of the error model parameters and the measurement discrepancies. Also output is a "single point" data tape which can be used on successive iterations to reduce the computation time. When using the "single point" data tape for Minitrack data, delete the Category 704 cards.

The output from the NAP-II program is then input to the POSTNAP program which, in effect, gives a status report of the reduction and prepares information for the next iteration.

The PRENAP, NAP, POSTNAP sequence is continued until the solution has converged.

FIGURE 3

NAP-II REDUCTION



C.5

2.6.2 Recommended Error Model

The results of this study indicate the following error models to be sufficient for reducing Minitrack data.

The error model terms to be used are dependent on whether the data was collected in the equatorial or polar modes.

EQUATORIAL ARRAY

$$l = l_0 + b_1 + r_e m_0 + \tau \dot{l}$$

$$m = m_0 + b_2 + s_e m_0 + \tau \dot{m}$$

POLAR ARRAY

$$l = l_0 + b_3 + s_p l_0 + \tau \dot{l}$$

$$m = m_0 + b_4 + r_p l_0 + \tau \dot{m}$$

where,

l_0 and m_0 are Minitrack measurements in
Minitrack counts/1000.

b_1, b_2, b_3 and b_4 are zero-set biases

r_e and r_p are rotation terms about the local vertical
of equatorial l and polar m measurements
respectively

s_e and s_p are scale factors of equatorial m and polar l
measurements respectively

τ is the timing error associated with the station

\dot{l} and \dot{m} are computed rates obtained from the orbital
equations within NAP-II

These error model terms are coded for input to NAP-II (see Reference 4,
The NAP-II User's Guide, Appendix IV-B).

The error model terms would correspond to the following term numbers for direction cosine data types (measurement code 6 and 7).

<u>Error Model Term</u>	<u>Error Model Term No.</u>
b_1, b_2, b_3, b_4	10
r_e and r_p	15 (see changes to MESOLD in Section 2.4.2)
s_e and s_p	14
τ	11

Note: Consult NAP-II User's Guide, Appendix IV-2.

2.6.3 Typical Set-up for NAP-II Program

The following is an example of a set of NAP-II control cards. This listing is output from the NAP-II program on each run.

Note that each station is defined twice (category 301, 302, and 303); once for the equatorial array and once for the polar array. Following the survey cards are the error model cards (category 601). For ease of recognition, the labels have been coded as to which term it is, i.e. FTMYRELB is the FTMYR station equatorial " λ " measurement zero-set bias "B". FTMYRPLB is the polar " λ " measurement bias. Other codes used are "ELS" and "PLS" for equatorial " λ " scale and polar " λ " scale, "ELR" and "PLR" for equatorial " λ " rotation and polar " λ " rotation.

It is recommended that a new user of NAP-II take the following listing and, using the NAP-II User's Guide, cross-reference the codes used in the listing to their meaning given in the User's Guide.

See Appendix A-4 for restriction on deck setup.

CONTROL DATA LISTING

DATA2

DATA I

... .. I AG1 KEY1 KEY2 KEY3 KEY4 KEY5 KEY6 KEY7 KEY8 KEY9 KEY10

[illegible]

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DATA2

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CONTROL DATA LISTING

CATEGORY	CONTINUE	LAB3L	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10	DATA1	DATA2
601	0	WAKFLFLB	0	11	0	1	10	21	21	1	0	0	C-0.10261300007523480000000-04	0.10000000000000000000 03
601	0	WAKFLFLB	0	11	0	1	10	22	22	1	0	0	C-0.073304345621594500000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	12	0	1	10	23	23	1	0	0	C-0.335581450000000000000-04	0.10000000000000000000 03
601	0	WAKFLFLB	0	12	0	1	10	24	24	1	0	0	C-0.324000000000000000000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	13	0	1	10	25	25	1	0	0	C-0.112327752500000000000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	17	0	1	10	26	26	1	0	0	C-0.226105553173557000000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	17	0	1	10	27	27	1	0	0	C-0.472221305345550000000-04	0.10000000000000000000 03
601	0	WAKFLFLB	0	14	0	1	10	28	28	1	0	0	C-0.2346702746256700000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	15	0	1	10	29	29	1	0	0	C-0.421075410533633000000-05	0.10000000000000000000 03
601	0	WAKFLFLB	0	15	0	1	10	30	30	1	0	0	C-0.247002572751764500000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	16	0	1	10	31	31	1	0	0	C-0.175922505437511000000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	16	0	1	10	32	32	1	0	0	C-0.5654600000000000000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	17	0	1	10	33	33	1	0	0	C-0.747672171315645000000-04	0.10000000000000000000 03
601	0	WAKFLFLB	0	17	0	1	10	34	34	1	0	0	C-0.4240000000000000000-04	0.10000000000000000000 03
601	0	WAKFLFLB	0	18	0	1	10	35	35	1	0	0	C-0.117126259479482000000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	18	0	1	10	36	36	1	0	0	C-0.3765463274500000000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	19	0	1	10	37	37	1	0	0	C-0.7435545236240000000-04	0.10000000000000000000 03
601	0	WAKFLFLB	0	19	0	1	10	38	38	1	0	0	C-0.5933000000000000000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	20	0	1	10	39	39	1	0	0	C-0.107590118752130000000-04	0.10000000000000000000 03
601	0	WAKFLFLB	0	20	0	1	10	40	40	1	0	0	C-0.2947475421531800000-03	0.10000000000000000000 03
601	0	WAKFLFLB	0	1	0	1	10	41	41	1	0	0	C-0.544130659359710000000-14	0.10000000000000000000 02
601	0	WAKFLFLB	0	2	0	1	14	42	42	1	0	0	C-0.5232755552193000000-03	0.10000000000000000000 02
601	0	WAKFLFLB	0	3	0	1	14	43	43	1	0	0	C-0.101446737585500000000-12	0.10000000000000000000 02
601	0	WAKFLFLB	0	5	0	1	14	44	44	1	0	0	C-0.0344472767000000000-03	0.10000000000000000000 02
601	0	WAKFLFLB	0	6	0	1	14	45	45	1	0	0	C-0.0	0.10000000000000000000 02
601	0	WAKFLFLB	0	7	0	1	14	46	46	1	0	0	C-0.132657721191400000000-03	0.100000000000

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CONTROL DATA LISTING


[illegible]

DATA I

DATA2

[illegible]

DATA2



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COURTROOM LAY-OUT LISTING

TELETYPE	CONTINUE	LABEL	KEY1	KEY2	KEY3	KEY4	KEY5	KEY6	KEY7	KEY8	KEY9	KEY10	DATA1	DATA2
702	0	GRKEM	54	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKOL	55	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	56	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKOL	57	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKOL	58	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKOL	59	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	60	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	61	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	62	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	63	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	64	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	65	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	66	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	67	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	68	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	69	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	70	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	71	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	72	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	73	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	74	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	75	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	76	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	77	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	78	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	79	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	80	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	81	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	82	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	83	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	84	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	85	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	86	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	87	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	88	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	89	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	90	0	1	0	0	0	0	0	0	0	0.0	0.0
702	0	GRKPM	91	0	1	0	0	0	0	0	0	0	0.0	0.0



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2. Control Systems Research, Inc., "Minitrack Tracking Function Description", March 1970, Final Report NASA Contract NAS5-10694.
3. Rice, William M., "A Review of NASA Minitrack Data Time-Tagging", November 1970, Goddard Space Flight Center X-551-70-41.
4. DBA Systems, Inc., "Network Analysis Program, Phase II, User's Guide to Data Preparation", December 1969, NASA Contract NAS5-10588.
5. Morduch, G. E., "An Algorithm for the Computation of the Gradient Of a Newtonian Potential Expressed as a Sum of Spherical Harmonics", June 1971, NASA/GSFC X-551-71-248.

APPENDIX A-1
CONSTANTS USED IN NAP-II

A-1.1

THE GRAVITY MODEL USED

The gravity model used for data processing under this contract was the Smithsonian M1 model, (Reference 1), which is built into the NAP program, modified by the GEOS-A resonant harmonics (Reference 2). The GEOS-A resonant harmonics were not obtained from the original source, but from (Reference 3).

The gravitational mass of the Earth was taken as $.3986032 \text{ D15 m}^3/\text{sec}^2$, which is the NAP default value.

The Smithsonian M1 values for the spherical harmonics coefficients are listed below:

<u>(N, M)</u>	<u>C(N, M)</u>	<u>S(N, M)</u>
(0, 0)	1.	0.
(1, 0)	0.	0.
(2, 0)	- .108264500002 D-2	0.
(3, 0)	.254599999999 D-5	0.
(4, 0)	.164900000002 D-5	0.
(5, 0)	.21 D-6	0.
(6, 0)	- .645999999993 D-6	0.
(7, 0)	.332999999998 D-6	0.
(8, 0)	.269999999997 D-6	0.
(9, 0)	.529999999998 D-7	0.
(10, 0)	.540000000002 D-7	0.
(11, 0)	- .302 D-6	0.
(12, 0)	.357000000006 D-6	0.
(13, 0)	.113999999999 D-6	0.
(14, 0)	- .178999999999 D-6	0.
(1, 1)	0.	0.
(2, 1)	0.	0.
(3, 1)	.209111899862 D-5	.287312837632 D-6
(4, 1)	- .542646846485 D-6	- .444932466779 D-6
(5, 1)	- .676515582477 D-7	- .88203930748 D-7
(6, 1)	- .36979402246 D-7	- .21243486397 D-7
(7, 1)	.14418923578 D-6	.114180308536 D-6
(8, 1)	- .515388203208 D-7	.446669776114 D-7
(9, 1)	.76024995806 D-7	.779743547594 D-8
(10, 1)	.648810099708 D-7	- .778572119639 D-7
(11, 1)	- .312872807930 D-7	.885489079044 D-8
(12, 1)	- .922805782847 D-7	- .401958347128 D-7
(13, 1)	0.	0.
(14, 1)	- .788307409236 D-8	.278535284599 D-8

<u>(N,M)</u>	<u>C(N,M)</u>	<u>S(N,M)</u>
(2, 2)	.153563789676 D-5	- .872066750118 D-6
(3, 2)	.250708728736 D-6	- .183761983737 D-6
(4, 2)	.737902432577 D-7	.147804093315 D-6
(5, 2)	.102117707526 D-6	- .375456547484 D-7
(6, 2)	.858383031385 D-8	- .455316216648 D-7
(7, 2)	.362552678174 D-7	.162351886106 D-7
(8, 2)	.21354899813 D-8	.320323497197 D-8
(9, 2)	- .27706980487 D-9	.242436079257 D-8
(10, 2)	- .624317809516 D-8	- .249727123811 D-8
(11, 2)	0.	0.
(12, 2)	- .469893640425 D-8	- .232665783121 D-9
(3, 3)	.782277124813 D-7	.225898207164 D-6
(4, 3)	.508569773273 D-7	- .113546717887 D-7
(5, 3)	- .171778742888 D-7	.231240615425 D-9
(6, 3)	- .111963004094 D-8	.642750579065 D-9
(7, 3)	.352147606138 D-8	.253546276422 D-9
(8, 3)	- .374070918995 D-9	.404400993503 D-10
(9, 3)	0.	0.
(10, 3)	- .378977225408 D-9	.174912565571 D-9
(4, 4)	- .11198293875 D-8	.485963696475 D-8
(5, 4)	- .206336328204 D-8	.498321698304 D-9
(6, 4)	- .166560812946 D-9	- .196087502512 D-8
(7, 4)	- .322776554575 D-9	- .216600056362 D-9
(8, 4)	- .276702101966 D-9	- .156623831302 D-10
(9, 4)	0.	0.
(10, 4)	- .435831320535 D-10	- .653746980798 D-10
(5, 5)	.384108946188 D-9	- .145764420605 D-8
(6, 5)	- .252611520257 D-9	- .369636026451 D-9
(7, 5)	.268980462153 D-10	.191117696793 D-10
(8, 5)	- .959291939079 D-11	.213578205308 D-10
(6, 6)	- .931919036559 D-11	- .36111862666 D-10
(7, 6)	- .145066373826 D-10	.437281413924 D-11
(8, 6)	- .474787418211 D-12	.88813175875 D-11

<u>(N,M)</u>	<u>C(N,M)</u>	<u>S(N,M)</u>
(7, 7)	.102027945339 D-11	.178085140954 D-11
(8, 7)	- .443617740607 D-13	.158070689181 D-12
(8, 8)	- .316141378363 D-12	.130025889487 D-12
(12, 12)	0.	0.
(13, 12)	- .1082186306 D-18	.895602460152 D-19
(14, 12)	0.	0.
(15, 12)	- .114596608272 D-19	.107203278705 D-19
(13, 13)	- .274440770475 D-19	.365921027295 D-20
(14, 13)	0.	0.
(15, 13)	- .127051846403 D-20	- .133101934329 D-20
(14, 14)	0.	0.
(15, 14)	.219788278315 D-22	- .532258360739 D-22

The GEOS-A resonant spherical harmonics coefficients are listed below:

<u>(N,M)</u>	<u>C(N,M)</u>	<u>S(N,M)</u>
(13, 12)	- .126299 D-18	.165220 D-18
(14, 12)	.139978 D-20	- .131772 D-19
(15, 12)	- .138126 D-19	- .189639 D-20

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1. Lundquist, C. A., Veis, G., "Geodetic Parameters for a 1966 Smithsonian Institution Standard Earth," SAO Special Report Number 200, Volume 1.
2. Kohnlein, W., "The Earth's Gravitational Field as Derived From a Combination of Satellite Data With Gravity Anomalies," Prepared for XIV General Assembly, International Union of Geodesy and Geophysics, International Association of Geodesy, October 1967.
3. Lerch, F. J., Marsh, J. G., O'Neill, B., "Evaluation of the Goddard Range and Range Rate System at Rosman by Intercomparison With GEOS-I Long Arc Orbital Solutions," Goddard Space Flight Center, Maryland, X-552-68-72, November 1967.

The C-5 Earth Model was adopted for the data processing. According to this model the Earth is defined geometrically by the following constants:

Rotation Rate	=	.7292115854937 D-4 radians/sec
Semi-Major Axis	=	6378165 meters
Eccentricity Squared	=	.669454185459 D-2.

The station coordinates are given below:

<u>Station Coordinates (Optical)</u>				
<u>Station</u>	<u>Station ID</u>	<u>Latitude</u>	<u>Longitude</u>	<u>Height Above Geoid</u>
COLDLK	29424	54°44'37.26"	249°57'21.90"	548 meters
NEWFL	31032	47°44'28.73"	307°16'46.67"	58 meters
JUPTH	37073	27°1'14.33"	279°53'12.72"	- 41 meters
JUPTR	29010	27°1'14.23"	279°53'12.95"	- 36 meters
JBC4L	37074	27°1'14.55"	279°53'12.76"	- 38 meters
COLEG	31033	64°52'17.78"	212°9'37.29"	139 meters
OOMER	31024	-31°23'26.96"	136°52'14.25"	148 meters
EDINB	37036	26°22'46.35"	261°40'7.34"	15 meters
JUP40	37072	27°1'14.39"	279°53'12.49"	- 38 meters
GFORK	31034	48°1'20.81"	262°59'19.55"	200 meters
ROSMA	31042	35°12'7.03"	277°7'40.81"	857 meters
PURIO	37040	18°15'28.30"	294°0'23.63"	5 meters
ORGAN	29001	32°25'24.70"	253°26'48.29"	1610 meters
GSFCP	37043	39°1'14.78"	283°10'20.39"	- 1 meter
BPOIN	31021	38°25'49.44"	282°54'48.65"	- 50 meters
EDWAFB	29425	34°57'50.17"	242°5'7.80"	754 meters

Station Coordinates (Optical) (Continued)

<u>Station</u>	<u>Station ID</u>	<u>Latitude</u>	<u>Longitude</u>	<u>Height Above Geoid</u>
JUP24	37071	27°1'14.00"	279°53'12.30"	- 38 meters
DENVR	37045	39°38'47.54"	255°23'38.52"	1751 meters
COLBA	37037	38°53'35.81"	267°47'40.85"	218 meters
FTMYR	31022	26°32'53.08"	278°8'3.80"	- 42 meters
BERMD	37039	32°21'48.94"	295°20'34.18"	- 28 meters
MOJAV	31030	35°19'47.57"	243°5'59.18"	874 meters
SATAG	31028	-33°8'58.76"	289°19'52.59"	705 meters

Station Coordinates (Minitrack)

<u>Station</u>	<u>Latitude</u>	<u>Longitude</u>	<u>Height Above Geoid</u>
Fort Myers	26°32'53.08"	278°8'3.80"	- 42 meters
Quito	-37'22.63"	281°25'15.23"	3554 meters
Lima	-11°46'37.56"	282°50'58.86"	34 meters
Santiago	-33°8'58.76"	289°19'52.59"	705 meters
New Foundland	47°44'28.73"	307°16'46.67"	58 meters
Winkfield	51°26'40.67"	359°18'8.35"	76 meters
Johannesburg	-25°53'2.7"	27°42'25.41"	1546 meters
Blossom Point	38°25'49.44"	282°54'48.65"	- 50 meters
College	64°52'17.78"	212°9'37.29"	139 meters
Mojave	35°19'47.57"	243°5'59.18"	874 meters
Grand Fork	48°1'20.81"	262°59'19.55"	200 meters
Woomera	-31°23'26.96"	136°52'14.25"	148 meters

APPENDIX A-2

SPECIAL PROGRAMS WRITTEN TO AID
MINITRACK DATA REDUCTION

A-2.1 PROGRAM FOR EXTRACTING MINITRACK MESSAGES
FOR GEOS I AND SAMPLE JCL

PROGRAM FOR EXTRACTING MINITRACK MESSAGES FOR SATELLITE ID 65891

```

DIMENSION D(65),T(8)
DATA T,'8','6','5','8','9','1',' ',' ','/
LOGICAL*1 D,T,D1,T1
REAL*8 DATA,TEST
EQUIVALENCE (DATA,C1,U(1)),(TEST,T1,T(1))
REWIND 9
REWIND 11
NPASST = 0
NPASSG = 0
100 READ (9, 601, END=900, ERR=100) D
IF(U1.NE.T1) GO TO 100
200 NPASST = NPASST + 1
IF (DATA.NE.TEST) GO TO 100
NPASSG=NPASSG+ 1
WRITE(6,602) NPASST, NPASSG
300 WRITE(11,601) D
400 REAC(9,601,END=900,ERR=400) D
IF(D1.EQ.T1) GO TO 200
GO TO 300
900 CONTINUE
REWIND 9
END FILE 11
REWIND 11
CO 940 I =1,100
910 CONTINUE
READ(11,601,END=950,ERR=910) D
WRITE(6,603) D
940 CONTINUE
950 CONTINUE
REWIND 11
STOP
601 FORMAT (65A1)
602 FORMAT (//2X,'TOTAL NUMBER OF MESSAGES', I10/
* 2X,'NUMBER OF GOES-A MESSAGES', I10)
603 FORMAT (10X,65A1)
STOP
END

```

```
/*  
//STEP2 EXEC LINKGO  
//GO.FT09F001 DD UNIT=(9TRACK,,DEFER),DISP=(OLD,KEEP),LABEL=(2,BLP),  
// DCB=(RECFM=FB,BLKSIZE=3250,LRECL=65,DEN=2),VOL=SER=31027G,DSN=&DEO  
//GO.FT11F001 DD UNIT=2400-9,LABEL=(7,BLP),DISP=(NEW,DELETE),  
// DCB=(RECFM=FB,BLKSIZE=3250,LRECL=65,DEN=2),VOL=SER=33951C,DSN=&MOR  
/*
```

0059 CARDS

A-2.2 MINITRACK SORT PROGRAM AND JCL

```

//Z7GEMSRJ JOB (G70041150A,T,C00138,007007),Z7,MSGLEVEL=1
//STEPI EXEC FORTRANH,PARM='OPT=2'
//SOURCE.SYSIN DD *
      DEFINE FILE 11(120C,2145,L,ID11)
      DIMENSION BLANKS(65),AMPID(65),MINI(65,33),DATA(65),MINY(2145)
      DIMENSION WORD(1202),LRECD(1200),K1(8),K2(8),K3(8),KD(8)
      DIMENSION KSTA(16),STATIQ(16),JCNE(10),MON(14)
      LOGICAL*1 BLANKS,AMPID,MINI,DATA,MINY,BIN,PEZ,DL,AMP
      REAL*8 STATIQ
      REAL*8 INTAPE,NDTAPE
      INTEGER*2 K1,K2,K3,KD,KSTA,NSTAD,NSTAT,L,LINED
      COMPLEX*16 WORD,WORD1,WORD2,WORD3,WORD0
      EQUIVALENCE (AMP,AMPID(1)),(MINI(1,1),MINY(1,1)),(DL,DATA(1,1)),
1(WORD1,K1(1)),ISEC1,(K1(3),IFROM1),(K1(5),IG01),(WORD2,K2(1)),
2      JSEC,ISEC2,(K2(3),IFROM2),(K2(5),IG02),(K2(7),NSTAT),
3(K2(8),L),(WORD3,K3(1)),ISEC3,(K3(3),IFROM3),(K3(5),IG03),
4(WORD,KD(1)),ISECD,(KD(3),IFROMD),(KD(5),IGOD),
5(KD(7),NSTAD),(KD(8),LINED)
      DATA AMPID(1),AMPID(2),AMPID(3),AMPID(4),AMPID(5),AMPID(6)
1'8',6',5',8',9',1' /
      DATA BLANKS(1),BIN,PEZ/' ',0', ' /
      DATA MON/0,31,59,90,120,151,181,212,243,273,304,334,365,500/
      REWIND 9
      REWIND 10
      ID11=1
      DO 10 I=2,65
10 BLANKS(I)=BLANKS(1)
      DO 20 I=7,65
20 AMPID(I)=BLANKS(1)
      IFROM3 = 1201
      IG01 = 1202
      ISEC3 = 2000000000
      ISEC1 = - 2000000000
      WORDC(1201) = WORD1
      WORDC(1202) = WORD3
      DO 30 I=1,16
30 REAC(5,1050) KSTA(I),STATIQ(I)
      JONE(1)=5
      JONE(2)=13
      JONE(3)=18
      JONE(4)=26
      JONE(5)=31
      JONE(6)=39
      JONE(7)=45

```

```

JCNE(8)=53
JONE(9)=57
JONE(10)=65
NDYR=365
IPAGE=1
40 CONTINUE
READ (5,1090,END=950) INTAPE,INFILE,NOTAPE,NDFILE
MTOT=0
M=1
C CHECK FOR AMPERSAND
100 READ(9,1000,ERR=100,END=500) DATA
IF(D1.NE.AMP) GO TO 100
C WHEN AMPERSAND HAS BEEN FOUND UPDATE TOTAL
C NUMBER OF MESSAGES
110 MTOT=MTOT+1
NENDAM=0
L=1
C READ MESSAGE
200 REAC(9,1000,ERR=200,END=350)(MINI(I,L),I=1,65)
IF(MINI(1,L).EQ.AMP) GO TO 360
210 J=1
J2=1
300 J1=JCNE(J2)
310 MTEST=MINI(J,L)-BIN
IF(MTEST.GT.9) GO TO 34C
IF(MTEST.LT.0) GO TO 34C
J=J+1
IF(J.LT.J1) GO TO 310
C CHECK FOR PERIOD
IF(MINI(J,L).NE.PEZ) GO TO 340
IF(J2.EQ.10) GO TO 320
J=J+1
J2=J2+1
GO TO 300
C ONE GOOD LINE OF DATA HAS BEEN PROCESSED
320 IF(L.GT.1) GO TO 33C
C COMPUTE STATION NUMBER FROM FIRST LINE
NSTAT=MINY(56)-BIN+10*(MINY(55)-BIN)
322 L = 2
GO TO 200
330 DO 334 IK = 1,65
IF (MINI(IK,L).NE.MINI(IK,1)) GO TO 336
334 CONTINUE
GO TO 322

```

336 CONTINUE

IF (MINI(56,L).NE.MINY(56)) GO TO 200

IF (MINI(55,L).NE.MINY(55)) GO TO 200

IF (L.GE.33) GO TO 380

C REAC NECT LINE

L=L+1

GO TO 200

C BAD LINE. IF CALIBRATION LINE BAD IGNORE THIS RECORD

340 CONTINUE

IF (L.LT.2) GO TO 348

DO 345 IK = 1,65

IF (MINI(IK,L).NE.BLANKS(1)) GO TO 200

345 CONTINUE

GO TO 370

348 CONTINUE

WRITE(6,107C) MTOY

GO TO 100

C END OF MESSAGES

350 NENDAM=1

GO TO 370

C NEW MESSAGE AMPERSAND HAS BEEN READ

360 NENDAM=-1

370 L=L-1

380 IF (L.GE.5) GO TO 385

WRITE (6,1080) MTOY

GO TO 415

385 CONTINUE

IDAY=MINY(107)-BIN+10*(MINY(106)-BIN+10*(MINY(105)-BIN))

IF (M.LE.1) IDAY1=IDAY

ICAY=IDAY-IDAY1

IF (IDAY.GT.180) IDAY=IDAY-NOYR

IF (IDAY.LT.(-180)) IDAY=IDAY+NOYR

IH=MINY(93)-BIN+10*(MINY(92)-BIN)

IM=MINY(80)-BIN+10*(MINY(79)-BIN)

IS=MINY(67)-BIN+10*(MINY(66)-BIN)

JSEC=IS+60*(IM+60*(IH+24*IDAY))

JPLUS = JSEC + 30

JMINUS = JSEC - 30

L=65*L

LI = M

M = M + 1

390 IF (JSEC.GE.ISEC3) GO TO 410

IFROM1 = IFROM3

400 WORD1 = WORD(IFROM1)

```

IF(JSEC.LI.ISEC1) GO TO 400
WORD3 = WORD(IG01)

C
C
GO TO 420
410 WORD3 = WORD(IG03)
IF(JSEC.GE.ISEC3) GO TO 410
WORD1 = WORD(IFROM3)

C
C
420 CONTINUE
IF(JPLUS.GT.ISEC3) GO TO 2000
430 IF(JMINUS.LI.ISEC1) GO TO 2020

C
C NO DUPLICATE MESSAGES
C
440 CONTINUE
IFROM2 = IFROM3
IG02 = IG01
IFROM3 = LI
IG01 = LI
WORD(IFROM2) = WORD1
WORD(LI) = WORD2
WORD(IG02) = WORD3
LREC(LI) = MTOT
WRITE(11,LI)(MINY(I),I=1,L)
IF(M.GT.1200) GO TO 500
415 IF(NENDAM) 110,100,500
500 CONTINUE
M = M - 1
WRITE(6,1010) MTOT,M
WRITE (6,1100) IPAGE,NDIAPPE,INTAPE,NDFILE,INFILE
N = C
WORD2 = WORD(1201)

510 CONTINUE
IG01 = IG02
IF(IG01.GT.1200) GO TO 500
N = N + 1
WORD2 = WORD(IG01)
DO 810 K=1,16
IF(ISTAT.EQ.KSTAT(K)) GO TO 820
810 CONTINUE
K = 16
820 ITO = ISEC2/86400

```



```

ITS = ISEC2 - ITD*86400
IF(ITS.GE.0) GO TO 815
ITC = ITD - 1
ITS = ITS + 86400
815 CONTINUE
IHR = ITS/3600
IMIN = (ITS - IHR*3600)/60
IS = ITS - IHR*3600 - IMIN*60
ITD=ITD+IDAY1
IF(ITC.GT.NDYR) ITD=ITD-NDYR
IF(ITD.LE.0) ITD=ITC+NDYR
IMON = 2 + ITD/32
IF (ITD.LE.MON(IMON)) IMON = IMON - 1
IMD = ITD - MON(IMON)
READ(11,IGOI,ERR=83C)(MINY(I),I=1,L)
L=L/65
WRITE(6,1020)N,LRECE(IGCI),NSTAT,STATIO(K),ITD,IMON,IMD,ITS,
* IHR,IMIN,IS,L
WRITE(10,1000) AMPID
WRITE(10,1000)((MINI(J,I),J=1,65),I=1,L)
WRITE(10,1000) BLANKS
C WRITE(6,1030) AMPID
C WRITE(6,1030)((MINI(J,I),J=1,65),I=1,L)
C WRITE(6,1030) BLANKS
GO TO 510
830 WRITE(6,1040) N
GO TO 510
900 CONTINUE
END FILE 10
WRITE(6,1060) IPAGE
WRITE(6,1060) IPAGE
GO TO 40
950 CONTINUE
REWIND 9
REWIND 10
STOP
1000 FORMAT(65A1)
1010 FORMAT(15X,'TOTAL NUMBER OF MESSAGES=',I5,
1 6X,'NUMBER OF PROCESSED MESSAGES=',I5)
1020 FORMAT(6X,14,14X,14,16X,12,12X,A6,12X,13,5X,12,7X,15,5X,12,
12X,12,2X,12,15)
1030 FORMAT(6X,65A1)
1040 FORMAT(6X,'ERROR RECORD NO.',I5)
1050 FORMAT(15,5X,A6)

```

```

1060 FORMAT(11)
1070 FORMAT(6X,'BAD CALIBRATION LINE MESSAGE NO.',I4,X,'REJECTED.')
1080 FORMAT(6X,'TOO FEW LINES MESSAGE NO.',I4,X,'REJECTED.')
1090 FORMAT(6X,'A8,I5,A8,I5)
1100 FORMAT(11,5X,'OUTPUT TAPE',7X,'INPUT TAPE',10X,'STATION',25X,'DAY',
1,5X,'MONTH',2X,'DAY',6X,'SEC',7X,'HR',2X,'MIN',X,'SEC',X,'LINE',/6X
1,'NO.',A8,7X,'NO.',A8,9X,'ID',12X,'NAME',60X,'NO.',/6X,'FILE',I5,9X
1,'FILE',I5/6X,'MESSAGE NO.',7X,'MESSAGE NO.')
1110 FORMAT(6X,'DUPLICATE MESSAGES',I5,X,'AND',I5,'. THE SECOND MESSAGE
1 HAS BEEN REJECTED.')

2000 WORDC = WORD3
2010 IF(STAT.EQ.NSTAD) GO TO 2040
WORDC = WORD(IGOD)
IF(JPLUS.GT.ISECD) GO TO 2010
GO TO 430

2020 WORDC = WORD1
2030 IF(STAT.EQ.NSTAD) GO TO 2040
WORDC = WORD(IFROMD)
IF(JMINUS.LT.ISECD) GO TO 2030
GO TO 440

2040 CONTINUE
M = M - 1
WORD1 = WORD(IFROMD)
IF(LINED-GE.L) GO TO 2100
WRITE(6,1110) MTOT,LRECC(IGOI)
WORD3 = WORD(IGOD)
LI = IGO1
IGOI = IGOD
IFROM3 = IFROMD
WORD(IFROM3) = WORD1
WORD(IGOI) = WORD3
GO TO 390

2100 CONTINUE
WRITE(6,1110) LRECD(IGOI),MTOT
GO TO 415
END

/*
//STEP2 EXEC LINKGO
//GO.FT09FC01 DD UNIT=(9TRACK,,DEFER),DISP=(OLD,KEEP),LABEL=(7,BLP),
// DCB=(RECFM=FB,BLKSIZE=3250,LRECL=65,DEN=2),VOL=SER=34248B
//GO.FT10F001 DD UNIT=(9TRACK,,DEFER),DISP=(NEW,DELETE),LABEL=(7,BLP),
// DCB=(RECFM=FB,LRECL=65,BLKSIZE=3250,DEN=2),VOL=SER=2135H
//GO.FT11F001 DD UNIT=2314,DSN=6MINI,DISP=(NEW,DELETE),
// DCB=RECFM=FT,SPACE=(CYL,(3C,2))

```

```

//GO.CLEAR DD DSN=&LODMO0(GSFC),DISP=(OLD,DELETE)
//GO.SYSABEND DD SYSOUT=A,DCB=(RECFM=VBA,LRECL=137,8LKSIZE=7265),
//          SPACE=(CYL,(1))

```

```

//GO.DATAS DD *

```

03	FTMYS
05	QUITOE
06	LIMAPU
08	SNTAGO
12	NEWFLD
15	WKFELD
16	JOBURG
19	ALASKA
21	CRORAL
23	MAUGAR
01	BPOINT
13	COLEGE
17	POJAVE
14	GRDFKS
18	WOOMER
00	NCNAME

```

342488 7 2135H 7

```

```

/*

```

0286 CARDS

A-2.3 THE MINITRACK PREPROCESSOR

```

//Z7GEMRWB JOB (G70041150A,T,000138,005005),Z7,MSGLEVEL=1
// EXEC  LOADER,PARM=MAP,CALL,SIZE=440K,REGION.CO=450K
//GO.SYSLIN DD UNIT=2400-9,LABEL=(1,BLP),DISP=(OLD,KEEP),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),VOL=SER=2023G
//GO.FT06F001 DD DUMMY
//GO.FT07F001 DD SYSOUT=B,DSN=DECK
//GO.FT09F001 DD UNIT=2400-9,LABEL=(2,BLP),DISP=(OLD,DELETE),
// DCB=(RECFM=FB,LRECL=65,BLKSIZE=3250,DEN=2),VOL=SER=1664J
//GO.FT11F001 DD DUMMY
//GO.FT12F001 DD UNIT=2400-9,LABEL=(2,BLP),DISP=(NEW,KEEP),
// DCB=(RECFM=VBS,LRECL=52,BLKSIZE=5204),VOL=SER=30060D
//GO.FT13F001 DD SYSOUT=A,SPACE=(CYL,(1,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT14F001 DD SYSOUT=A,SPACE=(CYL,(1,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT19F001 DD DUMMY
//GO.FT20F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT21F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT22F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT23F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT24F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT25F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT26F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT27F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT28F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT29F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT30F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT31F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT32F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT33F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)

```

```

//GO.FT34F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT35F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT36F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT37F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT38F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT39F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT40F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT41F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT42F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT43F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT44F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT45F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT46F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT47F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT48F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT49F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT50F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.FT51F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=3429)
//GO.SYSABEND DD SYSOUT=A,SPACE=(CYL,(1))
//GO.DATA5 DD *

```

FTMYR6 03 369 369 064 28 372 25 957 137 902 00 120 26 013 431 690107

FTM1E 03
FTM2E 03
FTM3E 03
FTM4E 03

FTM1P 03

FTM2P 03

FTM3P 03

FTM4P 03

QUIT06 05 380 379 952 00 889 00 822 766 082 00 726 00 054 020 690107

05

05

05

05

05

05

05

05

LIMAP6 06 382 382 460 28 655 52 950 022 940 00 966 00 247 876 690107

06

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06

SNTAG6 08 391 391 983 00 106 00 078 938 013 00 976 00 042 970 690107

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NEWFL6 12 372 372 467 29 070 25 935 174 887 00 518 28 929 914 690107

12

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WNKEL6 15 385 384 540 29 222 25 072 872 100 00 791 28 975 012 690107

15

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65891
00000

136.830

/*

//GO.FT08F001 DD *

GEOS-A MINITRACK DATA STARTING 08 JAN 1966 ARC 3

1 217 66 2 1

/*

//GO.FT08F002 DD DUMMY

//GO.FT08F003 DD DUMMY

//GO.FT08F004 DD DUMMY

/*

0239 CARDS

INTEGER SIG1,SIG2,SIG3,SIG4,SIG5,INO,ISO	0000010
INTECER AMP,END,CSTA,CANT,SIG,ANTD,HORD,MIND,SECD,SAT,DATE,KFA,KFB	0000020
INTEGER IGRADE	0000030
REAL NSFD,NSCD,NSMD	0000040
REAL IDIF1,IDIF2,IDIF3,IDIF4,IDIF5	0000050
REAL NSM,NSC,NSFPO,NSFEC,IDIF,NSF1,NSF2,NSF3,NSF4,NSF5	0000060
LOGICAL#1 SLE,SLN	0000070
LOGICAL#1 ASTA,ARMODA,ACUR,IALOB, IARATE,IAACC,IAWMER,IAWGER,IBLOB	0000080
XE,IBRATE,IBACC,IBNMER,IBNCR,ICIGA,IOUR,ISEC,LCOS,MCOS,IENO,INNO	0000090
LOGICAL#1 DATA,PEZ,BIN,SPX,IAMP	0000100
LOGICAL#1 MSGR	0000110
LOGICAL #1 LFILE	000012
REAL#8 XNAP	000013
REAL#8 STATIO	0000140
REAL#8 DNAP	0000150
REAL#8 A,A1,A2,A3	0000160
DIMENSION STATIO(34),KFA(17),KF8(17),EWM(17),CLEWM(17),EWC(17),	000017
1 CLEWC(17), EWFEQ(17), NSM(17), CLNSM(17), NSC(17), CLNSC(17),	000018
2 NSFEC(17), NSFPO(17), ISTA(68), IANT(68), C1(68), C2(68),C3(68),	000019
3 C4(68), C5(68), C6(68), C7(68), C8(68), KSAID(50), FREQ(50),	000020
4 KSTA(48), EWFP(17), TIM(31), CO(68)	000021
DIMENSION SECD(31),EWMD(31),EWCD(31),EWFD(31),NSMD(31),NSCD(31),NS	0000220
1FD(31),MIND(31),HORD(31),DAYD(31),ANTD(31),STAD(31),SIGD(31),EEWF	0000230
2(31),ENSF(31),IOAYD(31),AST(17),DATE(17),CD(68)	000024
DIMENSION ASTA(3),ARMODA(7),ADUR(7),IALOB(6),IARATE(5),IAACC(4),I	0000250
XAWMER(3),IAWGER(3),IBLOB(6),IBRATE(5),IBACC(4),IBNMER(3),IBNCR(3	0000260
X),ICIGA(3),IOUR(5),ISEC(6),LCOS(8),MCOS(8),IENO(3),INNO(3)	0000270
DIMENSION MSGR(80)	0000280
DIMENSION DATA(100)	0000290
DIMENSION SLE(4),SLN(4)	0000300
DIMENSION TFOVEW(31,5),FOVEW(31,5),TFOVNS(31,5),FOVNS(31,5)	0000310
DIMENSION DNAP(6),JUDY(34),IPASS(34),JUSEC(34)	000032
DIMENSION XNAP(6)	000033
DIMENSION IA(17)	000034
DIMENSION IPASST(34)	000035
EQUIVALENCE (SLN(1),INOVER)	0000360
EQUIVALENCE (SLE(1),IEOVER)	0000370
DIMENSION AACOS(31,5),BRCOS(31,5)	0000380
DATA PER,ASK,SPA,POL,EQ,F1,F2,F3,F4,F5,F6,F7,IAMP,SLA,PEZ,BIN,SPX/	0000390
1Z4B404040,Z5C404040,Z40404040,ZD7404040,ZC5404040,ZC1404040,ZC2404	0000400
2040,ZC3404040,ZC4404040,ZC5404040,ZC6404040,ZC7404040,Z50,Z6140404	0000410

```

30,Z4B,ZF0,Z40/
DATA STATIO(17)/'NONAME'//
DATA A1,A2,A3/'PASS','JUDAY','JUSEC'//
SLA=SLA
KDEG=25
LFILE=.FALSE.
DEGREE=KDEG
CCUS=COS(DEGREE*3.1459265/180.)
KSTA(17)=0
XNAP(5)=0.00
XNAP(6)=0.00
DNAP(6)=0.00
DNAP(5)=0.00
DO 330 I=1,34
IPASS(I)=0
IPASST(I)=0
JUDY(I)=0
330 JUSEC(I)=0
READ(5,760)IGRADE
760 FORMAT(9X,I1)
JL=0
JM=0
WRITE(6,760)IGRADE
1340 FORMAT (1H1,19(' '),80X,20(' '))
//50X,'INPUT STATION CONSTANTS'//
2X,'STATION KFA KFB EWM CLEWM EWC CLEWC EWFEQ',
1X,'EWFPD NSM CLNSM NSC CLNSC NSFEQ NSFPO DATE'//
2X,'NAME NO.'//
WRITE (13,1340)
1341 FORMAT (1X,A6,1X,I3,2(2X,I3),1X,F4.3,2X,F4.3,1X,F4.3,
* 2(3X,F4.3,2X,F4.3),1X,F4.3,2X,F4.3,2(3X,F4.3),3X,I6)
DO 35 J=1,16
C INPUT STATION CONSTANTS
READ(5,80) STATIO(J),KFA(J),KFB(J),EWM(J),CLEWM(J),EWC(J)
1,CLEWC(J),EWFEQ(J),EWFPD(J),NSM(J),CLNSM(J),NSC(J),CLNSC(J),NSFEQ(
2J),NSFPO(J),DATE(J)
WRITE(5,580)STATIO(J),KFA(J),KFB(J),EWM(J),CLEWM(J),EWC(J)
1,CLEWC(J),EWFEQ(J),EWFPD(J),NSM(J),CLNSM(J),NSC(J),CLNSC(J),NSFEQ(
2J),NSFPO(J),DATE(J)
80 FORMAT(A6,X,I2,I4,I4,3X,F4.3,F3.3,F4.3,X,F4.3,3X,F4.3,F3
X.3,F4.3,F3.3,X,F4.3,F4.3,5X,I6)
580 FORMAT(X,A6,X,I2,X,I3,X,I3,3X,F4.3,F4.3,F4.3,X,F4.3,
X3X,F4.3,F4.3,F4.3,F4.3,X,F4.3,F4.3,2X,I6)
WRITE (13,1341) STATIO(J),KFA(J),KFB(J),EWM(J),CLEWM(J),

```

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*      EWC(J),CLEWC(J),EWFEC(J),EWFPO(J),NSM(J),CLNSM(J),      000086
*      NSC(J),CLNSC(J),NSFEQ(J),NSFPO(J),DATE(J)      000087
DO 36 M=1,4      0000880
JL=JM+M      0000890
C      INPUT STATION COEFF.      0000900
      READ( 5,81) IANT(JL),ISIA(JL),CO(JL),C1(JL),C2(JL),C3(JL),C4(JL)      0000910
      WRITE(6,811) IANT(JL),ISIA(JL),CO(JL),C1(JL),C2(JL),C3(JL),C4(JL)      0000920
811  FORMAT(4X,A1,X,12,5(X,E15.8))      0000930
      READ(5,581) C5(JL),C6(JL),C7(JL),C8(JL)      0000940
581  FORMAT(8X,4(X,E12.8))      0000950
      WRITE(6,681) C5(JL),C6(JL),C7(JL),C8(JL)      0000960
681  FORMAT(9X,4(X,E15.8))      0000970
81  FORMAT(4X,A1,X,12,5(X,E12.8))      0000980
36  CONTINUE      0000990
      JM=JM+4      0001000
35  CONTINUE      0001010
      WRITE(6,500)(KSTA(I),I=1,16)      000102
500  FORMAT(X, 16(X,I2))      000103
DO 2 I=1,17      000104
      STATIO(I+17)=STATIO(I)      000105
      KSTA(I+17)=KSTA(I)+100      000106
2  CONTINUE      0001070
DO 37 J=1,50      0001080
C      INPUT SATELLITE CONSTANTS      0001090
      READ( 5,82) KSAID(J),FREQ(J)      0001100
82  FORMAT(15,19X,F8.3)      0001110
      WRITE( 6,582) KSAID(J),FREQ(J)      0001120
582  FORMAT(X,15,19X,F8.3)      0001130
      IF(KSAID(J))37,38,37      0001140
37  CONTINUE      0001150
38  KSATCT=J-1      0001160
      READ(8,305,END=321,ERR=902)(MSGR(I),I=1,80)      0001170
305  FORMAT(80A1)      0001180
      NAPEND = 0      000119
      IBI = 0      000120
      REWIND 9      000121
      IARC = 1      000122
      IARCS=-1      000123
      I201 = 201      000124
      I202 = 202      000125
      WRITE(13,340)(MSGR(I),I=1,80)      0001260
340  FORMAT(1H1,19(' '),80A1,20(' '),/50X,'PROCESSING MESSAGES',/)      0001270
      WRITE(14,340)(MSGR(I),I=1,80)      0001280
      WRITE(14,352)      0001290

```

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352 FORMAT (3X,'SUMMARY OF DATA MESSAGES PRODUCED',/3X,'MESSAGE',1X,
* 'DATA',3X,'STATION',3X,'ARC',2X,'PASS',2X,'START TIME',
* 6X,'L',9X,'M',9X,'N',7X,'LDT',6X,'MDOT',6X,'NDOT',
* / 3X,'NUMBER',3X,'PTS',2X,'NO.',2X,'NAME',14X,'DAY',2X,
* 'SEC',//)
902 CONTINUE
IF(NAPEND) 910,920,3
910 READ(9,601,END=915,ERR=910) (DATA(I),I=1,65)
GO TO 910
915 IB1 = 0
920 CONTINUE
READ(8,901,END=1,ERR=920) ILOW,IHIGH,IYEAR,NEWARC,NAPEND
IF(NEWARC.LE.0) GO TO 2010
IARC = NEWARC
IF(IARCS.EQ.IARC) GO TO 2010
DO 2005 I= 1,24
IPASST(I)=IPASS(I)+IPASST(I)
2005 IPASS(I) = 0
2010 CONTINUE
IF(ILOW.GT.IHIGH)IHIGH=ILOW
312 FORMAT(A5,13I5)
K=0
324 READ(8,312,ERR=313,END=313)A,N,(IA(I),I=1,12)
READ(8,901,ERR=313,END=313) (IA(I), I=13,17)
K=K+1
IF(A.EQ.A1)GO TO 314
IF(A.EQ.A2)GO TO 315
IF(A.EQ.A3)GO TO 316
GO TO 313
314 DO 317 I=1,17
317 IPASS(I+N-1)=IA(I)
GO TO 318
315 DO 319 I=1,17
319 JUDY(I+N-1)=IA(I)
GO TO 318
316 DO 323 I=1,17
323 JUSEC(I+N-1)=IA(I)
318 IF(K.LT.6)GO TO 324
313 CONTINUE
IPAGE=1
WRITE(6,302)IPAGE,(MSGR(I),I=1,80)
302 FORMAT(I1,19X,80A1,/)
IPAGE=0
WRITE(6,903)ILOW,IHIGH

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903 FORMAT('ODATA SET RANGES FROM DATA FILE   LOW = ',I5,4X,'HIGH = ',I5)
      KEND=0
901  FORMAT(5I5)
      IF(1B1.LT.ILOW) GO TO 39
      IF(1B1.EQ.ILOW) GO TO 2001
      1B1=0
      REWIND 9
      READ SATELLITE IDENTIFICATION,CHECK FOR AMPERSAND*****
39  CONTINUE
      READ(9,601,END=902,ERR=39)(DATA(I),I=1,65)
601  FORMAT(65A1)
94  CONTINUE
      IF(DATA(1).NE.IAMP)GO TO 39
      IF(DATA(7).EQ.SPX)GO TO 83
      IF(DATA(8).EQ.SPX)GO TO 83
      IF(DATA(4)-BIN.EQ.0)GO TO 85
      SAT=((DATA(3)-BIN)*1000.)+(DATA(4)-BIN)*1000.+(DATA(5)-BIN)*10
      XO.+(DATA(6)-BIN)*10.+(DATA(8)-BIN)
      GO TO 84
85  SAT=((DATA(2)-BIN)*1000.)+(DATA(3)-BIN)*1000.+(DATA(5)-BIN)*10
      XO.+(DATA(6)-BIN)*10.+(DATA(8)-BIN)
      IGRADE=(DATA(10)-BIN)
      IYEAR=(DATA(12)-BIN)*10+(DATA(13)-BIN)
      GO TO 84
83  SAT=((DATA(2)-BIN)*1000.)+(DATA(3)-BIN)*1000.+(DATA(4)-BIN)*10
      XO.+(DATA(5)-BIN)*10+(DATA(6)-BIN)
84  CONTINUE
      1B1=1B1+1
      IF(1B1.LT.ILOW)GO TO 39
      IF(1B1.GT.IHIGH)GO TO 9C2
2001 CONTINUE
      DO 602 M=1,50
      IF(SAT.EQ.KSAID(M))GO TO 603
602 CONTINUE
      WRITE( 6,635)
635  FORMAT(19H SAID NOT IN TABLE )
      WRITE(6,183)IAMP,SAT
183  FORMAT(X,A1,I5)
      GO TO 604
603 CONTINUE
      IF(IPAGE.EQ.0)GO TO 320
      WRITE(6,302)IPAGE,(MSGR(I),I=1,80)
      IPAGE=0

```

320	WRITE(6,310)IPAGE,181	0002180
	WRITE(6,660)(DATA(I),I=1,65)	0002190
	KKSAID=KSAID(M)	0002200
C	READ CAL.LINE WITH FORMAT CHECK *****	0002210
	READ(9,601,END=902,ERR=30)(DATA(I),I=1,65)	0002220
	IF(DATA(1).EQ.IAMP)GO TO 83	0002230
	WRITE(6,660)(DATA(I),I=1,65)	0002240
C	CHECK PERIODS IN CAL. LINE	0002250
	IF(DATA(5).NE.PEZ)GO TO 604	0002260
	IF(DATA(13).NE.PEZ)GO TO 604	0002270
	IF(DATA(18).NE.PEZ)GO TO 604	0002280
	IF(DATA(26).NE.PEZ)GO TO 604	0002290
	IF(DATA(31).NE.PEZ)GO TO 604	0002300
	IF(DATA(39).NE.PEZ)GO TO 604	0002310
	IF(DATA(45).NE.PEZ)GO TO 604	0002320
	IF(DATA(53).NE.PEZ)GO TO 604	0002330
	IF(DATA(57).NE.PEZ)GO TO 604	0002340
	IF(DATA(65).NE.PEZ)GO TO 604	0002350
	DO 605 K=1,4	0002360
	IF(DATA(K)-BIN.GT.9)GO TO 604	0002370
	IF(DATA(K)-BIN.LT.0)GO TO 604	0002380
	DATA(K)=DATA(K)-BIN	0002390
605	CONTINUE	0002400
	DO 606 K=6,12	0002410
	IF(DATA(K)-BIN.GT.9)GO TO 604	0002420
	IF(DATA(K)-BIN.LT.0)GO TO 604	0002430
	DATA(K)=DATA(K)-BIN	0002440
606	CONTINUE	0002450
	DO 607 K=14,17	0002460
	IF(DATA(K)-BIN.GT.9)GO TO 604	0002470
	IF(DATA(K)-BIN.LT.0)GO TO 604	0002480
	DATA(K)=DATA(K)-BIN	0002490
607	CONTINUE	0002500
	DO 608 K=19,25	0002510
	IF(DATA(K)-BIN.GT.9)GO TO 604	0002520
	IF(DATA(K)-BIN.LT.0)GO TO 604	0002530
	DATA(K)=DATA(K)-BIN	0002540
608	CONTINUE	0002550
	DO 609 K=27,30	0002560
	IF(DATA(K)-BIN.GT.9)GO TO 604	0002570
	IF(DATA(K)-BIN.LT.0)GO TO 604	0002580
	DATA(K)=DATA(K)-BIN	0002590
609	CONTINUE	0002600
	DO 610 K=32,38	0002610

IF(DATA(K)-BIN.GT.9)GO TO 604	0002620
IF(DATA(K)-BIN.LT.0)GO TO 604	0002630
DATA(K)=DATA(K)-BIN	0002640
610 CONTINUE	0002650
DO 611 K=40,44	0002660
IF(DATA(K)-BIN.GT.9)GO TO 604	0002670
IF(DATA(K)-BIN.LT.0)GO TO 604	0002680
DATA(K)=DATA(K)-BIN	0002690
611 CONTINUE	0002700
DO 612 K=46,52	0002710
IF(DATA(K)-BIN.GT.9)GO TO 604	0002720
IF(DATA(K)-BIN.LT.0)GO TO 604	0002730
DATA(K)=DATA(K)-BIN	0002740
612 CONTINUE	0002750
DO 613 K=54,56	0002760
IF(DATA(K)-BIN.GT.9)GO TO 604	0002770
IF(DATA(K)-BIN.LT.0)GO TO 604	0002780
DATA(K)=DATA(K)-BIN	0002790
613 CONTINUE	0002800
DO 614 K=58,64	0002810
IF(DATA(K)-BIN.GT.9)GO TO 604	0002820
IF(DATA(K)-BIN.LT.0)GO TO 604	0002830
DATA(K)=DATA(K)-BIN	0002840
614 CONTINUE	0002850
X=DATA(9)+DATA(22)+DATA(35)+DATA(49)+DATA(61)	0002860
IF(X.NE.45.)GO TO 604	0002870
CSTA=(DATA(55)*10.)+(DATA(56))	0002880
DO 616 L=1,17	000289
IF(KSTA(L).EQ.CSTA)GO TO 617	0002900
616 CONTINUE	0002910
WRITE(6,618)	0002920
618 FORMAT(27H WRONG STATION IN CAL.LINE)	0002930
GO TO 604	0002940
617 D=DATA(3)*10+DATA(4)	0002950
CEWM=D/100.	0002960
D=DATA(16)*10+DATA(17)	0002970
CEWC=D/100.	0002980
D=DATA(6)*100+DATA(7)*10+DATA(8)	0002990
CEWF1=D/1000.	0003000
D=DATA(19)*100+DATA(20)*10+DATA(21)	0003010
CEWF2=D/1000.	0003020
D=DATA(32)*100+DATA(33)*10+DATA(34)	0003030
CEWF3=D/1000.	0003040
D=DATA(46)*100+DATA(47)*10+DATA(48)	0003050

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CEWF4=D/1000.
D=DATA(58)*100+DATA(59)*10+DATA(60)
CEWF5=D/1000.
D=DATA(10)*100+DATA(11)*10+DATA(12)
CNSF1=D/1000.
D=DATA(23)*100+DATA(24)*10+DATA(25)
CNSF2=D/1000.
D=DATA(36)*100+DATA(37)*10+DATA(38)
CNSF3=D/1000.
D=DATA(50)*100+DATA(51)*10+DATA(52)
CNSF4=D/1000.
D=DATA(62)*100+DATA(63)*10+DATA(64)
CNSF5=D/1000.
D=DATA(29)*10+DATA(30)
CNSM=D/100.
D=DATA(43)*10+DATA(44)
CNSC=D/100.
CSTA=DATA(55)*10+DATA(56)
I11 = 1
WRITE (11,310) I11,I11
WRITE(11,501)IAMP,SAT,CSTA,STATIO(L)
501 FORMAT(X,A1,I5,X,I2,X,A6)
CANT=DATA(54)
END=DATA(65)
43 CEWM=EWM(L)+CEWM
CEWC=EWC(L)+CEWC
CNSM=NSM(L)+CNSM
CNSC=NSC(L)+CNSC
KM=5.
RATE=0.
IDIF1=CEWF2-CEWF1
IDIF2=CEWF3-CEWF2
IDIF3=CEWF4-CEWF3
IDIF4=CEWF5-CEWF4
CEWF1=CEWF3+((9.*(IDIF3-IDIF2))-(3.*(IDIF4-IDIF1)))/35.)
IDIF=0.
IF(CANT-2.)162,160,161
C NARROW BAND TRACKING FILTER *****
160 IDIF=0
AST(1)=SPA
GO TO 164
161 IDIF=0
AST(1)=ASK
GO TO 164
0003060
0003070
0003080
0003090
0003100
0003110
0003120
0003130
0003140
0003150
0003160
0003170
0003180
0003190
0003200
0003210
0003220
0003230
000324
000325
0003260
0003270
0003280
0003290
0003300
0003310
0003320
0003330
0003340
0003350
0003360
0003370
0003380
0003390
0003400
0003410
0003420
0003430
0003440
0003450
0003460
0003470
0003480
0003490

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162 IF(CANT.EQ.1.)GO TO 164
163 IDIF=.120
C 2 CPS TRACKING FILTER *****
AST(1)=PER
164 IDIF1=CNSF2-CNSF1
IDIF2=CNSF3-CNSF2
IDIF3=CNSF4-CNSF3
IDIF4=CNSF5-CNSF4
CNSF1=CNSF3+((9.*(IDIF3-IDIF2))-(3.*(IDIF4-IDIF1)))/35.)
CABLE LENGTH INEQUALITIES
CEWM=((CLEWM(L)/.846)*(136.5-FREQ(M)))+CEWM
CEWC=((CLEWC(L)/.846)*(136.5-FREQ(M)))+CEWC
CNSM=((CLNSM(L)/.846)*(136.5-FREQ(M)))+CNSM
CNSC=((CLNSC(L)/.846)*(136.5-FREQ(M)))+CNSC
WRITE(11,636)
636 FORMAT(55H CALIBRATED PHASE READINGS,5 POINT FITTED FINE READINGS)
C CALIBRATED ZENITH *****
WRITE(11,639)
639 FORMAT(63H CEWM CEWC CNSM CNSC CEFW
X CNSF )
WRITE(11,150)CEWM,CEWC,CNSM,CNSC,CEWF1,CNSF1
150 FORMAT(6(X,F10.6))
WRITE(11,640)
640 FORMAT(74H HRMNSC EWFINE EWMED EWCORS NSFINE
XNSMED NSCORS )
C READ DATA WITH FORMAT CHECK*****
DO 41 JK=1,60
K=JK
IF(K.EQ.32.)GO TO 120
621 READ(9,601,END=95,ERR=32)(DATA(I),I=1,65)
IF(DATA(1).EQ.IAMP)GO TO 120
WRITE(6,660)(DATA(I),I=1,65)
IF(DATA(10).EQ.SPX)GO TO 122
GO TO 124
122 IF(DATA(30).EQ.SPX)GO TO 123
GO TO 124
123 IF(DATA(50).EQ.SPX)GO TO 120
124 IF(DATA(5).NE.PEZ)GO TO 621
C CHECK PERIODS IN DATA LINE
IF(DATA(13).NE.PEZ)GO TO 621
IF(DATA(18).NE.PEZ)GO TO 621
IF(DATA(26).NE.PEZ)GO TO 621
IF(DATA(31).NE.PEZ)GO TO 621
IF(DATA(39).NE.PEZ)GO TO 621

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IF(DATA(45).NE.PEZ)GO TO 621	0003940
IF(DATA(53).NE.PEZ)GO TO 621	0003950
IF(DATA(57).NE.PEZ)GO TO 621	0003960
IF(DATA(65).NE.PEZ)GO TO 621	0003970
DO 622 J=1,4	0003980
IF(DATA(J)-BIN.GT.9)GO TO 621	0003990
IF(DATA(J)-BIN.LT.0)GO TO 621	0004000
DATA(J)=DATA(J)-BIN	0004010
CONTINUE	0004020
DO 623 J=6,12	0004030
IF(DATA(J)-BIN.GT.9)GO TO 621	0004040
IF(DATA(J)-BIN.LT.0)GO TO 621	0004050
DATA(J)=DATA(J)-BIN	0004060
CONTINUE	0004070
DO 624 J=14,17	0004080
IF(DATA(J)-BIN.GT.9)GO TO 621	0004090
IF(DATA(J)-BIN.LT.0)GO TO 621	0004100
DATA(J)=DATA(J)-BIN	0004110
CONTINUE	0004120
DO 625 J=19,25	0004130
IF(DATA(J)-BIN.GT.9)GO TO 621	0004140
IF(DATA(J)-BIN.LT.0)GO TO 621	0004150
DATA(J)=DATA(J)-BIN	0004160
CONTINUE	0004170
DO 626 J=27,30	0004180
IF(DATA(J)-BIN.GT.9)GO TO 621	0004190
IF(DATA(J)-BIN.LT.0)GO TO 621	0004200
DATA(J)=DATA(J)-BIN	0004210
CONTINUE	0004220
DO 627 J=32,38	0004230
IF(DATA(J)-BIN.GT.9)GO TO 621	0004240
IF(DATA(J)-BIN.LT.0)GO TO 621	0004250
DATA(J)=DATA(J)-BIN	0004260
CONTINUE	0004270
DO 628 J=40,44	0004280
IF(DATA(J)-BIN.GT.9)GO TO 621	0004290
IF(DATA(J)-BIN.LT.0)GO TO 621	0004300
DATA(J)=DATA(J)-BIN	0004310
CONTINUE	0004320
DO 629 J=46,52	0004330
IF(DATA(J)-BIN.GT.9)GO TO 621	0004340
IF(DATA(J)-BIN.LT.0)GO TO 621	0004350
DATA(J)=DATA(J)-BIN	0004360
CONTINUE	0004370

DO 630 J=54,56	0004380
IF(DATA(J)-BIN.GT.9)GO TO 621	0004390
IF(DATA(J)-BIN.LT.0)GO TO 621	0004400
DATA(J)=DATA(J)-BIN	0004410
630 CONTINUE	0004420
DO 631 J=58,64	0004430
IF(DATA(J)-BIN.GT.9)GO TO 621	0004440
IF(DATA(J)-BIN.LT.0)GO TO 621	0004450
DATA(J)=DATA(J)-BIN	0004460
631 CONTINUE	0004470
SECD(K)=DATA(1)*10+DATA(2)	0004480
MIND(K)=DATA(14)*10+DATA(15)	0004490
HORD(K)=DATA(27)*10+DATA(28)	0004500
ANTD(K)=DATA(54)	0004510
IDAYD(K)=DATA(40)*100+DATA(41)*10+DATA(42)	0004520
SYAD(K)=DATA(55)*10+DATA(56)	0004530
D=DATA(3)*10+DATA(4)	0004540
EWMD(K)=D/100.	0004550
D=DATA(16)*10+DATA(17)	0004560
EWCD(K)=D/100.	0004570
D=DATA(29)*10+DATA(30)	0004580
NSMD(K)=D/100.	0004590
D=DATA(43)*10+DATA(44)	0004600
NSCD(K)=D/100.	0004610
D=DATA(6)*100+DATA(7)*10+DATA(8)	0004620
EWf1=D/1000.	0004630
D=DATA(19)*100+DATA(20)*10+DATA(21)	0004640
EWf2=D/1000.	0004650
D=DATA(32)*100+DATA(33)*10+DATA(34)	0004660
EWf3=D/1000.	0004670
D=DATA(46)*100+DATA(47)*10+DATA(48)	0004680
EWf4=D/1000.	0004690
D=DATA(58)*100+DATA(59)*10+DATA(60)	0004700
EWf5=D/1000.	0004710
D=DATA(10)*100+DATA(11)*10+DATA(12)	0004720
NSf1=D/1000.	0004730
D=DATA(23)*100+DATA(24)*10+DATA(25)	0004740
NSf2=D/1000.	0004750
D=DATA(36)*100+DATA(37)*10+DATA(38)	0004760
NSf3=D/1000.	0004770
D=DATA(50)*100+DATA(51)*10+DATA(52)	0004780
NSf4=D/1000.	0004790
D=DATA(62)*100+DATA(63)*10+DATA(64)	0004800
NSf5=D/1000.	0004810

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SIG1=DATA(9)
SIG2=DATA(22)
SIG3=DATA(35)
SIG4=DATA(49)
SIG5=DATA(61)
END=DATA(65)
100 IF(ANTD(K)-2)102,101,101
101 ANT=57.
GO TO 103
102 ANT=46.
103 TIM(K)={(HORD(K)*3600.)+(60.*MIND(K)))+SECD(K)
FOVEW(K,1)=EWF1
FOVEW(K,2)=EWF2
FOVEW(K,3)=EWF3
FOVEW(K,4)=EWF4
FOVEW(K,5)=EWF5
FOVNS(K,1)=NSF1
FOVNS(K,2)=NSF2
FOVNS(K,3)=NSF3
FOVNS(K,4)=NSF4
FOVNS(K,5)=NSF5
FIT FIVE FINES EACH LINE
IDIF1=EWF2-EWF1
CALL NORMAL(IDIF1)
IDIF2=EWF3-EWF2
CALL NORMAL(IDIF2)
IDIF3=EWF4-EWF3
CALL NORMAL(IDIF3)
IDIF4=EWF5-EWF4
CALL NORMAL(IDIF4)
EWF(K)=EWF3+((9.*(IDIF3-IDIF2))-(3.*(IDIF4-IDIF1)))/35.)
IDIF5=((IDIF1+IDIF2+IDIF3+IDIF4)/4.)
ICTEW = IDIF5 * 0.05
COUNTER DELAY (TIME) *****
EWF(K)=(EWF(K)-(.05*IDIF5*EWF3))
IDIF1=NSF2-NSF1
CALL NORMAL(IDIF1)
IDIF2=NSF3-NSF2
CALL NORMAL(IDIF2)
IDIF3=NSF4-NSF3
CALL NORMAL(IDIF3)
IDIF4=NSF5-NSF4
CALL NORMAL(IDIF4)
ENSF(K)=NSF3+((9.*(IDIF3-IDIF2))-(3.*(IDIF4-IDIF1)))/35.)

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IDIF5=((IDIF1+IDIF2+IDIF3+IDIF4)/4.)
ICTNS = IDIF5 * 0.05
TIM2 = TIM(K) - TIM(1) + 0.000001
DO 300 IFOV = 1,5
  TFOVEW(K,IFOV)=TIM2+0.2*(IFOV-1)+FOVEW(K,IFOV)*0.01
  TFOVNS(K,IFOV)=TIM2+0.2*(IFOV-1)+FOVNS(K,IFOV)*0.01
300 CONTINUE
C
  FILTER DELAY (TIME)
  ENSF(K)=ENSF(K)-(.05*IDIF5*NSF3)
  IDIF1=SIG2-SIG1
  IDIF2=SIG3-SIG2
  IDIF3=SIG4-SIG3
  IDIF4=SIG5-SIG4
  SIGD(K)=SIG3+((9.*(IDIF3-IDIF2))-3.*(IDIF4-IDIF1))/35)
  WRITE(11,151)HORD(K),MIND(K),SECD(K),EWF(K),EWD(K),EWCD(K),ENSF(
XK),NSMD(K),NSCD(K)
151 FORMAT(X,12,12,12,X,(6(F10.6,X)))
41 CONTINUE
GO TO 120
95 CONTINUE
KEND=1
DATA MSG.COMplete,START SMOOTHING *****
C
120 SL=.01
AST(6)=SPA
K=K-1
NBRK=K
IF(K.LE.5)GO TO 780
GO TO 782
780 WRITE( 6,781)
781 FORMAT(27H LESS THAN 5 LINES OF DATA )
KZ=K-1
WRITE(13,341)IB1,CSTA,STATIO(L)
WRITE(13,346)
346 FORMAT(1H+,32X,'MESSAGE TOO SHORT')
IF(KEND.EQ.1)GO TO 902
GO TO 78
782 JK=K
IF(ANT.EQ.57.) GO TO 90
GO TO 91
90 CEWF1=CEWF1+EWFPO(L)
CNSF1=CNSF1+NSFPO(L)
AST(2)=POL
GO TO 121
91 CEWF1=CEWF1+EWFPO(L)

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CNSF1=CNSF1+NSFEQ(L)
AST(2)=EQ
121 SM=2.0
WRITE(11,638)
638 FORMAT(32H KC-KS1 USING STATION CONSTANTS )
WRITE(11,1152)CEWF1,EWFPO(L),EWFPO(L),CNSF1,NSFPO(L),NSFEQ(L)
CHECK TIME SEQUENCE *****
IB=0
IC=0
ID=0
IE=0
IF=0
IG=0
IH=0
KQ=K-1
DO 20 KS=1,KQ
806 ITZM=TIM(KS+1)-TIM(KS)
IF(ITZM)807,807,808
807 TIM(KS+1)=TIM(KS+1)+86400.
GO TO 806
808 IF(ITZM.NE.1)GO TO 21
IB=IB+1
GO TO 20
21 IF(ITZM.NE.2)GO TO 22
IC=IC+1
GO TO 20
22 IF(ITZM.NE.10)GO TO 23
ID=ID+1
GO TO 20
23 IF(ITZM.NE.20)GO TO 24
IE=IE+1
GO TO 20
24 IF(ITZM.NE.60)GO TO 25
IF=IF+1
GO TO 20
25 IF(ITZM.NE.120)GO TO 26
IG=IG+1
GO TO 20
26 IF(ITZM.NE.600)GO TO 20
IH=IH+1
GO TO 20
20 CONTINUE
ITZM=MAXO(IB,IC,ID,IE,IF,IG,IH)
IF(IB.EQ.ITZM)GO TO 200
0005700
0005710
0005720
0005730
0005740
0005750
0005760
0005770
0005780
0005790
0005800
0005810
0005820
0005830
0005840
0005850
0005860
0005870
0005880
0005890
0005900
0005910
0005920
0005930
0005940
0005950
0005960
0005970
0005980
0005990
0006000
0006010
0006020
0006030
0006040
0006050
0006060
0006070
0006080
0006090
0006100
0006110
0006120
0006130

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IF(IC.EQ.ITZM)GO TO 201	0006140
IF(ID.EQ.ITZM)GO TO 202	0006150
IF(IE.EQ.ITZM)GO TO 203	0006160
IF(IF.EQ.ITZM)GO TO 204	0006170
IF(IG.EQ.ITZM)GO TO 205	0006180
IF(IH.EQ.ITZM)GO TO 206	0006190
200 AST(3)=F1	0006200
TILI=1.	0006210
GO TO 207	0006220
201 AST(3)=F2	0006230
TILI=2.	0006240
GO TO 207	0006250
202 AST(3)=F3	0006260
TILI=10.	0006270
GO TO 207	0006280
203 AST(3)=F4	0006290
TILI=20.	0006300
GO TO 207	0006310
204 AST(3)=F5	0006320
TILI=60.	0006330
GO TO 207	0006340
205 AST(3)=F6	0006350
TILI=120.	0006360
GO TO 207	0006370
206 AST(3)=F7	0006380
TILI=600.	0006390
GO TO 207	0006400
72 WRITE(6,73)	0006410
73 FORMAT(22H TIME OUT OF SEQUENCE)	0006420
WRITE(13,341)IB1,CSTA,STATIO(L)	0006430
WRITE(13,345)	0006440
345 FORMAT(1H+,23X,'FRAME TIME OUT OF SEQUENCE')	0006450
KZ=K-1	0006460
78 WRITE(6,77)SAT,CSTA,STATIO(L),HORD(KZ),MIND(KZ),IDAYD(KZ)	0006470
77 FORMAT(X,15,X,12,X,A6,X,12,12,X,13)	0006480
GO TO 65	0006490
74 WRITE(6,75)	0006500
75 FORMAT(25H DATA EXCEEDS TIME CHECK)	0006510
WRITE(13,341)IB1,CSTA,STATIO(L)	0006520
WRITE(13,347)	0006530
347 FORMAT(1H+,31X,'EXCEEDS TIME CHECK')	0006540
KZ=K-1	0006550
GO TO 78	0006560
50 WRITE(11,51)	0006570

51	FORMAT(40H EAST MEDIUM CHANNEL EXCEEDS 100 COUNTS)	0006580
	AST(6)=F1	0006590
	RATE=0.	0006600
	GO TO 58	0006610
52	WRITE(11,53)	0006620
53	FORMAT(40H EAST COURSE CHANNEL EXCEEDS 100 COUNTS)	0006630
	AST(6)=F1	0006640
	RATE=0.	0006650
	GO TO 58	0006660
	GO TO 58	0006670
54	WRITE(11,55)	0006680
55	FORMAT(41H NORTH MEDIUM CHANNEL EXCEEDS 100 COUNTS)	0006690
	AST(6)=F2	0006700
	RATE=0.	0006710
	GO TO 59	0006720
56	WRITE(11,57)	0006730
57	FORMAT(41H NORTH COURSE CHANNEL EXCEEDS 100 COUNTS)	0006740
	AST(6)=F2	0006750
	RATE=0.	0006760
	GO TO 59	0006770
804	WRITE(11,805)	0006780
805	FORMAT(27H DATA WILL NOT LOBE ASSIGN)	0006790
	WRITE(13,341)IB1,CSIA,STATIO(L)	0006800
	WRITE(13,348)	0006810
348	FORMAT(1H+,29X,'WILL NOT LOBE ASSIGN')	0006820
	KZ=K-1	0006830
	GO TO 78	0006840
	EW AMBIGUITY LOBE ASSIGN.	0006850
207	SL=.015	0006860
	K=JK-1	0006870
	DO 70 N=1,K	0006880
	IF(TIM(N+1)-TIM(N))72,72,71	0006890
71	IF(TIM(N+1)-TIM(N)-(5.*TILI))70,70,74	0006900
70	CONTINUE	0006910
	K=JK	0006920
	CALL LOBASN(TIM,K,EWMD,RATE,ITD)	0006930
	IF(ITD.GE.100)GO TO 804	0006940
	CALL LOBASN(TIM,K,EWCD,RATE,ITD)	0006950
	IF(ITD.GE.100)GO TO 804	0006960
	CALL LSQUA(TIM,ALPHA,EWMD,K,MID,SIA,SL,EWMB,EWMC,SM,ENA,EOA)	0006970
	EWMA=ALPHA+EWMD(MID)	0006980
	EWMT=TIM(MID)-.15	0006990
	SA=SIA	0007000
	WRITE(11,643)	0007010
643	FORMAT(83H	
	ALPHA.EWM	RATE
	MID.PT.	SIGMA

	X	BETA	GAMMA		0007020
				WRITE(11,152)ALPHA,MID,RATE,SIA,EWMB,EWMC	0007030
152				FORMAT(X,F14.6,X,I6,X,4(F14.6,X))	0007040
				K=JK	0007050
				CALL LSQUA(TIM,ALPHA,EWCD,K,MID,SIA,SL,EWCB,EWCC,SM,ENB,EOB)	0007060
				EWCA=ALPHA+EWCD(MID)	0007070
				EWCT=TIM(MID)+.05	0007080
				SB=SIA	0007090
				WRITE(11,644)	0007100
644				FORMAT(83H	0007110
	X	BETA	ALPHA.EWC	MID.PT.	RATE
			GAMMA		SIGMA
					0007120
					0007130
					0007140
					0007150
					0007160
					0007170
					0007180
					0007190
					0007200
58					0007210
					0007220
					0007230
					0007240
					0007250
					0007260
					0007270
					0007280
224					0007290
					0007300
227					0007310
					0007320
					0007330
642					0007340
	X	BETA	ALPHA.EWF	MID.PT.	RATE
			GAMMA		SIGMA
					0007350
					0007360
					0007370
153					0007380
					0007390
					0007400
					0007410
					0007420
					0007430
					0007440
					0007450

C

NS AMBIGUITY LOBE ASSIGN.

SL=.015

RATE=0.

K=JK

SM=2.0

CALL LOBASN(TIM,K,NSMD,RATE,ITD)

IF(ITD.GE.100)GO TO 804

CALL LOBASN(TIM,K,NSCD,RATE,ITD)

IF(ITD,GE,100)GO TO 804	0007460
CALL LSQUA(TIM,ALPHA,NSMD,K,MID,SIA,SL,SNMB,SNMC,SM,ENX,EOD)	0007470
SNMA=ALPHA+NSMD(MID)	0007480
SNMT=TIM(MID)+.25	0007490
SD=SIA	0007500
WRITE(11,646)	0007510
646 FORMAT(83H	0007520
X BETA	0007530
ALPHA,NSM	0007540
MID,PT.	0007550
RATE	0007560
SIGMA	0007570
WRITE(11,152)ALPHA,MID,RATE,SIA,SNMB,SNMC	0007580
K=JK	0007590
CALL LSQUA(TIM,ALPHA,NSCD,K,MID,SIA,SL,SNCB,SNCC,SM,ENE,EOD)	0007600
SNCA=ALPHA+NSCD(MID)	0007610
SNCT=TIM(MID)+.45	0007620
SE=SIA	0007630
RATE=((SNMB*ANT/4.)+(SNCB*ANT/3.5))/2.)	0007640
IF(ABS(RATE).LE..05)RATE=0.0	0007650
WRITE(11,647)	0007660
647 FORMAT(83H	0007670
X BETA	0007680
ALPHA,NSC	0007690
MID,PT.	0007700
RATE	0007710
SIGMA	0007720
WRITE(11,152)ALPHA,MID,RATE,SIA,SNCB,SNCC	0007730
NSF LOBE ASSIGN.	0007740
IF(ABS(SD).GT..1)GO TO 54	0007750
IF(ABS(SE).GT..1)GO TO 56	0007760
59 SL=.01	0007770
SM=2.5	0007780
K=JK	0007790
CALL LOBASN(TIM,K,ENSF,RATE,ITD)	0007800
IF(ITD,GE,100)GO TO 804	0007810
CALL LSQUA(TIM,ALPHA,ENSF,K,MID,SIA,SL,SNFB,SNFC,SM,ENF,EOD)	0007820
MIDNS=MID	0007830
SNFT=TIM(MID)	0007840
SNFA=ALPHA+ENSF(MID)	0007850
230 SF=SIA	0007860
ISO=SIA*1000+.5	0007870
229 CALL ZERO(3,ISO,INNO)	0007880
IL=0	0007890
IK=0	0007900
IJ=50.	0007910
IF(ABS(SC).GT..05)GO TO 231	0007920
234 IF(ABS(SF).GT..05)GO TO 235	0007930
GO TO 239	0007940
231 AST(6)=F1	0007950
IK=50	0007960
GO TO 234	0007970
	0007980
	0007990

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235 AST(6)=F2
    IL=50
239 WRITE(11,645)
645 FORMAT(83H
      X      BETA
      ALPHA,NSF      MID.PT.      RATE      SIGMA
      GAMMA )
      WRITE(11,152)ALPHA,MID,RATE,SIA,SNFB,SNFC
      WRITE(11,153)SNMA,SNMT,SNCA,SNCT,RATE
      WRITE(11,777)
C      LOBE ASSIGNED DATA AFTER THE FIT HAS BEEN APPLIED *****
      WRITE(11,641)
641 FORMAT(99H FRA.TIME      EWFINE      O-C      EWMEDM      O-C      EWCORS      O-C
      XNSFINE      O-C      NSMEDM      O-C      NSCORS      O-C )
      K=JK
      DO 790 I=1,K
      T=TIM(I)-EWMT-.15
      AM=EWMA+(EWMB*T)+(EWMC*T**2)
      T=TIM(I)-EWCT+.05
      AN=EWCA+(EWC*B*T)+(EWCC*T**2)
      T=TIM(I)-EWFT
      AO=EWFA+(EWF*B*T)+(EWF*C*T**2)
      T=TIM(I)-SNMT+.25
      AP=SNMA+(SNMB*T)+(SNMC*T**2)
      T=TIM(I)-SNCT+.45
      AQ=SNCA+(SNCB*T)+(SNCC*T**2)
      T=TIM(I)-SNFT
      AR=SNFA+(SNFB*T)+(SNFC*T**2)
      AO=EEWF(I)-AO
      AM=EWMD(I)-AM
      AN=EWCD(I)-AN
      AR=ENSF(I)-AR
      AP=NSMD(I)-AP
      AQ=NSCD(I)-AQ
      WRITE(11,791)TIM(I),EEWF(I),AO,EWMD(I),AM,EWCD(I),AN,ENSF(I),AR,NS
      XMD(I),AP,NSCD(I),AQ
791 FORMAT(X,F7.1,6(X,F7.3,X,F6.3))
790 CONTINUE
      WRITE(11,792)ENA,SA,EOA,ENB,SB,EOB,ENC,SC,EOC
      WRITE(11,793)
      WRITE(11,794)
      WRITE(11,792)ENX,SD,EOD,ENE,SE,EOE,ENF,SF,EOF
792 FORMAT(3(X,I2,4X,F5.3,8X,I2))
793 FORMAT( 67H IN      EWM SIGMA      OT IN      EWC SIGMA      OT IN      EWF
      XSIGMA      OT )
794 FORMAT( 67H IN      NSM SIGMA      OT IN      NSC SIGMA      OT IN      NSF

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C.4

	XSIGMA	OT)		0008340
	ADJUST	TIME TO	EWFINE FITTED TIME	0008350
C	XKFA=	(KFA(L)/1000.)+1DIF		0008360
	XKFB=	(KFB(L)/1000.)+1DIF		0008370
	EW4SEC=	(EWFC*XKFA-EWFB)*XKFA		000838
	SN4SEC=	(SNFC*(EWFT-SNFT-XKFB)+SNFB)*(EWFT-SNFT-XKFB)		000839
	EWFA=	EWFA+EW4SEC		000840
	SNFA=	SNFA+SN4SEC		000841
	EWFB=	EWFB+2.*EWFC*(-XKFA)		0008420
	SNFB=	SNFB+2.*SNFC*(-XKFB)		0008430
	EWMA=	EWMA+EWMB*(EWFT-EWMT)+EWMC*((EWFT-EWMT)**2)		0008440
	EWCA=	EWCA+EWCB*(EWFT-EWCT)+EWCC*((EWFT-EWCT)**2)		0008450
	SNMA=	SNMA+SNMB*(EWFT-SNMT)+SNMC*((EWFT-SNMT)**2)		0008460
	SNCA=	SNCA+SNCB*(EWFT-SNCT)+SNCC*((EWFT-SNCT)**2)		0008470
118	EWFB=	EWFA-CEWF1		0008480
C	PHASE	ANGLE (FITTED) MINUS KS2+KC-KS1		0008490
	EWMB=	EWMA-CEWM		0008500
	EWCB=	EWCA-CEWC		0008510
	SNFB=	SNFA-CNSF1		0008520
	SNMB=	SNMA-CNSM		0008530
	SNCB=	SNCA-CNSC		0008540
C	REMOVE	LOBE INTERGER		0008550
	LDIF=	EWFB		0008560
	EWFB=	EWFB-LDIF		0008570
	LDIF=	EWMB		0008580
	EWMB=	EWMB-LDIF		0008590
	LDIF=	EWCB		0008600
	EWCB=	EWCB-LDIF		0008610
	LDIF=	SNFB		0008620
	SNFB=	SNFB-LDIF		0008630
	LDIF=	SNMB		0008640
	SNMB=	SNMB-LDIF		0008650
	LDIF=	SNCB		0008660
	SNCB=	SNCB-LDIF		0008670
	AB=	EWMB-EWCB		0008680
	LDIF=	AB		0008690
	AB=	AB-LDIF		0008700
	CALL	NORMAL(AB)		0008710
	BC=	SNMB-SNCB		0008720
	LDIF=	BC		0008730
	BC=	BC-LDIF		0008740
	CALL	NORMAL(BC)		0008750
	AB4=	AB*8.		0008760
	BC4=	BC*8.		0008770

AB3=AB*7.	0008780
BC3=BC*7.	0008790
EAB4=AB4-EWMBB	0008800
LDIF=EAB4	0008810
EAB4=EAB4-LDIF	0008820
CALL NORMAL(EAB4)	0008830
EBC4=BC4-SNMBB	0008840
LDIF=EBC4	0008850
EBC4=EBC4-LDIF	0008860
CALL NORMAL(EBC4)	0008870
DE=AB4-EAB4	0008880
FG=BC4-EBC4	0008890
EAB3=AB3-EWCB8	0008900
LDIF=EAB3	0008910
EAB3=EAB3-LDIF	0008920
CALL NORMAL(EAB3)	0008930
EBC3=BC3-SNCBB	0008940
LDIF=EBC3	0008950
EBC3=EBC3-LDIF	0008960
CALL NORMAL(EBC3)	0008970
DE3=AB3-EAB3	0008980
FG3=BC3-EBC3	0008990
CORE=DE+DE3	0009000
CORN=FG+FG3	0009010
COREF=(ANT/7.5)*CORE	0009020
CORNF=(ANT/7.5)*CORN	0009030
FE=COREF-EWFBB	0009040
LDIF=FE	0009050
FE=FE-LDIF	0009060
CALL NORMAL(FE)	0009070
FN=CORNF-SNFB8	0009080
LDIF=FN	0009090
FN=FN-LDIF	0009100
CALL NORMAL(FN)	0009110
EWLOBE=COREF-FE	0009120
SNLOBE=CORNF-FN	0009130
AMBIGUITY ERRORS	0009140
EWMER=4./ANT*EWLOBE-DE	0009150
CALL NORMAL(EWMER)	0009160
EWGER=3.5/ANT*EWLOBE-DE3	0009170
CALL NORMAL(EWGER)	0009180
SNMER=4./ANT*SNLOBE-FG	0009190
CALL NORMAL(SNMER)	0009200
SNCER=3.5/ANT*SNLOBE-FG3	0009210

C

CALL NORMAL(SNCER)	0009220
ABB=AB*2	0009230
ADE=DE/4	0009240
ADE3=DE3/3.5	0009250
ACORE=CORE/7.5	0009260
AEWLOB=EWLOBE/ANT	0009270
WRITE(11,1152)ABB,ADE3,ADE,ACORE,AEWLOB,EWFT	0009280
ABC=BC*2	0009290
AFG=FG3/3.5	0009300
AFG3=FG3/3.5	0009310
AFG=FG/4	0009320
ACORN=CORN/7.5	0009330
ASNLOB=SNLOBE/ANT	0009340
WRITE(11,1152)ABC,AFG3,AFG,ACORN,ASNLOB,SNFT	0009350
FORMAT(6(X,F14.6))	0009360
1152 IF(ANTD(K)-2)650,651,651	0009370
651 WRITE(11,648)	0009380
648 FORMAT(12H POLAR PASS)	0009390
GO TO 652	0009400
650 WRITE(11,649)	0009410
649 FORMAT(17H EQUATORIAL PASS)	0009420
GO TO 652	0009430
652 IAO=2	0009440
IBO=3	0009450
SMITTY=((FREQ(M)/136.)*ANT)	0009460
ACOS=EWLOBE/SMITTY	0009470
BCOS=SNLOBE/SMITTY	0009480
DCOS= 1.-ACOS*ACOS-BCOS*BCOS	000949
IF(DCOS.GE.0.0) DCOS = SQRT(DCOS)	000950
ADOT = EWFB/SMITTY	000951
BDOY = SNFB/SMITTY	000952
IF(DCOS.NE.0.) DDOY = -(ACOS * ADOT + BCOS * BDOY)/DCOS	000953
LL = L	000954
IF(ANT.EQ.57.) LL = L + 17	000955
IPASS(LL) = IPASS(LL) + 1	000956
WRITE(6,1017) ACOS,BCOS,DCOS,ADOT,BDOY,DDOT,IARC,IPASS(LL)	000957
1017 FORMAT(3X,4HL = ,F9.7,3X,4HM = ,F9.7,3X,4HN = ,F9.7,3X,7HDDOT = ,	000958
IF9.7,3X,7HDDOT = ,F9.7,3X,7HNDOT = ,F9.7/X,6HARC = ,I3,3X,	000959
17HPASS = ,I3)	000960
IF(LFILE) GO TO 1042	000961
C WRITE HEADINGS ON FILES	000962
DO 1040 LF=1,16	000963
LX=(LF-1)*2+20	000964
WRITE(LX,1051) STATIO(LF),KSTA(LF)	000965


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DELTA=TFOVEW(IFOV, IFIX)-TFOVNS(IFOV, IFIX)+XKFB      001010
FOVEW(IFOV, IFIX)=FOVEW(IFOV, IFIX)-DELTA* EWF8 -CEWF1  001011
FOVNS(IFOV, IFIX)=FOVNS(IFOV, IFIX)+DELTA*SNF8 - CNSF1  001012
327 CONTINUE      0010130
CALL FIXUP2(FOVEW(IFOV, 3), EWF(IFOV))      0010140
CALL FIXUP2(FOVNS(IFOV, 3), ENSF(IFOV))      0010150
CALL FIXUP2(FOVEW(IFOV, 2), FOVEW(IFOV, 3))      0010160
CALL FIXUP2(FOVEW(IFOV, 1), FOVEW(IFOV, 2))      0010170
CALL FIXUP2(FOVEW(IFOV, 4), FOVEW(IFOV, 3))      0010180
CALL FIXUP2(FOVEW(IFOV, 5), FOVEW(IFOV, 4))      0010190
CALL FIXUP2(FOVNS(IFOV, 2), FOVNS(IFOV, 3))      0010200
CALL FIXUP2(FOVNS(IFOV, 1), FOVNS(IFOV, 2))      0010210
CALL FIXUP2(FOVNS(IFOV, 4), FOVNS(IFOV, 3))      0010220
CALL FIXUP2(FOVNS(IFOV, 5), FOVNS(IFOV, 4))      0010230
DO 301 JOUT=1,5      0010240
AACOS(IFOV, JOUT)=FOVEW(IFOV, JOUT)/SMITTY      0010250
BBCOS(IFOV, JOUT)=FOVNS(IFOV, JOUT)/SMITTY      0010260
301 CONTINUE      0010270
N5=5*NBK      0010280
IPAGE=1      0010290
IGMT=TIM(1)      0010300
WRITE(6,310)IPAGE, IBL, IGMT      0010310
IPAGE=0      0010320
WRITE(6,302)IPAGE, (MSGR(I), I=1,80)      0010330
IPAGE=1      0010340
WRITE(6,306)KKSAD, STATIO(L), IDAYD(1), N5      0010350
306 FORMAT('OSATELLITE = ', I6, 7X, 'STATION = ', A6, 6X, 'DAY = ', I3, 7X,
1'DATA CARDS = ', I3/)      0010360
WRITE(6,308)      0010370
308 FORMAT(6X, 'EWF TIME', 2X, 'EWF COUNT', 6X, 'L', 9X, 'NSF TIME', 2X, 'NSF C
OUNT', 6X, 'M')      0010380
307 FORMAT(' SATELLITE = ', I6, 7X, 'STATION = ', A6, 6X, 'DAY = ', I3, 7X,
1'DATA CARDS = ', I3)      0010390
309 FORMAT(6X, 'EWF TIME', 2X, 'EWF COUNT', 6X, 'L', 9X, 'NSF TIME', 2X, 'NSF C
OUNT', 6X, 'M')      0010400
310 FORMAT(11, 'S', '/', ' DATA MESSAGE NO. ', I5, 6X, 'GMT IN SEC. ', I5/)      0010410
311 FORMAT( ' S', '/', ' DATA MESSAGE NO. ', I5, 6X, 'GMT IN SEC ', I5)      0010420
DO 303 IOUT=1, NBK      0010430
DO 303 JOUT=1, 5      0010440
KLM=(IOUT-1)*5+JOUT      0010450
303 WRITE(6,304)TFOVEW(IOUT, JOUT), FOVEW(IOUT, JOUT), AACOS(IOUT, JOUT),
* TFOVEW(IOUT, JOUT), FOVNS(IOUT, JOUT), BBCOS(IOUT, JOUT), KLM      0010460
304 FORMAT(2(4X, F10.5, 2X, F9.5, 2X, F8.5), 6X, I4)      0010470
JOY=JULDY(IYEAR, IDAYD(1))      0010480
                                0010490
                                0010500
                                001051
                                0010520
                                0010530

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L = LL
IF(JDY.LT.JUDY(L))GO TO 331
IF((JDY.EQ.JUDY(L)).AND.(IGMT.LT.JUSEC(L)))GO TO 331
JUSEC(L)=IGMT
JUDY(L)=JDY
DNAP(1)=0.00
DNAP(2) = IARC
DNAP(3)=KSTA(L)
DNAP(4)=IPASS(L)
WRITE(12)(DNAP(I),I=1,6)
WRITE (19) DNAP
JDAY=JDY
DNAP(1)=JDAY
JDAY1=1
I=2*N5
WRITE(14,353)IB1,I,KSTA(L),STATIO(L),IARC,IPASS(L),JDAY,IGMT
*,ACOS,BCOS,DCOS,ADCT,BDOT,DDOT
353 FORMAT (3X,15,16,2X,13,2X,A6,14,15,2X,15,16,6(2X,F8.6))
DO 332 IOUT=1,NBRK
DO 332 JOUT=1,5
DNAP(2)=IGMT+TFOVEW(IOUT,JOUT)
DNAP(3)=AACOS(IOUT,JOUT)
DNAP(4)=BBCOS(IOUT,JOUT)
335 IF(DNAP(2).LT.86400.00)GO TO 333
JDAY=JDAY+JDAY1
DNAP(1)=JDAY
JDAY1=0
DNAP(2)=DNAP(2)-86400.00
333 WRITE(12)(DNAP(I),I=1,6)
332 CONTINUE
I=DNAP(2)
XNAP(1)=JULDY(IYEAR,IDAYD(MID))
XNAP(2)=TIM(MID)
XNAP(3)=ACOS
XNAP(4)=BCOS
WRITE(19) XNAP
IF(IARCS.LT.0) GO TO 1995
II = 1
IF(IARCS.NE.IARC) II = 2
WRITE(7,2501) STATIO(LS),POLEQ,IARCS,JS,IPASSS,II
1995 IF(ANT.EQ.57.) GO TO 2000
POLEQ = EQ
JS = L + L - 1
GO TO 2100

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2000	POLEQ = POL	001098
	JS = L + L - 34	001099
2100	TIMSTR = IGMT + TFOVEW(1,1) - 1.	001100
	TIMEND = IGMT + TFOVEW(NBRK,5) + 1.	001101
	WRITE(7,2500) I201,STATIO(L),POLEQ,IARC,JS,IPASS(L),	001102
*	IYEAR,IDAYD(1),TIMSTR	001103
	WRITE(7,2500) I202,STATIO(L),POLEQ,IARC,JS,IPASS(L),	001104
*	IYEAR,IDAYD(1),TIMEND	001105
	IARCS = IARC	001106
	LS = L	001107
	IPASSS = IPASS(L)	001108
2500	FORMAT(I3,2X,A6,A2,3I3,6X,I3,' 1',I3,10X,F9.1)	001109
2501	FORMAT('999',2X,A6,A2,4I3)	001110
	GO TO 94	001111
331	CONTINUE	001112
	WRITE(I3,341)IB1,CSTA,STATIO(L)	001113
341	FORMAT(' DATA MESSAGE NC.',I5,38X,'STATION NO.',I3,6X,'STATION NAM	001114
	IE',A6)	001115
	WRITE(I3,342)	001116
342	FORMAT(IH+,26X,'MESSAGE OUT OF SEQUENCE')	001117
	GO TO 94	001118
30	WRITE(6,31)	001119
31	FORMAT(17H CAL.LINE PARITY)	001120
	WRITE(I3,341)IB1,CSTA,STATIO(L)	001121
	WRITE(I3,343)	001122
343	FORMAT(IH+,33X,'CAL. LINE PARITY')	001123
	GO TO 94	001124
32	WRITE(11,33)	001125
33	FORMAT(24H DATA PARITY,NO MSG.END)	001126
	GO TO 621	001127
604	CONTINUE	001128
	WRITE(I3,341)IB1,CSTA,STATIO(L)	001129
	WRITE(I3,344)	001130
344	FORMAT(IH+,34X,'CAL. LINE ERROR')	001131
	DO 60 JZ=1,60	001132
	JY=JZ	001133
	IF(JY.EQ.32)GO TO 94	001134
61	READ(9,601,END=902,ERR=61)(DATA(I),I=1,65)	001135
	IF(CATA(1).EQ.IAMP)GO TO 94	001136
	IF(DATA(10).EQ.SPX)GO TO 62	001137
	GO TO 64	001138
62	IF(CATA(30).EQ.SPX)GO TO 63	001139
	GO TO 64	001140
63	IF(DATA(50).EQ.SPX)GO TO 39	001141

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64 WRITE( 6,660)(DATA(I),I=1,65) 0011420
660 FORMAT(X,65A1) 0011430
60 CONTINUE 0011440
GO TO 94 0011450
65 K=JK-1 0011460
DO 66 I=1,K 0011470
WRITE( 6,67)HORD(I),MIND(I),SECD(I),EEWF(I),EWMCD(I),ENSF(I 0011480
X),NSMD(I),NSCD(I),AMTD(I),IDAYD(I),STAD(I) 0011490
67 FORMAT(X,I2,I2,I2,X,(6(F10.6,X)),I2,X,I3,X,I2,X) 0011500
66 CONTINUE 0011510
GO TO 94 0011520
777 FORMAT(1H1) 0011530
1 CONTINUE 001154
DNAP(1) = -1.00 001155
DNAP(2) = 0.00 001156
DNAP(4) = 0.00 001157
WRITE(12) (DNAP(I), I = 1,6) 001158
WRITE(19) DNAP 001159
END FILE 19 001160
REWIND 19 001161
3 WRITE (6,990) 001162
WRITE(11,990) 0011630
WRITE(13,340)(MSGR(I),I=1,80) 0011640
WRITE(13,349) 0011650
349 FORMAT(3X,'SUMMARY OF PASSES',//3X,'STATION NO.',9X,'STATION NAME', 0011660
113X,'PASSES',14X,'JUL DAY',17X,'SEC') 0011670
II = 3 001168
WRITE(7,2501) STATIO(LS),POLEQ,IARCS,JS,IPASSS,II 001169
DO 350 J=1,17 001170
I=J 0011710
DO 350 JJ=1,2 0011720
IPASST(I) = IPASST(I) + IPASS(I) 001173
WRITE(13,351)KSTA(I),STATIO(I),IPASST(I),JUDY(I),JUSEC(I) 001174
I=I+17 001175
350 CONTINUE 0011760
351 FORMAT(4X,I5,I7X,A6,I5X,I5,2(17X,I5)) 0011770
WRITE(13,990) 0011780
END FILE 12 0011790
REWIND 12 0011800
990 FORMAT(50X,'JOB IS COMPLETE',2(/1H1)) 0011810
DO 355 J=1,2 0011820
N1=17*J 001183
N=N1-16 001184
WRITE(13,336)A1,N,(IPASS(I),I=N,N1) 0011850

```

355	CONTINUE	0011860
	DO 356 J=1,2	0011870
	N1=17*J	001188
	N=N1-16	001189
	WRITE(13,336)A2,N,(JUDY(I),I=N,N1)	0011900
356	CONTINUE	0011910
	DO 357 J=1,2	0011920
	N1=17*J	001193
	N=N1-16	001194
	WRITE(13,336)A3,N,(JUSEC(I),I=N,N1)	0011950
357	CONTINUE	0011960
336	FORMAT(1X,A5,1815)	001197
	STOP	0011980
321	WRITE(6,322)	0011990
322	FORMAT('1 *STOP* NO DATA IN FT08 FILE')	0012000
	STOP	0012010
	END	0012020
	SUBROUTINE FIXUP1(EWLOBE,EWF,JOE)	0012030
	FOVEWF=EWLOBE-EWF	0012040
	JOE=FOVEWF	0012050
	IF(ABS(FOVEWF-JOE)-0.5)1,1,2	0012060
2	IF(FOVEWF-JOE)3,3,4	0012070
3	JOE=JOE-1	0012080
	RETURN	0012090
4	JOE=JOE+1	0012100
1	RETURN	0012110
	END	0012120
	SUBROUTINE FIXUP2(EWMID,EWF)	0012130
	IF(EWF-LT.0.0) EWMID=CWMID-1.0	0012140
	DIFF=EWF-EWMID	0012150
	NDIFF=DIFF	0012160
	IF(ABS(DIFF-NDIFF)-0.5)1,1,2	0012170
1	EWMID=EWMID+NDIFF	0012180
	RETURN	0012190
2	IF(DIFF)3,3,4	0012200
3	NDIFF=NDIFF-1	0012210
	GO TO 1	0012220
4	NDIFF=NDIFF+1	0012230
	GO TO 1	0012240
	END	0012250
	SUBROUTINE LOBASN(TEM,I,A,RATE,L)	0012260
	DIMENSION A(31),TEM(31)	0012270
	K=I-1	0012280
	IF(RATE-GT.0.)A(1)=A(1)+1.	0012290

```

IF(RATE.LT.0.)A(1)=A(1)-1.
DO 10 J=1,K
L=0
JJ=J+1
DELTA=RATE*(TEM(JJ)-TEM(J))
11 X=A(JJ)-A(J)
L=L+1
IF(L.GE.100)GO TO 12
IF(ABS(DELTA-X)-.500)10,10,6
6 IF(DELTA)4,5,3
4 A(JJ)=A(JJ)-1
GO TO 11
3 A(JJ)=A(JJ)+1
GO TO 11
5 IF(X)3,10,4
10 CONTINUE
12 RETURN
END
SUBROUTINE LSQUA(T,ALPHA,XY,ITO,L,SIGMA,F,BETA,GAMMA,SM,INN,IOT)
DIMENSION B(3,4),A(3,4),T(32),XY(32)
DO 1 I=1,3
DO 1 J=1,4
1 A(I,J)=0.0
L=(ITO+1)/2
A(1,1)=ITO
INN=ITO
DELSQ=0.
DO 10 I=1,ITO
RAPPA=XY(I)-XY(L)
TAU=T(I)-T(L)
A(1,2)=A(1,2)+TAU
A(1,3)=A(1,3)+TAU**2
A(1,4)=A(1,4)+RAPPA
A(2,3)=A(2,3)+TAU**3
A(2,4)=A(2,4)+RAPPA*TAU
A(3,3)=A(3,3)+TAU**4
A(3,4)=A(3,4)+RAPPA*TAU**2
10 DELSQ=RAPPA**2+DELSQ
67 A(2,2)=A(1,3)
A(2,1)=A(2,4)
A(3,1)=A(3,4)
N=1
DO20 K=1,3
N=N+1

```

```

0015 J=N,4
15 B(K,J)=A(K,J)/A(K,K)
IF(N-4)12,21,11
12 DO20I=N,3
DO20J=I,4
20 A(I,J)=A(I,J)-A(K,I)*B(K,J)
21 GAMMA=B(3,4)
BETA=B(2,4)-GAMMA*B(2,3)
ALPHA =B(1,4)-BETA*B(1,2)-GAMMA*B(1,3)
N=A(1,1)
SIGMA=((DELSQ-ALPHA*A(1,4)-BETA*A(2,1)-GAMMA*A(3,1))/A(1,1))
IF(SIGMA)70,71,71
70 SIGMA=0.
71 SIGMA=SQRT(SIGMA)
IF(SIGMA-F )59,59,35
35 DO61I=1,3
DO61J=1,4
61 A(I,J)=0.0
DELSQ=0.0
DO65I=1,ITO
RAPPA=XY(I)-XY(L)
TAU= T(I)-T(L)
R=RAPPA-ALPHA-BETA*TAU-GAMMA*TAU**2
IF(R)2,3,3
2 R=-R
3 IF(R-SM*SIGMA)32,32,65
32 A(1,1)=A(1,1)+1.
A(1,2)=A(1,2)+TAU
A(1,3)=A(1,3)+TAU**2
A(1,4)=A(1,4)+RAPPA
A(2,3) =A(2,3)+TAU**3
A(2,4)=A(2,4)+RAPPA*TAU
A(3,3) =A(3,3) +TAU**4
A(3,4)=A(3,4)+RAPPA*TAU**2
DELSQ=RAPPA**2+DELSQ
65 CONTINUE
IF(A(1,1)-5)59,66,66
66 IF(A(1,1)-N )67,59,67
59 ITO=A(1,1)
IOI=ITO
RETURN
11 WRITE( 6,7)
7 FORMAT(30H THIS MSG. HAS EXCESSIVE NOISE)
RETURN

```



```

0013180
0013190
0013200
0013210
0013220
0013230
0013240
0013250
0013260
0013270
0013280
0013290
0013300
0013310
0013320
0013330
0013340
0013350
0013360
0013370
0013380
0013390
0013400
0013410
0013420
0013430
0013440
0013450
0013460
0013470
0013480
0013490
0013500
0013510
0013520
0013530
0013540
0013550
0013560
0013570
0013580
0013590
0013600
0013610

END
SUBROUTINE NORMAL(X)
  IF(X)113,114,115
  113 IF(ABS(X)-.5)114,114,116
  116 X=X+1.0
  GO TO 114
  115 IF(ABS(X)-.5)114,114,117
  117 X=X-1.0
  114 RETURN
END
SUBROUTINE ZERO(N,IIN,AREA)
  DIMENSION DIV(7)
  INTEGER DIV
  LOGICAL*1 PLUS,MINUS,ASK,IC(10),AREA(80)
  DATA PLUS,MINUS,ASK,IC(1),IC(2),IC(3),IC(4),IC(5),IC(6),IC(7),IC(8)
  X,IC(9),IC(10)/Z40,Z60,Z5C,ZF0,ZF1,ZF2,ZF3,ZF4,ZF5,ZF6,ZF7,ZF8,ZF9
  X/
  DATA DIV(1),DIV(2),DIV(3),DIV(4),DIV(5),DIV(6),DIV(7)/1000000,1000
  X00,10000,1000,100,10,1/
  AREA(1)=PLUS
  IF(IIN)1,2,2
  1 AREA(1)=MINUS
  IIN=IABS(IIN)
  2 IJ=9-N
  K=2
  J=N-1
  DO 4 I=1,J
    ITEMP=IIN/DIV(IJ)
    IF(ITEMP.LE.9.)GO TO 6
    AREA(K)=ASK
    GO TO 5
  6 AREA(K)=IC(ITEMP+1)
  5 IIN=IIN-(ITEMP*DIV(IJ))
  IJ=IJ+1
  K=K+1
  4 CONTINUE
  RETURN
END
INTEGER FUNCTION JULDY(Y,D)
  INTEGER Y,D
  L=(Y-50+1)/4
  JULDY=L*366
  JULDY=(Y-50-L)*365+JULDY+D-1
  RETURN

```

END

0013620

1371 CARDS

**A-2.4 A PROGRAM FOR MERGING TWO OPTICAL DATA TAPES
(IN A GEOS FORMAT) INTO A SINGLE TAPE - SAMPLE JCL**

PROGRAM FOR COMBINING TWO GEOS-FCRMATED DATA TAPES
FOR USE BY OPTICAL PREPROCESSOR PROGRAM

```

REAL*8 TAPE
INTEGER*2 ID, I10
LOGICAL*1 A, B, AA, BB, ZERC, BLANK, AA1, BB1, I9
DIMENSION A(78), B(78), AA(2), BB(2)
EQUIVALENCE (A(17), IYMA), (A(21), IDHA), (A(25), IMSA), (A(29), IFSA),
1(B(5), ID), (B(17), IYMB), (B(21), IDHB), (B(25), IMSB), (B(29), IFSB),
2(AA1, AA(1)), (BB1, BB(1)))
COMMON TAPE, IFILE, IYM, INIT, LINE
DATA ZERO, BLANK / 0., ' ' /
DATA I9, I10 / 9, 10 /
INIT = 0
READ (5, 900) TAPE, IFILE
READ (1, 1000, END = 300) AA, A
READ (1, 1000, END = 300) AA, A
READ (1, 1000, END = 300) AA, A
DO 5 I = 23, 32
IF (A(I).EQ.BLANK) A(I) = ZERO
5 CONTINUE
10 READ (2, 1000, END = 400) BB, B
IF (ID.NE.I10) GO TO 10
DO 15 I = 23, 32
IF (B(I).EQ.BLANK) B(I) = ZERO
15 CONTINUE
C
IF (IYMA - IYMB) 20, 20, 30
20 CALL RESET (IYMA)
GO TO 35
30 CALL RESET (IYMB)
35 INIT = -1
40 CONTINUE
IF (IYMA - IYMB) 100, 50, 200
50 IF (IDHA - IDHB) 100, 60, 200
60 IF (IMSA - IMSB) 100, 70, 200
70 IF (IFSA, GT, IFSB) GO TO 200
100 CONTINUE
IF (IYMA, GT, IYM) CALL RESET (IYMA)
WRITE (3, 1000) AA, A

```


PROGRAM FOR COMBINING TWO GEOS-FCRMATED DATA TAPES
FOR USE BY OPTICAL PREPROCESSOR PROGRAM

```

REAL*8 TAPE
INTEGER*2 IO, I10
LOGICAL*1 A, B, AA, BB, ZERC, BLANK, AA1, BB1, I9
DIMENSION A(78), B(78), AA(2), BB(2)
EQUIVALENCE (A(17), IYMA), (A(21), IDHA), (A(25), IMSA), (A(29), IFSA),
1(B(5), ID), (B(17), IYMB), (B(21), IDHB), (B(25), IMSB), (B(29), IFSB),
2(AA1, AA(1)), (BB1, BB(1))
COMMON TAPE, IFILE, IYM, INIT, LINE
DATA ZERO, BLANK / 0., ' ' /
DATA I9, I10 / 9., 10. /
INIT = 0
READ (5, 900) TAPE, IFILE
READ (1, 1000, END = 300) AA, A
READ (1, 1000, END = 300) AA, A
READ (1, 1000, END = 300) AA, A
DO 5 I = 23, 32
IF (A(I).EQ.BLANK) A(I) = ZERO
5 CONTINUE
10 READ (2, 1000, END = 400) BB, B
IF (ID.NE.I10) GO TO 10
DO 15 I = 23, 32
IF (B(I).EQ.BLANK) B(I) = ZERO
15 CONTINUE
C
IF (IYMA - IYMB) 20, 20, 30
20 CALL RESET (IYMA)
GO TO 35
30 CALL RESET (IYMB)
35 INIT = -1
40 CONTINUE
IF (IYMA - IYMB) 100, 50, 200
50 IF (IDHA - IDHB) 100, 60, 200
60 IF (IMSA - IMSB) 100, 70, 200
70 IF (IFSA.GT.IFSB) GO TO 200
100 CONTINUE
IF (IYMA.GT.IYM) CALL RESET (IYMA)
WRITE (3, 1000) AA, A

```

```

WRITE (6,1010) AA,A
LINE = LINE - 1
IF (LINE.LT.0) CALL TITLE
READ (1,1000,END = 300) AA,A
IF(AA1.EQ.19) GO TO 300
DO 150 I = 23,32
IF (A(I).EQ.BLANK) A(I) = ZERO
150 CONTINUE
GO TO 40
200 IF (IYMB.GT.IYM) CALL RESET (IYMB)
WRITE (3,1000) BB,B
WRITE (6,1010) BB,B
LINE = LINE - 1
IF (LINE.LT.0) CALL TITLE
210 READ (2,1000,END = 400) BB,B
IF(BB1.EQ.19) GO TO 400
IF (ID.NE.110) GO TO 210
DO 215 I = 23,32
IF (B(I).EQ.BLANK) B(I) = ZERO
215 CONTINUE
GO TO 40
300 IF (IYMB.GT.IYM) CALL RESET (IYMB)
WRITE (3,1000) BB,B
WRITE (6,1010) BB,B
LINE = LINE - 1
IF (LINE.LT.0) CALL TITLE
310 READ (2,1000,END = 500) BB,B
IF(BB1.EQ.19) GO TO 500
IF (ID.NE.110) GO TO 310
GO TO 300
400 IF (IYMA.GT.IYM) CALL RESET (IYMA)
WRITE (3,1000) AA,A
WRITE (6,1010) AA,A
LINE = LINE - 1
IF (LINE.LT.0) CALL TITLE
READ (1,1000,END = 500) AA,A
IF(AA1.EQ.19) GO TO 500
GO TO 400
500 CONTINUE
END FILE 3
REWIND 1
REWIND 2
REWIND 3
WRITE (6,1040)

```


// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),VOL=SER=1666H
//GO.FT03F001 DD UNIT=2400-9,LABEL=(12,BLP),DISP=(NEW,PASS),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200,DEN=2),VOL=SER=3826F
//GO.FT03F002 DD UNIT=2400-9,LABEL=(13,BLP),DISP=(NEW,DELETE),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200,DEN=2),VOL=SER=3826F

//GO.DATAS DD *

3826F

12

/*

0140 CARDS

A-2.5 OPTICAL PREPROCESSING PROGRAM - SAMPLE JCL

C	1	
C	2	
C	3	
C	4	
C	5	
C	6	IMPLICIT REAL*8 (A-H,O-Z)
C	7	
C	8	
C	9	DIMENSION A(13),NOSTA(3C),NONAME(30),C(80),MONTH(12)
C	10	
C	11	COMMON/W/ TIM(49,30),RA(49,30),DEC(49,30),STNAM(30),TPASS,
C	12	IJDAYA(30),NUM(30),NRCRDER(30),IYR1,IYR2,IMOI,IDA1,IDA2,JDAY1,
C	13	IJDAY2,IARC,IARCS,ISIA(3C),JSTA(3C),NPASS(30),KSTA(30),KEY4,K,JS
C	14	COMMON /M/ TIM2
C	15	
C	16	
C	17	
C	18	THE NUMBERS IN ARRAY MONTH ARE THE DAY NUMBERS OF THE LAST DAY OF
C	19	THE PRECEDING MONTH. THE DAY NUMBERS ARE OBTAINED BY NUMBERING
C	20	THE DAYS OF THE YEAR CONSECUTIVELY STARTING WITH DAY NUMBER ZERO
C	21	ON 1 JANUARY.
C	22	
C	23	DATA MONTH/-1,30,58,89,119,150,180,211,242,272,303,333/
C	24	DATA MINUS/0-0/
C	25	
C	26	
C	27	TORBT IS USED BY THE PROGRAM TO SEPARATE ORBITS. OBSERVATIONS
C	28	(FOR ANY ONE STATION) SEPARATED BY MORE THAN TORBT SECONDS ARE
C	29	REGARDED AS BELONGING TO DIFFERENT ORBITS.
C	30	TPASS IS USED BY THE PROGRAM TO SEPARATE PASSES. A PASS IS
C	31	REGARDED AS CONSISTING OF THE OBSERVATIONS OF ONE PHOTOGRAPHIC
C	32	PLATE. OBSERVATIONS(FOR ANY ONE STATION) SEPARATED BY MORE THAN
C	33	TPASS SECONDS ARE REGARDED AS BELONGING TO DIFFERENT PASSES.
C	34	DELT IS THE TIME(IN SECONDS) ADDED TO THE OBSERVATION TIME TO
C	35	ACCOUNT FOR SATELLITE FLASH BUILD-UP.
C	36	NMAX IS THE MAXIMUM NUMBER OF OBSERVATIONS THAT THE PROGRAM
C	37	CAN ACCEPT FOR ANY ONE STATION AND ORBIT.
C	38	
C	39	TORBT = 2700.00
C	40	TPASS = 45.00
C	41	DELT = .000500

NMAX = 49

REWIND 1
READ (1,1080) C
READ (1,1080) C
REWIND 2

SET UP INITIAL CONDITIONS. SETTING KEY4 TO A NEGATIVE NUMBER
ENSURES THAT THE FIRST NAP CARD PUNCHED BY SUBROUTINE DATWT
IS A '201' CARD.
'IS' IS THE NUMBER OF STATIONS FOR WHICH OBSERVATIONS HAVE BEEN
ACCUMULATED BUT NOT YET OUTPUT ON TAPE.
IYMD2 IS THE CURRENT (YEAR,MONTH,DAY). SETTING IT TO A LARGE
NUMBER ENSURES THAT WHEN THE FIRST OBSERVATION PAST THE START TIME
FOR THE ARC IS READ IN, THE PROGRAM WILL ASSUME THAT A NEW DAY HAS
COMMENCED.

IYMD IS, IN GENERAL, THE (YEAR,MONTH,DAY) OF THE LAST OBSERVATION
READ IN. HOWEVER, THE FIRST TIME IT IS USED NOTHING HAS BEEN
READ IN. SETTING IT TO A LARGE NEGATIVE NUMBER ENSURES THAT
THE PROGRAM WILL CONTINUE TESTING FOR THE START OF THE FIRST ARC.
JDAY2 IS THE CURRENT JULIAN DAY NUMBER. SETTING IT EQUAL TO A
LARGE NEGATIVE NUMBER ENSURES THAT THE PREVIOUS JULIAN DAY NUMBER
ALWAYS IS LESS THAN THE CURRENT ONE, SINCE THE NEXT OBSERVATION
READ IN MUST OF NECESSITY HAVE A LARGER JULIAN DAY NUMBER.
TIM2 IS SET TO A LARGE NEGATIVE NUMBER (-1.0+30) TO INITIALIZE
SUBROUTINE TIMCOR.

KEY4 = -1
IS = 0
IYMD2 = 1000000
IYMD = -1000000
JDAY2 = -1000000
IARC = -1000000
TIM2 = -1.0+30
NOLIST = 0

SECATR IS THE CONVERSION CONSTANT FROM ARC-SECONDS TO RADIANS.
SECTTR IS THE CONVERSION CONSTANT FROM HOUR-ANGLE SECONDS TO
RADIANS.

SECATR = .0174532925200/3600.00
SECTTR = SECATR*15.00
WRITE(3,1060)
DO 10 NUMSTA = 1,30

```

86 READ(5,1000) KSTA(NUMSTA),STNAM(NUMSTA),ISTA(NUMSTA),IEND
87 WRITE(3,1001) KSTA(NUMSTA),STNAM(NUMSTA),ISTA(NUMSTA)
88 JSTA(NUMSTA) = ISTA(NUMSTA) - (ISTA(NUMSTA)/10000) * 10000
89 NUM(NUMSTA) = 0
90 IF (IEND.LT.0) GO TO 15
91 10 CONTINUE
92 C NUMBER OF STATIONS EXCEEDS 30
93 WRITE(6,2000)
94 GO TO 700
95 C
96 15 WRITE(3,1070)
97 20 CONTINUE
98 READ(5,1010,END=600) NARC,IYMDB,IHB,IMB,SECB,IYMDE,IHE,IME,SECE
99 WRITE (3,1011) NARC,IYMCB,IHB,IMB,SECB,IYMDE,IHE,IME,SECE
100 BTIME = 3600*IHB + 60*IMB + SECB
101 ETIME = 3600*IHE + 60*IME + SECE
102 C
103 KEY 4 IS INITIALLY NEGATIVE. IT IS SET EQUAL TO 1 AFTER THE FIRST
104 CALL TO SUBROUTINE DATAWT.
105 C
106 C
107 IF (IARC.EQ.NARC) GO TO 100
108 C
109 A NEW ARC HAS COMMENCED. IF DATA HAS BEEN ACCUMULATED FOR THE PRE-
110 VIOUS ARC, BUT NOT YET OUTPUT (IS>0), THEN IT IS OUTPUT NOW.
111 C
112 K = IS
113 IF (K.GT.0) CALL DATAWT
114 IARC = NARC
115 IF A NEW ARC HAS BEEN STARTED SET KEY4 TO 2 IN ORDER THAT
116 SUBROUTINE DATAWT SHOULD PUNCH A '2' IN KEY4 OF THE NEXT NAP '999'
117 CARD
118 C
119 IF (KEY4.GE.0) KEY4 = 2
120 C
121 NOLIST IS THE NUMBER OF NONLISTED STATIONS FOR THE ARC.
122 NUMSTA IS THE NUMBER OF LISTED STATIONS (CONSTANT FOR THIS RUN).
123 C
124 IF (NCLIST.GT.0) WRITE(6,2020) (NONAME(I),NOSTA(I),I=1,NOLIST)
125 NOLIST = 0
126 DO 40 I = 1,NUMSTA
127 NPASS(I) = 0
128 40 CONTINUE
129 WRITE(12,3000) IARC

```

C		130
C	READ DATA TAPE TILL THE TIME OF OBSERVATION IS PASSED THE START	131
C	TIME FOR THE ARC, THEN GO TO 200. (IYMD IS INITIALIZED TO A	132
C	LARGE NEGATIVE NUMBER.)	133
C	100 CONTINUE	134
C	IF (IYMD-IYMD8) 110, 120, 200	135
C	110 READ(1, 1020, END=110) A, NSIA, IYMD, IH, IM, SEC, NHR, MIN, RSEC, NSIGN,	136
C	INDEG, NMIN, DSEC, NRED	137
C	GO TO 100	138
C	120 TIME = IH*3600 + IM*60 + SEC	139
C	IF (TIME.LT.BTIME) GO TO 110	140
C		141
C	200 CONTINUE	142
C		143
C	IF THE TIME OF OBSERVATION IS PASSED THE END TIME FOR THE ARC GO	144
C	TO 20, OTHERWISE PROCEED TO 220.	145
C		146
C	IF (IYMD-IYMD8) 220, 210, 20	147
C	210 IF (TIME.GT.EIME) GO TO 20	148
C		149
C	220 CONTINUE	150
C		151
C	IYMD2 IS THE CURRENT (YEAR, MONTH, DAY). IT IS INITIALIZED TO A LARGE	152
C	POSITIVE NUMBER.	153
C		154
C	TIME = TIME + DELT	155
C	IF (IYMD.EQ.IYMD2) GO TO 270	156
C	IF (IS.LE.0) GO TO 260	157
C		158
C	NORCER IS AN ARRAY OF STATION NUMBERS FOR WHICH OBSERVATIONS HAVE	159
C	BEEN ACCUMULATED. THE STATIONS HAVE BEEN ARRANGED IN A SEQUENCE	160
C	SUCH THAT IF I<J THEN THE TIME OF THE FIRST ACCUMULATED (BUT NOT	161
C	YET OUTPUT) OBSERVATION FOR STATION NORDER(I) PRECEDES THAT FOR	162
C	STATION NORDER(J).	163
C		164
C	JDAY1 IS THE JULIAN DAY PRECEDING THE CURRENT ONE (JDAY2). JDAYA(L)	165
C	IS THE JULIAN DAY OF THE FIRST OBSERVATION OF STATION NUMBER L.	166
C		167
C	DO 230 K = 1, IS	168
C	L = NORDER(K)	169
C	IF (JDAYA(L).GT.JDAY1) GO TO 240	170
C	230 CONTINUE	171
C	K = IS	172
C	GO TO 250	173

240 K = K - 1

174

C

K IS THE NUMBER OF OBSERVATIONS IN ARRAY NORDEK FOR WHICH THE DAY
OF THE FIRST OBSERVATION PRECEDES THE CURRENT DAY, WHICH HAS JUST
COME TO AN END. THE OBSERVATIONS FOR THOSE STATIONS ARE OUTPUT.

175
176
177
178

C
C
C
C

250 IF (K.GT.0) CALL DATANT

179

260 CONTINUE

180

JDAY1 = JDAY2

181

IYR1 = IYR2

182

IMO1 = IMO2

183

IDA1 = IDA2

184

IYMU2 = IYMD

185

IYR2 = IYMD/10000

186

IMU2 = IYMD/100 - 100*IYR2

187

IDA2 = IYMD - 10000*IYR2 - 100*IMO2

188

COMPUTE JULIAN DAY NUMBER

189

LEAPYR = 49

190

IF (IMO2.GT.2) LEAPYR = 48

191

JDAY2 = (IYR2 - 50)*365 + (IYR2 - LEAPYR)/4 + MONTH(IMO2) + IDA2

192

193

C

270 CONTINUE

194

DO 280 I = 1, NUMSTA

195

IF (NSTA.EQ.ISTA(I)) GO TO 290

196

280 CONTINUE

197

IF (NCLIST.LE.0) GO TO 284

198

DO 282 I = 1, NOLIST

199

IF (NSTA.EQ.NONAME(I)) GO TO 286

200

282 CONTINUE

201

IF (NCLIST.GE.30) GO TO 450

202

284 NOLIST = NOLIST + 1

203

NOSTA(NOLIST) = 1

204

NONAME(NOLIST) = NSTA

205

GO TO 320

206

286 NOSTA(I) = NOSTA(I) + 1

207

GO TO 320

208

209

290 RADRA = (NHR*3600 + MIN*60 + RSEC)*SECTTR

210

RADDEC = (NDEG*3600 + NMIN*60 + DSEC)*SECATR

211

IF (NSIGN.EQ.MINUS) RADDEC = -RADDEC

212

213

C

300 CONTINUE

214

N = NUM(I) + 1

215

IF (N.GT.1) GO TO 340

216

217

C	FIRST POINT IN STATION-OBSERVATION ARRAY	218
	JDAYA(I) = JDAY2	219
	IS = IS + 1	220
	NORDER(IS) = I	221
	310 CONTINUE	222
	IF (N.LE.NMAX) GO TO 315	223
	WRITE(6,2030) SINAM(I), ISTA(I)	224
	GO TO 700	225
C		226
	315 CONTINUE	227
	TIM(N,I) = TIME	228
	RA(N,I) = RADRA	229
	DEC(N,I) = RADDEC	230
	NUM(I) = N	231
C		232
	320 READ(1,1020,END=320) A,NSTA,IYMD,IH,IM,SEC,NHR,MIN,RSEC,NSIGN,	233
	INDEG,NMIN,DSEC,NREQ	234
	TIME = IH*3600 + IM*60 + SEC	235
	GO TO 200	236
C		237
	340 CONTINUE	238
	TIMDIF = (JDAY2 - JDAYA(I))*86400 + TIME - TIM(1,I)	239
	IF (TIMDIF.LT.TORBT) GO TO 310	240
	DO 350 K = 1,IS	241
	IF (NORDER(K).EQ.I) GO TO 360	242
	350 CONTINUE	243
	360 CALL DATAT	244
	GO TO 300	245
C		246
	450 CONTINUE	247
	WRITE(6,2010) NONAME,NSTA	248
	GO TO 700	249
	600 K = IS	250
	IF (K.GT.0) CALL DATAT	251
	KEY4 = 3	252
	CALL DATAT	253
	IF(NOLIST.GT.0)WRITE(6,2020) (NONAME(I),NSTA(I),I=1,NOLIST)	254
	WRITE(12,1050)	255
	700 CONTINUE	256
	REWIND 1	257
	END FILE 2	258
	REWIND 2	259
	STOP	260
	1000 FORMAT (I5,5X,A8,2X,2I5)	261


```

1001 FORMAT(11X,15,15X,A8,12X,15) 262
1010 FORMAT(15,5X,16,213,D10.0,16,213,D10.0) 263
1011 FORMAT(7X,15,4X,216,13,F9.5) 264
1020 FORMAT(13A1,15,16,212,F6.4,13,12,F5.3,A1,212,F4.2,16) 265
1050 FORMAT(15X,/'JOB CCMPLETED') 266
1060 FORMAT(112X,'STATION',10X,'NUMBER(NAP)',11X,'NAME',16X,'ID'//) 267
1070 FORMAT(110X,'ARC',19X,'START',28X,'STOP',9X,'NUMBER',2(10X,'DATE' 268
1,5X,'HR MN SECONDS')) 269
1080 FORMAT(80A1) 270
2000 FORMAT(15X,'NUMBER OF STATIONS EXCEEDS 30') 271
2010 FORMAT(11,15X,'THE FOLLOWING STATION NUMBERS ARE NOT IN THE TABLE 272
*/3(10(5X,15))/5X,15/15X,'JOB ABORTED') 273
2020 FORMAT(11,15X,'THE FOLLOWING STATION NUMBERS WERE NOT IN THE TABL 274
*/15X,'STATION NUMBER',20X,'NUMBER OF OBSERVATIONS',30(18X,15,27 275
*/15//)) 276
2030 FORMAT(15X,A8,'-',15,5X,'NUMBER OF DATA POINTS EXCEEDS 49') 277
3000 FORMAT(110X,'DATA SUMMARY FOR ARC NUMBER',15/14X,'STATION',6X, 278
*/DATE',7X,'GMT',9X,'PASS',5X,'NUMBER OF DATA',12X,'ID',4X,'NAME',3 279
*/X,'YR MO DA',3X,'HR MN SEC',6X,'NO.',4X,'POINTS FOR ORBIT'//) 280
END 281
SUBROUTINE DATAWT 282
IMPLICIT REAL*8 (A-H,O-Z) 283
COMMON/W/ TIM(49,30),RA(49,30),DEC(49,30),STNAM(30),TPASS, 284
1JDAYA(30),NUM(30),NCRDER(30),1YR1,1YR2,1MO1,1MO2,1DA1,1DA2,JDAY1, 285
1JDAY2,IARC,IARCS,ISTA(30),JSIA(30),NPASS(30),KSTA(30),IT,K,IS 286
COMMON /SAO/ M,N 287
DATA 11,1201,1202,1999/1,201,202,999/ 288
C IT = -1 ON FIRST ENTRY,IT = 1 SUBSEQUENTLY,IT = 3 ON LAST ENTRY 289
C 290
IF (IT.GE.3) GO TO 200 291
DO 100 I = 1,K 292
IF (IT.LT.0) GO TO 10 293
WRITE (7,1000) 1999,SNAME,IARCS,NSTAS,NPASSS,IT 294
10 CONTINUE 295
IT = 1 296
IARCS = IARC 297
M = NORDER(I) 298
SNAME = STNAM(M) 299
NSTAS = KSTA(M) 300
NSTI2 = ISTA(M) 301
NSTA = JSTA(M) 302
WRITE (6,1010) 11,SNAME,ISTA(M),IARC 303
WRITE (6,1020) 304
N = NUM(M) 305

```

```

306 NUM(M) = 0
307 IF((JSTA(M)+20000).EQ.NST12) CALL SAOCOR
308 DO 90 J = 1,N
309 TIMP = TIM(J,M)
310 IF (J.LE.1) GO TO 50
311 TIMDIF = TIMP - TIM(J-1,M)
312 IF (TIMDIF.GT.TPASS) GO TO 40
313 IF (TIMDIF.GE.0.00) GO TO 20
314 IF (TIMDIF IS NEGATIVE THEN THE LAST OBSERVATION HAS BEEN MADE ON
315 THE DAY FOLLOWING THE PREVIOUS OBSERVATION
316 IF((TIMDIF + 86400.00).GT.TPASS) GO TO 40
317 UPDATE DATE TO NEXT DAY WHICH MUST BE DAY 2
318 IYRM = IYR2
319 IMOM = IMO2
320 IDAM = IDA2
321 DDAYM = JDAY2
322
323 20 CONTINUE
324 DELTRA = RA(J,M) - RA(J-1,M)
325 DELDEC = DEC(J,M) - DEC(J-1,M)
326
327 30 CONTINUE
328 IHP = TIMP/3600.00
329 IMP = TIMP/60.00 - 60*IHP
330 SECP = TIMP - 3600*IHP - 60*IMP
331 GO TO 80
332 40 S = SECP + 0.0100
333 WRITE(7,1001) I202,SNAME,IARC,NSTAS,NPASS(M),IYRM,IMOM,IDAM,IHP,
334 1TIMP,S
335 WRITE(7,1000) I999,SNAME,IARC,NSTAS,NPASS(M),IT
336 WRITE (12,1040) NST12,SNAME,IYRM,IMOM,IDAM,IHP,IMP,SECP,NPASS(M)
337 IF (TIMDIF.LT.0.00) GO TO 60
338 GO TO 70
339 50 CONTINUE
340 IF (JDAYA(M).GT.JDAY1) GO TO 60
341 IYRM = IYR1
342 IMOM = IMO1
343 IDAM = IDA1
344 DDAYM = JDAY1
345 GO TO 70
346 60 IYRM = IYR2
347 IMOM = IMO2
348 IDAM = IDA2
349 DDAYM = JDAY2
350 70 CONTINUE
351 DELTRA = 0.00

```

```

350 DELDEC = 0.00
351 IHP = TIMP/3600.00
352 IMP = TIMP/60.00 - 60*IHP
353 SECP = TIMP - 3600*IHP - 60*IHP
354 S = SECP - 0.0100
355 NPASS(M) = NPASS(M) + 1
356 WRITE (7,1001) I201,SNAME,IARC,NSTAS,NPASS(M),IYRM,IMOM,IDAM,IHP,
357 IIMP,S
358 80 CONTINUE
359 WRITE (6,1030) IYRM,IMOM,IDAM,IHP,IMP,SECP,NPASS(M),RA(J,M),
360 IDELTRA,DEC(J,M),DELDEC
361 WRITE(2) NSTA,DDAYM,TIMP,RA(J,M),DEC(J,M)
362 90 CONTINUE
363 S = SECP + 0.0100
364 WRITE(7,1001)I202,SNAME,IARC,NSTAS,NPASS(M),IYRM,IMOM,IDAM,IHP,
365 IIMP,S
366 NPASS = NPASS(M)
367 WRITE (12,1040) NST12,SNAME,IYRM,IMOM,IDAM,IHP,IMP,SECP,NPASS(M),N
368 100 CONTINUE
369 IS = IS - K
370 IF(IS.LE.0) GO TO 130
371 DO 120 I = 1,IS
372 NORDER(I) = NORDER(I + K)
373 120 CONTINUE
374 130 CONTINUE
375 RETURN
376 200 WRITE(7,1000)I999,SNAME,IARCS,NSTAS,NPASSS,IT
377 RETURN
378 1000 FORMAT (I3,2X,A8,4I3)
379 1001 FORMAT (I3,2X,A8,3I3,6X,5I3,F15.3)
380 1010 FORMAT(I1,9X,A8," - ",I5,15X,"ARC NUMBER",I8//)
381 1020 FORMAT(4X,"DATE",7X,"GMT",9X,"PASS",3X,"RIGHT ASCENSION",4X,"DELTA
382 1 RA",9X,"DECLINATION",8X,"DELTA CEC",2X,"YR MO DA",2X,"HR MN SEC",
383 1,5X,"NO.",5X,"(RADIANS)",8X,"(RADIANS)",9X,"(RADIANS)",9X,"(RADIAN
384 1S)"/)
385 1030 FORMAT(X,3I3,I4,I3,F8.4,I4,4(3X,F15.10))
386 1040 FORMAT(10X,15,X,A8,3I3,15,I3,F4.0,I8,8X,I5)
387 END
388 SUBROUTINE TIMCOR
389 IMPLICIT REAL*8(A-H,O-Z)
390 COMMON/T/ TIM,COR,STHETA,CTHETA,ZETA,Z
391 COMMON/M/ TIM2
392 DIMENSION MONTH(12)
393 DATA MONTH/-1,30,58,89,119,150,180,211,242,272,303,333/

```

```

394 DATA TIM2IN /-1.0+30/
395 5 TIMDIF = TIM - TIM2
396 IF (TIMDIF.LE.0.00) GO TO 15
397 10 COR1 = COR2
398 TIM1 = TIM2
399 IYR1 = IYR2
400 IMO1 = IMO2
401 IDA1 = IDA2
402 READ (4,30,END=20) IYR2,IMO2,IDA2,COR2
403 WRITE (3,60) IYR2,IMO2,IDA2,COR2
404 LEAPYR = 49
405 IF (IMO2.GT.2) LEAPYR = 48
406 TIM2 = (IYR2 - 50)*365 + (IYR2 - LEAPYR)/4 + MONTH(IMO2) + IDA2
407 IF (TIM1.LE.TIM2IN) GO TO 10
408 F = (COR2 - COR1)/(TIM2 - TIM1)
409 GO TO 5
410 15 COR = COR2 + F*TIMDIF
411 RETURN
412 20 WRITE (6,50)
413 STOP
414 30 FORMAT (3I2,4X,F10.5)
415 50 FORMAT (X,END OF DATA SET 4,(TIME CORRECTIONS),JOB ABORTED.%)
416 60 FORMAT (90X,3I3,2X,A.1 - UTC = ,F10.5)
417 END
418 SUBROUTINE PRENUT
419 C
420 IMPLICIT REAL*8(C-H,O-Z)
421 C
422 COMMON/T/ DAYS,COR,SHP,CHP,UP,ZP
423 DIMENSION A(23),AS(30),ADP(30),ADE(30),ADELE(23),ADELP(23)
424 C
425 C
426 DATA ADELE/0.,0.,-2.,2.,2.,-2.,3.,3.,0.,5.,7.,8.,0.,0.,0.,-24.,-66
427 *,0.,0.,0.,0.,0.,0./
428 C
429 DATA ADELP/-2.,-3.,3.,-3.,-3.,-4.,4.,-5.,-5.,10.,-10.,-15.,16.,-2
430 *,1.,45.,0.,0.,0.,0.,0.,0.,0.,0.,0.,0./
431 C
432 C
433 DATA ADE/-3.,3.,3.,-2.,3.,3.,3.,0.,-3.,0.,5.,7.,-7.,-10.,0.,11.,-1
434 *,1.,0.,14.,23.,22.,30.,-31.,0.,-50.,0.,0.,183.,0.,0.,0./
435 C
436 DATA ADP/5.,-5.,-5.,6.,-6.,-6.,-6.,6.,7.,-7.,-9.,-13.,14.,19.,25.,
437 *-26.,26.,28.,-32.,-44.,-52.,-57.,58.,60.,114.,-149.,-261.,0.,0.,0.

```

*/		438
C		439
	DATA STRAD,DPLUS/.4848136811D-5,18262.500/	440
	DATA ADR/57.2957795/	441
C		442
C		443
	DD = DPLUS + DAYS	444
	TD = DD/36525.00	445
	AT = TD	446
	ADD = DD/10000.00	447
	ADD2 = ADD * ADD	448
	ELD = 13.064992446500*DD + 296.10460800	449
	CALL PRINCP(ELD,AL)	450
	ELPD = .985600266900*DD + 358.47583300	451
	CALL PRINCP(ELPD,ALP)	452
	EFD = 13.229350449000*DD + 11.25088900	453
	CALL PRINCP(EFD,AF)	454
	DED = 12.190749191400*DD + 350.73748600	455
	CALL PRINCP(DED,AD)	456
	OMEGU = .052953922200*DD - 259.18327500	457
	CALL PRINCP(OMEGU,AMEG)	458
	AL = {AL + (.0006890 + .000000295*ADD) * ADD2}/ADR	459
	ALP = {ALP - (.0000112 + .000000068 * ADD) * ADD2}/ADR	460
	AF = {AF - (.0002407 + .000000007 * ADD) * ADD2}/ADR	461
	AD = {AD - (.0001076 - .000000039 * ADD) * ADD2}/ADR	462
	AMEG = {(0.0001557 + .000000046 * ADD) * ADD2 - AMEG}/ADR	463
	A(23) = AMEG	464
	A(21) = AMEG + AMEG	465
	A(9) = 2. * {AL - AF}	466
	A(16) = AMEG - A(9)	467
	A(5) = 2. * {AF - ALP - AD} + AMEG	468
	A(4) = A(16) + AMEG	469
	A(1) = AL - ALP - AD	470
	A(22) = 2. * {AF - AD + AMEG}	471
	A(20) = ALP	472
	A(19) = ALP + A(22)	473
	A(18) = A(22) - ALP	474
	A(17) = A(22) - AMEG	475
	A(15) = 2. * {AL - AD}	476
	A(14) = 2. * {AF - AD}	477
	A(13) = ALP + ALP	478
	A(12) = ALP + AMEG	479
	A(11) = A(12) + A(12) + A(14)	480
	A(10) = AMEG - ALP	481

A(8) = AMEG - A(15)	482
A(7) = A(10) + A(14)	483
A(6) = A(15) + AMEG	484
A(3) = A(12) + A(14)	485
A(2) = AL - AD	486
AS(30) = 2 * (AF + AMEG)	487
AS(29) = AL	488
AS(28) = AS(30) - AMEG	489
AS(27) = AS(30) + AL	490
AS(26) = AL - AD - AD	491
AS(25) = AS(30) - AL	492
AS(24) = AD + AD	493
AS(23) = AL + AMEG	494
AS(22) = AMEG - AL	495
AS(21) = AS(24) + AS(25)	496
AS(20) = AS(27) - AMEG	497
AS(19) = AS(30) + AS(24)	498
AS(18) = AL + AL	499
AS(17) = AS(27) - AS(24)	500
AS(16) = AS(30) + AS(18)	501
AS(15) = AF + AF	502
AS(14) = AS(22) + AS(15)	503
AS(13) = AS(22) + AS(24)	504
AS(12) = AS(23) - AS(24)	505
AS(11) = AS(14) + AS(24)	506
AS(10) = AS(26) + ALP	507
AS(9) = AS(30) + ALP	508
AS(8) = AL + AS(24)	509
AS(7) = AMEG + AS(24)	510
AS(6) = AS(30) - ALP	511
AS(5) = AS(30) + AS(8)	512
AS(4) = AS(17) + AL	513
AS(3) = AMEG - AS(24)	514
AS(2) = AS(19) - AMEG	515
AS(1) = AS(17) - AMEG	516
ASS16 = AD	517
ASS15 = AS(10) - AL	518
ASS14 = AL - ALP	519
ASS13 = AL - AF - AF	520
ASS12 = AS(16) - AMEG	521
ASS11 = AL + AF + AF	522
ASS10 = AL + ALP	523
ASS9 = AS(30) + ASS14	524
ASS8 = AMEG - AL - AL	525

```

ASS7 = AS(14) - AD - AD 526
ASS6 = AL + AL + AMEG 527
ASS5 = AS(25) - ASS15 528
ASS4 = ASS5 + AL 529
ASS3 = AL + AMEG + AMEG 530
ASS2 = AS(27) + ALP 531
ASS1 = AS(27) + AL + AL 532
ADELP(23) = -172327. - 173.7*AT 533
ADELP(21) = 2088. + 0.2 * AT 534
ADELP(22) = - 12729. - 1.3 * AT 535
ADELP(20) = 1261. - 3.1 * AT 536
ADELP(19) = -497. + 1.2 * AT 537
ADELP(18) = 214. - 0.5 * AT 538
ADELP(17) = 124. + 0.1 * AT 539
ADELP(13) = 16. - 0.1 * AT 540
ADELP(11) = -15. + 0.1 * AT 541
ACELE(23) = 92100. + 9.1 * AT 542
ADELE(21) = - 904. + 0.4 * AT 543
ACELE(22) = 5522. - 2.9 * AT 544
ADELE(19) = 216. - 0.6 * AT 545
ADELE(18) = -93. + 0.3 * AT 546
ADP(20) = -2037. - 0.2 * AT 547
ADP(29) = 675. + 0.1 * AT 548
ADP(28) = -342. - 0.4 * AT 549
ADE(30) = 884. - 0.5 * AT 550
ADE(27) = 113. - 0.1 * AT 551
BDELE = 0. 552
BDELP = 0. 553
DO 100 I = 1,23 554
BDELE = BDELE + ADELE(I) * COS(A(I)) 555
BDELP = BDELP + ADELP(I) * SIN(A(I)) 556
100 CONTINUE 557
BDE = 2. * COS(ASS12) 558
BDP = 2. * (-SIN(ASS1) + SIN(ASS2) - SIN(ASS3) - SIN(ASS4) - SIN(ASS5) 559
      + SIN(ASS6) - SIN(ASS7) - SIN(ASS8)) + 560
      3. * (-SIN(ASS9) - SIN(ASS10) + SIN(ASS11)) + 561
      4. * (-SIN(ASS12) + SIN(ASS13) + SIN(ASS14) - SIN(ASS15) - SIN(ASS16)) 562
DO 200 I = 1,30 563
BDE = BDE + ADE(I) * COS(AS(I)) 564
BDP = BDP + ADP(I) * SIN(AS(I)) 565
200 CONTINUE 566
DELTAE = (BDE + BDELE)/36000000. 567
SOTAP = (BDP + BDELP)/10000. 568
EPSC=23.4522944DO - TD*(0.0130125DO + TD*(0.00000164DO - 569

```

```

1TD*0.000000503D0)) + DELTAE
150 = DAYS/36525.00
TDRAD = T50 * STRAD
C
C
C
U = ZETA, H = THETA, UAZ = ZETA + Z
U = TORAD*(2304.997DC + T50*(.302D0 + T50*.0179D0))
Z = TORAD*(2304.997DC + T50*(1.093D0 + T50*.0192D0))
H = TORAD*(2004.298DC - T50*(.0426D0 + T50*.0416D0))
XPSI = BDTAP*STRAD
XEPS = DELTAE/ADR
EPSC = EPSD/ADR
CZ = DCOS(Z)
SZ = DSIN(Z)
SH = DSIN(H)
CH = DCOS(H)
CEPSD = DCOS(EPSD)
SEPSD = DSIN(EPSD)
EPSG = EPSD - XEPS
CEPSO = DCOS(EPSD)
SEPSO = DSIN(EPSD)
SXPSI = DSIN(XPSI)
CXPSI = DCOS(XPSI)
SUI = SEPSO*CEPSD - CEPSO*SEPSD*CXPSI
CUI = SEPSD*SXPSI
SZI = SEPSD*CEPSO - CEPSD*SEPSO*CXPSI
CZI = SEPSO*SXPSI
CHI = CEPSD*CEPSO + SEPSD*SEPSO*CXPSI
ZI = DATAN2(SZI,CZI)
CUAZ = CZ * CUI - SZ*SUI
CHP = CH*CHI - SH*CUAZ
CUPMU = SH*CHI + CH*CUAZ
SUPMU = CZ*SUI + SZ*CUI
UPMU = DATAN2(SUPMU,CUPMU)
UP = U + UPMU
CUPLU = DCOS(UPMU)
SUPLU = DSIN(UPMU)
SHP = CUPMU*CUPLU + SUPMU*SUPLU
CZPMZ = CH*SHP - SH*CHP*CUPLU
SZPMZ = SH * SUPLU
ZP = ZI + DATAN2(SZPMZ,CZPMZ)
RETURN
END
SUBROUTINE PRINCP(XCOURL,X)

```



```

REAL*8 XDOUBL,XT
1 = XDOUBL
XT = ((I + 180)/360)*360
XDOUBL = XDOUBL - XT
X = XDOUBL
RETURN
END
SUBROUTINE SAOCOR
IMPLICIT REAL*8 (A-H,C-Z)
COMMON/W/ TIM(49,30),RA(49,30),DEC(49,30),STNAM(30),TPASS,
1JDAYA(30),NUM(30),NCRDER(30),IYR1,IYR2,IMO1,IMO2,IDA1,IDA2,JDAY1,
1JDAY2,IARC,IARCS,ISTA(30),JSTA(30),NPASS(30),KEY4,K,IS
COMMON/SAO/ M,N
COMMON/T/ DAYS,COR,STHETA,CTHETA,ZETA,Z
DATA PI,TWOPI/3.141592653589793,6.283185307179586/
DAYS = JDAYA(M) + TIM(1,M)/86400.DO
CALL PRENUT
CALL TIMCOR
DO 500 I = 1,N
  UARO = ZETA + RA(I,M)
  CDECO = DCOS(DEC(I,M))
  SDECO = DSIN(DEC(I,M))
  SRMZ = CDECO * DSIN(UARO)
  DUM = CDECO * DCOS(UARO)
  CRMZ = CTHETA*DUM - STHETA*SDECO
  SDEC = CTHETA*SDECO + STHETA*DUM
  RMZ = DATAN2(SRMZ,CRMZ)
  CDEC = SRMZ * DSIN(RMZ) + CRMZ*DCOS(RMZ)
  DECF = DATAN2(SDEC,CDEC)
  AF = RMZ + Z
  IF (DECF.GT.PI) DECF = DECF - TWOPI
  IF (AF.GE.TWOPI) AF = AF - TWOPI
  RA(I,M) = AF
  DEC(I,M) = DECF
  TIM(I,M) = TIM(I,M) - CCR
  THIS IS A TEMPORARY CHANGE TO FIX ERROR IN SAO TIME
  ITIME=TIM(I,M)
  TIM(I,M)=ITIME
500 CONTINUE
RETURN
END

```

```

//Z7GEMOPB JOB (G70041150A,T,000138,H00H00),69,MSGLEVEL=1
// EXEC LOADER,PARM='MAP,CALL,SIZE=150K',REGION.GO=160K
//GO.FT06F001 DD SYSOUT=A,SPACE=(CYL,(8,2))
//GO.FT07F001 DD SYSOUT=B,DSN=DECK
//GO.SYSLIN DD UNIT=2400-9,LABEL=(5,BLP),DISP=(NEW,KEEP),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),VOL=SER=33599C
//GO.FT01F001 DD UNIT=2400-9,LABEL=(3,BLP),DISP=(OLD,DELETE),
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200,DEN=2),VOL=SER=3826F
//GO.FT02F001 DD DUMMY
//GO.FT03F001 DD SYSOUT=A,SPACE=(CYL,(2,2))
//GO.FT12F001 DD SYSOUT=A,SPACE=(CYL,(2,2))
//GO.SYSABEND DD SYSOUT=A,SPACE=(CYL,(1))
//GO.DATAS DD *

```

9	ORGAN	29001
19	SPAIN	29004
10	JUPTR	29010
50	COLDLK	29424
11	EDWAFB	29425
3	BPOIN	31021
1	FTMYR	31022
47	OOMER	31024
48	SATAG	31028
2	MOJAV	31030
68	NEWFL	31032
52	COLEG	31033
4	GFORK	31034
25	ROSMa	31042
6	EDINB	37036
5	COLBA	37037
14	BERMD	37039
16	PURIO	37040
7	GSFCP	37043
26	DENVR	37045
32	JUP24	37071
40	JUP40	37072
53	JUPTH	37073
33	JBC4L	37074
2	660108	0
		660115 0 0

/*

//GO.FT04F001 DD *

651225 4.3395

661225 4.3576

/*

**A-2.6 PRENAP CARD UPDATER PROGRAM
AND SAMPLE JCL**

IMPLICIT REAL*8 (A-H,O-Z)

IMPLICIT REAL*8 (A-H,O-Z)

LOGGICAL#1 A,B,BLANK

```

DIMENSION A(80), B(80), M(80), KAT(2), KEY(10), DATA(2)

```

EQUIVALENCE (B(1), BETA)

DATA INS.REP.DEL.MCD/INS 'REP','DEL','MOD'/'

DATA BLANKS - BLANK /

DATA PLANKS, BLANK,
INTEGER*4 ALPHA, INS, REP, DEL

1000 EQBWA1 (A4-X-15-5X-15)

[illegible]

IC01 FORMAT (10X, A4, A12, 3D, A12, /
IC10 FORMAT (10X, 'UPDATE ERRCB ', A4)

IC10 FORMAT (10X, UPDATE, ERRORS, ...)
2020 ENDMAT (13, 12, A8, 1013, D22-15, D15-8)

2020 FORMAT: (13,12)

2010 FORMAT (80A1)
2011 FORMAT (10X, 80A1)

FORMAL 110X, 800
WHITE 16 30001

WRITE (6,3000)
WRITE (6,3010)

WRITE (6,30) 3000 FORMAT (111,30Y,0RCCBAM TO UPDATE NAP INPUT CARDS STORED ON TAPE.

FORMAL (I, I, 30X, PROGRAM TO UPDATE NAME INFO CARDS STORED ON 1412
 411/22Y, INS 111 9Y, INSERTS CARDS AFTER SEQUENCE NUMBER 11, 1/3X, 0D

#//3X,	INS	11,	9X,	INSETS AFTER SEQUENCE NUMBER 12.	DATA
*E!	11	13	DELETES CARDS BETWEEN (AND INCLUDING) SEQUENCE NUMB		

TABLE 11. DELETES CARDS BETWEEN (AND INCLUDING) SEQUENCE NO. 1 AND 12. DELETES CARDS BETWEEN (AND INCLUDING) SEQUENCE NO. 1 AND 12.

NUMBERS 11 AND 12. 13X; REP 11 12 DELETES CARDS BETWEEN (AND IN-
CLUDING) SEQUENCE NUMBERS 11 AND 12-AND THEN INSERTS CARDS 13X. MO

#LOADING) SEQUENCE NUMBERS 11 AND 12, AND THEN INSERT 3 CARDS: 120, 115
 *C 11 12 MOVIES CARDS BETWEEN (AND INCLUDING) SEQUENCE NUMB

#	11	12	MUSIC
1	11	12	11
2	11	12	11
3	11	12	11
4	11	12	11
5	11	12	11
6	11	12	11
7	11	12	11
8	11	12	11
9	11	12	11
10	11	12	11
11	11	12	11
12	11	12	11
13	11	12	11
14	11	12	11
15	11	12	11
16	11	12	11
17	11	12	11
18	11	12	11
19	11	12	11
20	11	12	11
21	11	12	11
22	11	12	11
23	11	12	11
24	11	12	11
25	11	12	11
26	11	12	11
27	11	12	11
28	11	12	11
29	11	12	11
30	11	12	11
31	11	12	11
32	11	12	11
33	11	12	11
34	11	12	11
35	11	12	11
36	11	12	11
37	11	12	11
38	11	12	11
39	11	12	11
40	11	12	11
41	11	12	11
42	11	12	11
43	11	12	11
44	11	12	11
45	11	12	11
46	11	12	11
47	11	12	11
48	11	12	11
49	11	12	11
50	11	12	11
51	11	12	11
52	11	12	11
53	11	12	11
54	11	12	11
55	11	12	11
56	11	12	11
57	11	12	11
58	11	12	11
59	11	12	11
60	11	12	11
61	11	12	11
62	11	12	11
63	11	12	11
64	11	12	11
65	11	12	11
66	11	12	11
67	11	12	11
68	11	12	11
69	11	12	11
70	11	12	11
71	11	12	11
72	11	12	11
73	11	12	11
74	11	12	11
75	11	12	11
76	11	12	11
77	11	12	11
78	11	12	11
79	11	12	11
80	11	12	11
81	11	12	11
82	11	12	11
83	11	12	11
84	11	12	11
85	11	12	11
86	11	12	11
87	11	12	11
88	11	12	11
89	11	12	11
90	11	12	11
91	11	12	11
92	11	12	11
93	11	12	11
94	11	12	11
95	11	12	11
96	11	12	11
97	11	12	11
98	11	12	11
99	11	12	11
100	11	12	11

*ERS II AND 12.077)

FORMAT (22X, 'FORMAL FUR ABOVE FOUR CARUS (A4,X,13,3X,13)' // NOTE THAT

*TINS, DEL, REP, AND MCD START IN 71A, COLUMN 1 AND HAL COLUMN
COLUMNS OF BANK 1, 22Y INS AND REP MUST BE FOLLOWED BY THE CAR

*4 SHOULD BE BLANK. //ZXX; INS AND REP MUST BE FOLLOWED BY A BLANK CA

*DS TO BE INSERTED. THE CARDS MUST 1/1X, BE FOLLOWED BY A BLANK CARD

* * * * *

*2X, THE MOD CARDS MUST BE FOLLOWED BY A MODIFYING CARD. COLUMNS IN

*OT TO BE MODIFIED//IX, SHOULD BE LEFT BLANK.//IX,*****

111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000 1001 1002 1003 1004 1005 1006 1007 1008 1009 1010 1011 1012 1013 1014 1015 1016 1017 1018 1019 1020 1021 1022 1023 1024 1025 1026 1027 1028 1029 1030 1031 1032 1033 1034 1035 1036 1037 1038 1039 1040 1041 1042 1043 1044 1045 1046 1047 1048 1049 1050 1051 1052 1053 1054 1055 1056 1057 1058 1059 1060 1061 1062 1063 1064 1065 1066 1067 1068 1069 1070 1071 1072 1073 1074 1075 1076 1077 1078 1079 1080 1081 1082 1083 1084 1085 1086 1087 1088 1089 1090 1091 1092 1093 1094 1095 1096 1097 1098 1099 1100 1101 1102 1103 1104 1105 1106

011

10 READ (5,1000,END = 100) ALPHA, Y1, Y2

WRITE (6,1001) ALPHA,IL,I2

IF (ALPHA.EQ.INS) GC TO 20

IF (ALPHA.EQ.REP) GC TO 30

IF (ALPHA.EC.DEL) GC TO 30

IF(ALPHA.EQ. MOD). GO TO 30

WRITE {6,1010} ALPHA

STOP

20 IF (I.GE.Y1) GO TO 40

```
READ(9,END=200) KAT,XLAB,KEY,DATA,I
```

WRITE (12,2020) KAT, XLABL,KEY,DATA.

```

GO IC 20
30 I1=I1-1
GO TO 20
40 IF (ALPHA.EQ.DEL) GC TO 70
IF (ALPHA.EQ.MOD) GC TO 300
50 READ (5,2010) B
WRITE (6,2011) B
IF (BETA.EQ.BLANKS) GO TO 60
WRITE (12,2010) B
GO TO 50
60 IF (ALPHA.EQ.INS) GC TO 10
70 IF (I.GE.I2) GO TO 10
REAC(9,END=200) KAT,XLABL,KEY,DATA,I
GO IC 70
100 READ (9,END=200) KAT,XLABL,KEY,DATA,I
WRITE(12,2020) KAT,XLABL,KEY,DATA
GO TO 100
200 STOP
300 READ (5,2010) B
WRITE(6,2011) B
L=0
DO 310 J=1,80
IF(B(I).EQ.BLANK) GO TO 310
L=L+1
M(L)=J
310 CONTINUE
320 CONTINUE
IF(I.GE.I2) GO TO 10
REWIND 10
REAC (9,END=200) KAT,XLABL,KEY,DATA,I
WRITE (10,2020) KAT,XLABL,KEY,DATA
REWIND 10
REAC (10,2010) A
DO 330 K=1,L
J=M(K)
330 A(J)=B(J)
WRITE(12,2010) A
GO TO 320
END

```

```
// EXEC LOADER, PARM='MAP,CALL,SIZE=100K',REGION=GO=110K
//GO.SYSLIN DD *
```

***** PRENAP CARD UPDATER OBJECT DECK IS INSERTED HERE *****

```
/*
//GO.FT09FC01 DD UNIT=9TRACK,LABEL=(3,BLP),DSN=ITAPEGEM,
// DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3204),DISP=(OLD,PASS),
// VOL=SER=5630
//GO.FT10FC01 DD UNIT=DISK,SPACE=(TRK,(1,1)),
// DCB=(RECFM=VBS,LRECL=84,BLKSIZE=172),DISP=(NEW,DELETE)
//GO.FT12FC01 DD UNIT=DISK,SPACE=(CYL,(3,2)),DSN=NAPOLEON,
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),DISP=(NEW,PASS)
//GO.DATAS DD *
```

```
INS 12
999 OMQJAV6E 2 25 22 1 0 0 0 0 0 0 0.0 0.0
```

```
DEL 30 35
REP 36 40
999 OGFORK6E 2 27 21 1 0 0 0 0 0 0 0.0 0.0
201 OFMYR6E 2 1 22 0 0 66 1 34 0 0 0.51500000D 03 0.0
202 OFMYR6E 2 1 22 0 0 66 1 34 0 0 0.57780000D 03 0.0
701 IFTMEQL 1 1 6 3 1 0.10000000D 01 0.10000000D 16
701 IFTMEQM 2 1 7 4 1 0.10000000D 01 0.10000000D 16
```

```
MCC 50 55
0
```

0034 CARDS

A-2.7 POST NAP PROGRAM


```

C      KOUNT = 0
C      READ OPTION CARD FOR 701 CONTINUATION 1 CARDS
C      IF THE STANDARD DEVIATION OF A SET OF MEASUREMENTS FOR A PASS
C      (SDEVL AND SOCUM) EXCEEDS SOMAX OR IF THE MEAN MEASUREMENT ERROR
C      IN MINTRACK COUNTS EXCEEDS MAXERR THEN THE MEASUREMENT IS
C      EFFECTIVELY WEIGHTED OUT OF THE SOLUTION.
C      IOPT = -1, 0, OR 1 IF IOPT = 1 THEN (UNLESS ACCORDING TO THE ABOVE
C      CRITERION THE MEASUREMENT HAS BEEN WEIGHTED OUT OF THE SOLUTION)
C      THE A PRIORI MEASUREMENT SIGMA FOR THE PASS IS GIVEN AS
C      10 TIMES THE OBSERVED STANDARD DEVIATION FOR THE PASS.
C      NOTE THAT SDEVL = 0.00 DOES NOT INDICATE THAT
C      THE STANDARD DEVIATION EQUALS ZERO, BUT RATHER THAT NO STANDARD
C      DEVIATION HAS BEEN COMPUTED FOR THIS NAP RUN. IF THAT IS THE
C      CASE, AND A 701, CONTINUATION 1, FOR THE L-MEASUREMENT WAS USED
C      IN THIS RUN THEN THAT CARD IS COPIED (UNLESS THE MEASUREMENT
C      HAS BEEN WEIGHTED OUT BECAUSE OF AN EXCESSIVE ERROR -SEE ABOVE)
C      HOWEVER, IF NO PREVIOUS CARD EXISTS AND IOPT IS NOT EQUAL TO ZERO
C      THEN THE MEASUREMENT IS EFFECTIVELY WEIGHTED OUT. THE SAME APPLIES
C      TO THE M-MEASUREMENTS.
C      FREQC = 136.8300 (GEOS 1)
C      = 136.3200 (GEOS 11)
C
C      READ (5,1100) IOPT, MAXERR, SOMAX, FREQC
C      WRITE(6,1101) IOPT, MAXERR, SOMAX, FREQC
C
C      WRITE (31,1102)
C      I=0
C      2 READ(10) N,X,Y
C      IF(N.NE.601) GO TO 4
C      I=I+1
C      WRITE(12) N,X,Y
C      GO TO 2
C      4 REWIND 10
C      REWIND 12
C      DO 6 J=1,I
C      6 READ(10)
C
C      PLOB=136.00/(FREQC*57.00)
C      PCNT=PLOB/1000.00
C      EMPLOB=136.00/(FREQC*46.00)-PLOB
C      EMPCNT=EMPLOB/1000.00
C
C      READ NAP CONTROL CARDS

```

```

10 READ(27,1110,END=999) KAT,KONT,XLABL,KEY,DATA
   IF(KAT.EQ.601) CALL UP601
20 KOUNT=KOUNT+1
   WRITE(8) KAT,KONT,XLABL,KEY, DATA,KOUNT
   WRITE(6,1000) KOUNT,KAT,KONT,XLABL,KEY,DATA
   IF(KAT.NE.202) GO TO 10

```

```

PROCESS PASS

```

```

100 X701(1)=0.00
    X701(2)=0.00
    X704(1)=0.00
    X704(2)=0.00
    KSEVEN(1)=0
    KSEVEN(2)=0
    SL701=-1.00
    SM701=-1.00
    SL704=0.00
    SM704=0.00

```

```

XK=0 OR 1 AND CNT= PCNT OR ECNT DEPENDING ON WHETHER THE STATION
IS POLAR(EVEN) OR EQUATORIAL(ODD)

```

```

SEC=DATA(1)
IDAY=KEY(8)
NSTATN=KEY(2)
LF= NSTATN+30
XK=NSTATN-NSTATN/2*2
CNT=PCNT+EMPCNT*XK

```

```

READ(10) XLABLM,MN2,NUMPT1,NUMPT2,XLABLL,XMEANL,SDEVL,XMEANM,SDEVM
MN1=MN2-1
110 READ(27,1110,END=999) KAT,KONT,XLABL,KEY,DATA
   IF(KAT.EQ.999) GO TO 200

```

```

LM12 = 1 OR 2 ACCORDING AS KEY(1) IS ODD(L) OR EVEN(M)

```

```

LM12=2-KEY(1) + KEY(1)/2*2
   IF(KAT.EQ.701) GO TO 130
   IF(KAT.EQ.704) GO TO 140
120 KOUNT = KOUNT + 1
   WRITE(8) KAT,KONT,XLABL,KEY,DATA,KOUNT
   WRITE(6,1000) KOUNT,KAT,KONT,XLABL,KEY,DATA
   GO TO 110

```

```

C
C
C
130 701 CARD
130 X701(LM12) = DATA(2)
KSEVEN(LM12)=KEY(7)
GO TO 110
C
C
C
140 704 CARD
140 X704(LM12) = DATA(1)
GO TO 110
999 CARD
C
C
C
200 ERRORL=(XMEANL-X704(1)+ABIAS(MN1))/CNT
IF(ERRORL.LT.0.00) GO TO 210
ERROR=ERRORL + 0.500
LLOBE=-(ERROR + 500)/1000
GO TO 220
210 ERROR=ERRORL-0.500
LLOBE= -(ERROR-500)/1000
220 ERRORM=(XMEANM-X704(2)+ABIAS(MN2))/CNT
IF(ERRORM.LT.0.00) GO TO 230
MERROR=ERRORM + 0.500
MLOBE=-(MERROR + 500)/1000
GO TO 240
230 MERROR = ERRORM -0.500
MLOBE=-(MERROR-500)/1000
240 IF(LLOBE.EQ.0) GO TO 250
ERROR=LERROR + 1000*LLOBE
SL704=1000*LLOBE
SL704=SL704*CNT
KOUNT=KOUNT + 1
WRITE(8) K704,XLABLL,MN1,KEY704,SL704,BLANK,KOUNT
WRITE(6,1000) KOUNT,K704,XLABLL,MN1,KEY704,SL704
250 IF(MLOBE.EQ.0) GO TO 255
MERROR=MERROR + 1000*MLOBE
SM704=1000*MLOBE
SM704=SM704*CNT
KOUNT=KOUNT + 1
WRITE (8) K704,XLABLM,MN2,KEY704,SM704,BLANK,KOUNT
WRITE(6,1000) KOUNT,K704,XLABLM,MN2,KEY704,SM704
C
C
C
255 IF(SDEVL.LE.0.00) GO TO 320

```

```

260 IF(IABS(LERROR).GT.MAXERR) GO TO 330
   IF(SDEV.LE.O.DO) GO TO 300
   IF(SDEV.LGT.SDMAX) GO TO 340
   IF(IOPT.LE.O) GO TO 355
   SL701= SDEV*10.DO
   KL701(5)=0
280 KOUNT=KOUNT + 1
   WRITE(8) K701,XLABLL,MN1,NSTATN,KL701,X1,SL701,KOUNT
   WRITE(6,1000) KOUNT,K701,XLABLL,MN1,NSTATN,KL701,X1,SL701
   GO TO 355

```

C

```

290 SL701=D15
295 KL701(5)=1
   GO TO 280
300 IF(X701(1).GT.O.DO) GO TO 290
   IF(IOPT.NE.O) GO TO 290
   GO TO 355
320 IF(X701(1).GE.D15) GO TO 260
   SDEV=X701(1)*1.D-1
   IF(KSEVEN(1).GT.O) SDEV=SDEV*1.D-6
   GO TO 260
330 IF(SDEV.LE.O.DO) GO TO 290
340 IF(IOPT.LE.O) GO TO 290
   SL701=SDEV*1.D7
   GO TO 295

```

C

```

355 IF(SDEV.LE.O.DO) GO TO 420
360 IF(IABS(MERROR).GT.MAXERR) GO TO 430
   IF(SDEV.LE.O.DO) GO TO 400
   IF(SDEV.LGT.SDMAX) GO TO 440
   IF(IOPT.LE.O) GO TO 500
   SM701=SDEV * 10.DO
   KM701(5)= 0
380 KOUNT=KOUNT + 1
   WRITE(8)K701,XLABLM,MN2,NSTATN,KM701,X1,SM701,KOUNT
   WRITE (6,1000) KOUNT,K701,XLABLM,MN2,NSTATN,KM701,X1,SM701
   GO TO 500
390 SM701=D15
395 KM701(5)=1
   GO TO 380
400 IF(X701(2).GT.O.DO) GO TO 390
   IF(IOPT.NE.O) GO TO 390
   GO TO 500
420 IF(X701(2).GE.D15) GO TO 360

```

```

SDEVM=X701(2)*1.D-1
IF(KSEVEN(2).GT.0) SDEVM=SDEVM*1.D-6
GO TO 360
430 IF(SDEVM.LE.0.00) GO TO 390
440 IF(IOPT.LE.0) GO TO 390
SM701=SDEVM*1.D7
GO TO 395

C
500 LSD=SDEVL/CNT+0.500
MSD=SDEVM/CNT+0.500
WRITE(11) LF, IDAY, SEC, KEY(1), KEY(3), LERROR, MERROR, LLOBE, MLOBE,
* LSD, MSD, KL701(5), KM701(5), KSEVEN
GO TO 20

C
999 REWIND 11
READ(10,END=998)
998 CALL IWRITE
REWIND 8
997 READ(8,END=996) KAT, KONT, XLABL, KEY, DATA, KOUNT
WRITE(10) KAT, KONT, XLABL, KEY, DATA, KOUNT
GO TO 997
996 CONTINUE
WRITE(6,1006)
STOP
1000 FORMAT(2I8, I2, A8, 10I3, D22.15, D22.8)
1100 FORMAT(2I5, 2D10.1)
1101 FORMAT(1X, IOPT=, I2, 5X, MAXERR=, I4, 5X, SDMAX=, D11.3, 5X, FREQCY=
*, F9.3////)
1102 FORMAT(1'///30X, B I A S V A L U E S'//
314X, 'STATION', 13X, 'PREPROCESSOR', 12X, 'NEW' /
412X, 'NAME NUMBER', 13X, 'BIAS', 16X, 'BIAS'//)
1006 FORMAT (///20X, 'PROCESS COMPLETE')
END

```

```

SUBROUTINE UP601
IMPLICIT REAL*8 (A-H,O-Z)
COMMON /U601/ PLOB, EMPLOB, ABIAS(60), XLABL, DATA(2), KAT, KONT,
*KEY(10)
DIMENSION IBIAS(60)
DATA IBIAS/957, 13, 137, 431, 822, 54, 766, 20, 950, 247, 22, 876,
* 78, 42, 938, 970, 935, 929, 174, 914, 72, 975, 872, 12,
2 53, 938, 94, 870, 12*0,
3 948, 94, 83, 889, 959, 807, 842, 926, 30, 577, 76, 126,

```

```

4      64,949,603, 2, 31,935,950,120/
1103  FORMAT(11X,A8,I5,I4X,I4,I6X,I4)
      READ(12) N,YLABL,DATA(1)
      IF(KEY(5).NE.10) RETURN

```

C
C
C
C
C

UPDATE BIAS

```

      XK=0 OR 1 AND ULOBE=PLOB OR ELOB DEPENDING ON WHETHER THE STATION
      NUMBER IS EVEN(POLAR) OR ODD(EQUATORIAL)
      IV=KEY(7)
      XK=KEY(2)-KEY(2)/2*2
      ULOBE=PLOB+EMPL0B*XK
      BIAS=DATA(1)/ULOB
      LBIAS=BIAS+0.500
      IF(BIAS.LT.0.00) LBIAS=BIAS-0.500
      BIAS=(BIAS-DFLOAT(LBIAS))
      DATA(1)=BIAS*ULOB
      BIAS=BIAS*1000.00 + DFLOAT(ICIAS(IV))
      ABIAS(IV)=DFLOAT(LBIAS)*ULOB
      IF(BIAS.LT.-0.500) BIAS=BIAS+1000.00
      IF(BIAS.GE.999.500) BIAS=BIAS-1000.00
      LBIAS=BIAS+0.500
      WRITE (31,1103) XLABL,KEY(2),IBIAS(IV),LBIAS
      RETURN
      END

```

SUBROUTINE IWRITE

```

      IMPLICIT REAL*8 (A-H,O-Z)
      LOGICAL*1 GRAPH,SYMBOL,STAR,ELEVOK,PLOT,BLANK,ELEV,WT
      DIMENSION SYMBOL(2),GRAPH(83),SIGMA(2),DMS(2),NOBS(2),PLOT(2),
1      SUMT(2),SUMTSQ(2),SUMET(2),SCALE(2),TIMSEC(160),QMEAS(160,2),
2      ERR(2),IGRAPH(2),KI(2),SLOPE(2),IROPE(2),NEDIT(2),STATIO(30),
3      QMEAN(2),WT(2),KSEVEN(2)
      DATA BLANK,GRAPH /84*0,0/
      DATA SYMBOL,STAR/'L','M','*','*'/
      DATA IGRAPH /21,63/
      DATA STATIO/'FTMYR6E','FTMYR6P','QUIT06E','QUIT06P',
*      'LIMA6E','LIMA6P','SNTAG6E','SNTAG6P',
*      'NEWFL6E','NEWFL6P','WNKFL6E','WNKFL6P',
*      'JOBUR6E','JOBUR6P','ULASK6E','ULASK6P',
*      'ORORA6E','ORORA6P','MADG6E','MADGA6P',
*      'BPOIN6E','BPOIN6P','COLEG6E','COLEG6P',
*      'MOJAV6E','MOJAV6P','GFORK6E','GFORK6P',
*      'WOMER6E','WOMER6P' /

```

DO 5 I=31,60

```

M=I-30
WRITE(I,1104) STATIO(M),M
5 CONTINUE
10 READ(10,END=200) NOARC,NOPASS,ISTSID,STLABL,ELEVOK,LMEAN,LA,SIGMA,
  *QMS,TOCURR,TSCURR,(TIMSEC(L),L=1,LA),((QMEAS(L,I),L=1,LA),I=1,2)
  READ(11) LF,IDAY,SEC,KEY1,KEY3,LError,MERROR,
  * LLOBE,MLOBE,LSD,MSD,KEY7L,KEY7M,KSEVEN
  IH= TSCURR/3600.00
  SEC= TSCURR - (IH*3600)
  IM=SEC/60.00
  SEC=SEC-(60*IM)
  DO 20 I=1,2
    PLOT(I) = STAR
    WT(I)=BLANK
    IF(KSEVEN(I).GT.0) WT(I)=STAR
    IF(ELEVOK) PLOT(I)= SYMBOL(I)
    NOBS(I)=0
    SUMT(I)=0.00
    SUMFSQ(I)=0.00
    SUMET(I)=0.00
    SCALE(I)= 0.1500*SIGMA(I)
20 CONTINUE
    IF(LA.LE.1) GO TO 45
    DO 28 I=1,2
      N=0
      SUM=0.00
      TWOSIG=SIGMA(I)*3.00
      DO 22 L=1,LA
        IF(QMEAS(L,I).GE.10.020) GO TO 22
        SUM=SUM+QMEAS(L,I)
        N=N+1
      22 CONTINUE
      N1=N
      SUM1=SUM
      24 CONTINUE
      NOLD=N
      EN=N
      AVRAVE=SUM/EN
      N=N1
      SUM=SUM1
      DO 26 L=1,LA
        IF(QMEAS(L,I).GE.10.020) GO TO 26
        IF(DABS(QMEAS(L,I)-AVRAVE).LE.TWOSIG) GO TO 26
      SUM = SUM-QMEAS(L,I)

```

```

N=N-1
26 CONTINUE
IF(N.LT.NOLD) GO TO 24
QMEAN(I)= AVRAE
28 CONTINUE
WRITE(20,1105) STLABL,ISTSID,NOARC,NOPASS,IDAY,IH,IM,SEC,QMEAN,
*SIGMA
DO 40 L= 1,LA
TIM= TIMSEC(L)- TSCURR
IF(TIM.GT.3600.D0) TIM= TIM- 86400.D0
IF(TIM.LT.-3600.D0) TIM = TIM + 86400.D0
DO 30 I=1,2
ERR(I)= QMEAS(L,I)-QMEAN(I)
IF(ERR(I).GE.10.D20) GO TO 500
ERRORP= ERR(I)/SCALE(I)
IF (DABS(ERRORP).GT.20.D0) GO TO 520
KI(I) = ERRORP + IGRAPH(I)
GRAPH(KI(I)) = PLOT(I)
NOBS(I)= NOBS(I)+1
SUMT(I)= SUMT(I)+ TIM
SUMTSQ(I) = SUMTSQ(I) + TIM*TIM
SUMET(I)= SUMET(I)+ ERR(I)*TIM
30 CONTINUE
WRITE(20,1106) TIM,ERR,GRAPH
GRAPH(KI(1)) = BLANK
GRAPH(KI(2)) = BLANK
40 CONTINUE
45 CONTINUE
DO 50 I=1,2
PLOT(I)= BLANK
IF(LA.LE.1) NOBS(I)=LA
NEDIT(I)= LA - NOBS(I)
SLOPE(I)= 0.D0
IROPE(I)=0
IF(NOBS(I).LE.2) GO TO 50
OBSNUM= NOBS(I)
TBAR= SUMT(I)/OBSNUM
SLOPE(I)= SUMET(I)/(SUMTSQ(I)-SUMT(I)*TBAR)
IROPE(I)=100
TP=1.D0+(1.D0-SLOPE(I)*SUMET(I)/(SIGMA(I)*SIGMA(I)))/(OBSNUM-2.D0)
IF(TP.GT.0.D0) IROPE(I)=100.D0*(1.005D0-DSQRT(TP))
50 CONTINUE
ELEV=STAR
IF(ELEVOK) ELEV=BLANK

```


A-2.8 SAMPLE JCL FOR COMPLETE NAP RUN

```
*****  
//***** (JOB CARD) *****  
***** JCL FOR PRENAP: *****
```

JCL FOR PRENAP:

```

// EXEC LOADER, PARM='MAP,CALL,SIZE=100K',REGION.CO=110K.
//GO.SYSLIN DD *

```

*****OBJECT DECK FOR PRENAP-CARD-UPDATE PROGRAM INSERTED HERE*****

☆

```
//GO.FT09F001 DD UNIT=9TRACK,LABEL=(11,BLP),DSN=ITAPEGEM,
// DCB=(RECFM=VBS,LRECL=80,BLKSIZE=3204),DISP=(OLD,PASS),
// VOL=SER=345036
//GO.FT10F001 DD UNIT=DISK,SPACE=(TRK,(1,1)),
// DCB=(RECFM=VBS,LRECL=84,BLKSIZE=172),DISP=(NEW,DELETE)
//GO.FT12F001 DD UNIT=DISK,SPACE=(CYL,(3,1)),DSN=NAPOLEON
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),DISP=(NEW,PASS)
```

400-1-1

1919

.720000000000000000D04.5000000000-13

[illegible]

MOD. 173 186

0.0000000000000000.I00000000D-02

[illegible]

JCL FOR NAP:

```
// EXEC LINKGO,PARM=OVLY,MAP,LIST,XREF°,NBLK=300,REGION,GO=499K
//LINK.SYSPRINT DD SYSOUT=A,SPACE=(CYL,(2,1))
//LINK.SYSUT1 DD SPACE=(CYL,(5,2))
//LINK.TAPELIB DD UNIT=24CO-9,LABEL=(2,BLP,IN),DISP=(OLD,PASS),
// DSN=NAPOBJ,
// DCB=(RECFM=FB,LRECL=80,BLKSIZE=3200),VOL=SER=34503G
//LINK.SYSLIN DD *
INSERT CLEAN
INSERT COMSOL,TSPARM,ASPARM,ACINFO,PSPARM,STINFO,TYLE,GENCOM,MSINFO
INSERT CCEBUG,IONUMB,GPCOM,EXTCM,EARTH,ICONST,FCONST,CONMET
INSERT CINTG,CMEASR,RSUMR
INSERT MAIN,PAGE,ROTFIX,ROTINT,RESID,SIGWT,DAYHMS,CWORK
INSERT CLEAR
CVERLAY ALPHA
INSERT DREUIT,SPOLCD,DEFLT,INPCRD,GENFIL,EDIT,GAUSS,RANDU
INSERT UNIFD2,GPRSM2,GEOS,EDPOLY,REPRT2,RDMS,COMGHA,JULDAY,ECINT
CVERLAY ALPHA
INSERT PRITIAL
INSERT MATMUT
INSERT REFRCI,ROTPAR,MEASUR,RSUM,MESOLD,ROTBK,ROTOLO,ROTOMA,AZIM
INSERT ELEV,RARIES,SPOVEL,SVAREQ
INSERT SOFORT,SOFSEC,KICKER,ENGRAT
INSERT EXPAND
INSERT SOLVEX,SOVARY,ENTRNS,SOLANG,ENROOT,CLEAR
INSERT CKTIME,ENUTAT,PENMAT,PENUT,VARIEQ,ENEXPS
INSERT ENVARY,SUMBDY,ENDIST,KCOM,JCOM,HCOM,GCOM,FCOM,ECOM
INSERT DCOM,CCOM,BCOM,ACOM,PRIMY
CVERLAY ALPHA
INSERT SOLVER,INVERT,FINALP
CVERLAY ALPHA
INSERT SIMOUT
```

*****ANY OBJECT DECKS FOR LINK STEP ARE INSERTED HERE*****

INCLUDE TAPELIB
ENTRY MAIN

```
//LINK.SYSUCUMP DD SYSOUT=A,SPACE=(CYL,(1))
//GO.FT06FC01 DD SYSOUT=A,DCB=(RECFM=VBA,LRECL=137,BLKSIZE=7265),
// SPACE=(CYL,(9,1))
//SYSPRINT DD SYSOUT=A,DCB=(RECFM=VBA,LRECL=137,BLKSIZE=7265)
//GO.FT10FC01 DD UNIT=DISK,SPACE=(TRK,(3,1)),DSN=ATGOUTP,
```

```

//      DCB=(RECFM=VBS,LRECL=64,BLKSIZE=644),DISP=(NEW,PASS)
//GO.FT21F001 DD UNIT=DISK,SPACE=(CYL,(10,1)),DSN=Z7GEM21,
//      DCB=(RECFM=VBS,LRECL=156,BLKSIZE=7180)
//GO.FT22F001 DD UNIT=DISK,SPACE=(CYL,(4,1)),
//      DCB=(RECFM=VBS,LRECL=304,BLKSIZE=6996)
//GO.FT23F001 DD UNIT=2314,SPACE=(TRK,(4,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT24F001 DD UNIT=2314,SPACE=(TRK,(8,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT25F001 DD UNIT=DISK,SPACE=(CYL,(1,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT26F001 DD UNIT=2314,SPACE=(TRK,(8,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT27F001 DD UNIT=DISK,SPACE=(CYL,(3,1)),DSN=ATGCARDS,
//      DCB=(RECFM=VBS,LRECL=88,BLKSIZE=884),DISP=(NEW,DELETE)
//GO.FT28F001 DD DUMMY
//GO.FT29F001 DD UNIT=2400-9,LABEL=(5,BLP),DISP=(OLD,PASS),
//      DCB=(RECFM=VBS,LRECL=52,BLKSIZE=5204),VOL=SER=34503G
//GO.FT30F001 DD DUMMY
//GO.FT31F001 DD UNIT=2314,SPACE=(TRK,(4,1)),
//      DCB=(RECFM=VBS,LRECL=200,BLKSIZE=404)
//GO.FT32F001 DD UNIT=DISK,SPACE=(CYL,(9,1)),DSN=Z7GEM32,
//      DCB=(RECFM=VBS,LRECL=2168,BLKSIZE=2172)
//GO.FT33F001 DD DUMMY
//GO.FT35F001 DD DUMMY
//GO.FT36F001 DD UNIT=DISK,SPACE=(CYL,(1,1)),DSN=Z7GEM36,
//      DCB=(RECFM=VBS,LRECL=36,BLKSIZE=364),DISP=(NEW,DELETE)
//GO.FT37F001 DD UNIT=AFF=FT25F001,LABEL=(13,BLP),DSN=NURITE,
//      DCB=(RECFM=VBS,LRECL=3825,BLKSIZE=7654),DISP=(NEW,PASS),
//      VOL=SER=34503G
//GO.FT37F002 DD UNIT=AFF=FT25F001,LABEL=(14,BLP),DSN=NUPASS,
//      DCB=(RECFM=VBS,LRECL=64,BLKSIZE=644),DISP=(NEW,PASS),
//      VOL=SER=34503G
//GO.FT37F003 DD DUMMY
//CO.SYSABEND DD SYSOUT=A,SPACE=(CYL,(1))
//GO.DATAS DD UNIT=DISK,DSN=NAPOLEON,DISP=(OLD,PASS)
/*

```

A-2-94

JCL FOR POST NAP:

```

// EXEC  LOADER,PARM=MAP,CALL,SIZE=180K,REGION.GO=190K
//GO.SYSLIN DD *

```

*****OBJECT DECK INSERTED HERE*****

```
/*
//GO.FT06F001 DD SYSOUT=A,DCB=(RECFM=VBA,LRECL=137,BLKSIZE=7265),
// SPACE=(CYL,(5,1))
//GO.FT08F001 DD UNIT=DISK,SPACE=(CYL,(4,1)),DSN=Z7GEM08,
// DCB=(RECFM=VBS,LRECL=80,BLKSIZE=1604),DISP=(NEW,DELETE)
//GO.FT10F001 DD UNIT=9TRACK,LABEL=(14,BLP),DSN=Z7GEM10,
// DCB=(RECFM=VBS,LRECL=64,BLKSIZE=3204),DISP=(OLD,PASS),
// VOL=SER=34503G
//GO.FT10F002 DD UNIT=9TRACK,LABEL=(13,BLP),DSN=Z7GEM1A,
// DCB=(RECFM=VBS,LRECL=3825,BLKSIZE=7654),DISP=(OLD,PASS),
// VOL=SER=34503G
//GO.FT10F003 DD UNIT=9TRACK,LABEL=(15,BLP),DSN=Z7GEM1B,
// DCB=(RECFM=VBS,LRECL=80,BLKSIZE=1604),DISP=(NEW,KEEP),
// VOL=SER=34503G
//GO.FT11F001 DD UNIT=DISK,SPACE=(CYL,(3,1)),DSN=Z7GEM11,
// DCB=(RECFM=VBS,LRECL=76,BLKSIZE=764),DISP=(NEW,DELETE)
//GO.FT12F001 DD UNIT=DISK,SPACE=(TRK,(1,1)),DSN=Z7GEM12,
// DCB=(RECFM=VBS,LRECL=24,BLKSIZE=244),DISP=(NEW,DELETE)
//GO.FT20F001 DD DUMMY
//GO.FT27F001 DD UNIT=DISK,DSN=NAPOLEON,DISP=(OLD,DELETE)
//GO.FT31F001 DD SYSOUT=A,SPACE=(TRK,(4,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT32F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT33F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT34F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT35F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT36F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT37F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT38F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT39F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT40F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT41F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
```

```

//GO.FT42F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT43F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT44F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT45F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT46F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT47F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT48F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT49F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT50F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT51F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT52F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT53F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT54F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT55F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT56F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT57F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT58F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT59F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.FT60F001 DD SYSOUT=A,SPACE=(TRK,(2,1)),
// DCB=(RECFM=VBA,LRECL=137,BLKSIZE=689)
//GO.DATAS DD *

```

1 20 0.50-3 136.830C

/*

APPENDIX A-3
SUBROUTINE MODIFICATIONS TO NAP-II

A-3.1 SUBROUTINE ENEXPS

SUBROUTINE ENEXPS(ITN) 101430
SUBROUTINE ENEXPS(ITN) COMMENTS 101440
101450
101460
1. FOR EACH POWER SERIES COMPUTED THIS SUBROUTINE IS CALLED 101470
(KTR-2) TIMES BY SUBROUTINE EXPAND. KTR IS THE NUMBER OF 101480
TERMS IN THE POWER SERIES FOR POSITION (X,Y,Z) AND ITN IS THE 101490
TERM NUMBER BEING COMPUTED ON THE CURRENT ITERATION. 101500
INITIAL POSITION AND VELOCITY WOULD CORRESPOND TO ITN=1 AND 2 101510
RESPECTIVELY AND ARE NOT COMPUTED BY THIS SUBROUTINE. FOR EACH 101520
POWER SERIES THAT THIS SUBROUTINE IS CALLED THE INITIAL VALUE 101530
OF ITN IS THUS 3. 101540
101550
2. THIS SUBROUTINE COMPUTES THE EFFECTS OF THE GRAVITATIONAL 101560
FORCE OF N-BODIES ON EACH OTHER. THE EFFECT OF SOLAR RADIATION 101570
PRESSURE IS ALSO COMPUTED. HOWEVER, THE GRAVITATIONAL PULL 101580
OF THE PRIMARY SOURCE ON THE PROBE IS NOT COMPUTED HERE BUT 101590
IN SUBROUTINE EXPAND. 101600
101610
101620
101630
3. DENOTING (ITN-3) BY K, THE COEFFICIENTS OF T**K FOR RELATIVE 101640
DISTANCES AND THE COEFFICIENTS T**(K+2) FOR POSITIONS RELATIVE 101650
TO THE PRIMARY SOURCE ARE COMPUTED. NOTE THAT THE COEFFICIENT OF 101660
T**{(Y+2)} IS ACTUALLY THE (3+K)TH, I.E. ITN-TH COEFFICIENT. THE 101670
CONTRIBUTION TO THE ITN-TH POSITION COEFFICIENTS OF THE PROBE 101680
OF THE PRIMARY SOURCE GRAVITY FIELD AND DRAG ARE CONTAINED IN 101690
(XPO,YPO,ZPO) WHEN THIS ROUTINE IS CALLED. 101700
101710
101720
4. THE COEFFICIENTS OF THE RELATIVE BODY POSITIONS ARE ARRANGED 101730
SUCH THAT SEQUENTIAL COEFFICIENTS OF ANY ONE BODY ARE ALWAYS 101740
'NBD' COEFFICIENTS APART 'NBD' THUS APPEARS AS A UNIT AND HAS 101750
FOR THIS REASON BEEN EQUIVALENCED TO 'ONE'. THE UNIT 'UNIT' 101760
CORRESPONDING TO RELATIVE DISTANCES IS NBD(NBD-1)/2, THE NUMBER OF 101770
RELATIVE DISTANCES BETWEEN NBD BODIES. THE VALUE OF K APPEARING 101780
IN THE PROGRAM IS GIVEN BY (ITN-3)*ONE AND CORRESPONDS THE 101790
K OF COMMENT 3 ABOVE. THUS X(N+K) IS THE COEFFICIENT OF T**K OF 101800
X-POSITION OF BODY N. 101810
101820
101830
5. SINCE ITN IS INITIALLY 3 (SEE COMMENT 1) IT FOLLOWS THAT K 101840
IS INITIALLY 0. 101850
101860

```

101870
101880
101890
101900
101910
101920
101930
101940
101950
101960
101970
101980
101990
102000
102010
102020
102030
102040
102050
102060
102070
102080
102090
102100
102110
102120
102130
102140
102150
102160
102170
102180
102190
102200
102210
102220
102230
102240
102250
102260
102270
102280
102290
102300

6A. IF SOLAR PRESSURE IS NOT BEING COMPUTED (KSP=0) THEN NO
COMPUTATIONS ARE PERFORMED FOR THE PROBE-PRIMARY SOURCE
COMBINATION (SEE COMMENT 2).

IF SOLAR PRESSURE IS BEING COMPUTED THEN THE PROBE-PRIMARY
SOURCE DISTANCE MUST BE COMPUTED (BUT NOT THE PRIMARY SOURCE
GRAVITATIONAL FORCE).
6B. IF THE SUN IS NOT THE PRIMARY SOURCE, THEN SHADOW
COMPUTATIONS ARE PERFORMED, BUT

6C. IF THE SUN IS THE PRIMARY SOURCE, THEN NO SHADOW
COMPUTATIONS ARE PERFORMED.

DENOTING THE PROBE-PRIMARY SOURCE POSITION IN THE R, THETA
AND PHI ARRAYS BY N (WHERE N.LE.45) THE FOLLOWING QUANTITIES ARE
COMPUTED
FOR CASE 6A. (NPRNPS= N, NPSNPR= 100, KSP2= 0)
FOR CASE 6B. (NPRNPS= 100, NPSNPR= N, KSP2= 1)
FOR CASE 6C. (NPRNPS= 100, NPSNPR= 100, KSP2= 0)

IMPLICIT REAL*8 (A-H,O-Z)
INTEGER*4 ONE,TWO,UNIT,S
REAL*8 KPIKPI2
COMMON /CCOM/
1XPO(16),YPO(16),ZPO(16),XBD(160),YBD(160),ZBD(160),CGB(14),SGB(14)
2,XTL(14),YTL(14),CLB(14),SLB(14),CLT(14),SLT(14),VRB(14),
3RPT(14),RMT(14),RMO(14),RZR(14),RMR(14)
COMMON /ECOM/
1BDY(10),BMU(10),BTM(10),HTL(16),BRT(10),BRA(10),BDT(10),STL(16)
2,RST(825),VST(825),WST(770),NCN(10),NBT(10)
COMMON /ICOM/
1NBD,NTE,NHT,NSU,NPR,NPS,NOS,ICN,KTR,KDR,KVE,KDV,KSP,ISP,KIN,MPT
EQUIVALENCE (A(1),STL(1)),(THETAC(1),HTL(1)),(X(1),XBD(1)),
* (Y(1),YBD(1)),(Z(1),ZBD(1)),(R(1),RST(1)),(THETA(1),VST(1)),
* (PHI(1),WST(1)),(ONE,NBD)
DIMENSION A(16),THETAC(16),X(160),Y(160),Z(160),R(825),THETA(825),
* PHI(770)
IJO= 0

```

XK= ITN - 3	102310
OK3= -XK/3.DO	102320
KP1KP2= (XK+1.00)*(XK+2.00)	102330
K= (ITN-3) * ONE	102340
	102350
FOR (K=0) SEE COMMENT 5.	102360
IF(K.LE.0) GO TO 1300	102370
	102380
100 KMONE= K - ONE	102390
KPTWO= K + TWO	102400
	102410
DO 700 IO= 1,NBDM1	102420
IK= IO + K	102430
IKPTWO= IK + TWO	102440
GMI= BMU(IO)	102450
	102460
IOPI=IO+1	102470
DO 600 JO=IOPI,NBD	102480
JK= JO + K	102490
IJO= IJO + 1	102500
IJS= IJO	102510
IJK= IJK + 1	102520
IJKMS= IJK	102530
	102540
FOR 'IJO=NPRNPS' SEE COMMENT 6.	102550
	102560
IF(IJO.EQ.NPRNPS) GO TO 600	102570
	102580
XIJO= X(IO) - X(JO)	102590
YIJO= Y(IO) - Y(JO)	102600
ZIJO= Z(IO) - Z(JO)	102610
	102620
FOR 'K=0' SEE COMMENT 5.	102630
	102640
IF(K.LE.0) GO TO 1200	102650
	102660
FXIJK= THETA(IJO) * (X(IK)-X(JK))	102670
FYIJK= THETA(IJO) * (Y(IK)-Y(JK))	102680
FZIJK= THETA(IJO) * (Z(IK)-Z(JK))	102690
RIJK= XIJO*(X(IK)-X(JK)) + YIJO*(Y(IK)-Y(JK)) + ZIJO*(Z(IK)-Z(JK))	102700
THIJK= 0.DO	102710
PHIJK= 0.DO	102720
	102730
IF(KMONE.LE.0) GO TO 400	102740

C	DO 300 S= ONE, KMONE, ONE	102750
	IJS = IJS + UNIT	102760
	IJKMS= IJKMS - UNIT	102770
	PHIJK= R(IJS) * PHI(IJKMS) + PHIJK	102780
	THIJK= THETA(IJS) * PHI(IJKMS) + THIJK	102790
	FXIJK= THETA(IJS) * (X(IK-S) - X(JK-S)) + FXIJK	102800
	FYIJK= THETA(IJS) * (Y(IK-S) - Y(JK-S)) + FYIJK	102810
	FZIJK= THETA(IJS) * (Z(IK-S) - Z(JK-S)) + FZIJK	102820
	IF(IJS-IJKMS) 200, 1000, 300	102830
		102840
C		102850
	200 RIJK= (X(IO+S)-X(JO+S)) * (X(IK-S)-X(JK-S))	102860
	1 + (Y(IO+S)-Y(JO+S)) * (Y(IK-S)-Y(JK-S))	102870
	2 + (Z(IO+S)-Z(JO+S)) * (Z(IK-S)-Z(JK-S))	102880
	3 - R(IJS) * R(IJKMS) + RIJK	102890
	300 CONTINUE	102900
C		102910
	400 R(IJK) = RIJK/R(IJO)	102920
C		102930
C	FOR *IJO=NPSNPR* SEE COMMENT 6.	102940
	IF(IJO.EQ.NPSNPR) GO TO 2000	102950
C		102960
	PHI(IJK) = (R(IJK)*XK - PHIJK)/R(IJO)	102970
	THETA(IJK) = (PHI(IJK)*THETA(IJO) + THIJK)/QK3	102980
	FXIJK = THETA(IJK)*XIJO + FXIJK	102990
	FYIJK = THETA(IJK)*YIJO + FYIJK	103000
	FZIJK = THETA(IJK)*ZIJO + FZIJK	103010
C		103020
C		103030
	500 IF(IJO.EQ.NPRNSU) GO TO 1100	103040
C		103050
	X(IKPTWO) = - BMU(JO)*FXIJK + X(IKPTWO)	103060
	Y(IKPTWO) = - BMU(JO)*FYIJK + Y(IKPTWO)	103070
	Z(IKPTWO) = - BMU(JO)*FZIJK + Z(IKPTWO)	103080
C		103090
	X(JK+TWO) = GMI*FXIJK + X(JK+TWO)	103100
	Y(JK+TWO) = GMI*FYIJK + Y(JK+TWO)	103110
	Z(JK+TWO) = GMI*FZIJK + Z(JK+TWO)	103120
C		103130
	600 CONTINUE	103140
	700 CONTINUE	103150
C		103160
	800 L1= KPTWO + 1	103170
	L2= L1 + NBDMI	103180

```

C
FXIJK= X(NPS+KPTWO)
FYIJK= Y(NPS+KPTWO)
FZIJK= Z(NPS+KPTWO)
DO 900 L= LI,L2
X(L)= (X(L) - FXIJK)/KPIKP2
Y(L)= (Y(L) - FYIJK)/KPIKP2
Z(L)= (Z(L) - FZIJK)/KPIKP2
900 CONTINUE
C
SEC COMMENT 3.
C
X(NPR+KPTWO) = X(NPR+KPTWO) + XPO(ITN)
XPO(ITN) = X(NPR+KPTWO)
Y(NPR+KPTWO) = Y(NPR+KPTWO) + YPO(ITN)
YPO(ITN) = Y(NPR+KPTWO)
Z(NPR+KPTWO) = Z(NPR+KPTWO) + ZPO(ITN)
ZPO(ITN) = Z(NPR+KPTWO)
C
KSP2 IS GREATER THAN ZERO IF SHADOW COMPUTATIONS ARE REQUIRED.
C
IF(KSP2.GT.0) GO TO 2300
C
RETURN
C
1000 RIJK= ((X(IK-S) -X(JK-S))**2 + (Y(IK-S) - Y(JK-S))**2
* (Z(IK-S) -Z(JK-S))**2 - R(IJS)**2) * 0.5D0 + RIJK
GO TO 300
C
1100 X(NPR+KPTWO) = GMSUN * FXIJK + X(NPR+KPTWO)
Y(NPR+KPTWO) = GMSUN * FYIJK + Y(NPR+KPTWO)
Z(NPR+KPTWO) = GMSUN * FZIJK + Z(NPR+KPTWO)
GO TO 600
C
1200 RIJK = XIJO**2 + YIJO**2 + ZIJO**2
R(IJO) = DSQRT(RIJK)
THETA(IJO) = R(IJO)/RIJK/RIJK
FXIJK = THETA(IJO) * XIJO

```

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103950
103960
103970

103990
104000
104010
104020
104030
104040
104050
104060

A(KTR-1) = 0.00
 THETAC(KTR-1) = 0.00
 IF(ISP.GT.0) GMSUN = GMSUN - SPC
 GO TO 1450

1550 GMSUN = -SPC
 GO TO 1440

SOLAR PRESSURE SHADOW SERIES.

2000 AK = R(IJK)*R(IJO)
 ITNM2 = ITN - 2
 L = ITNM2/2

NOTE THAT, PROVIDED THAT K IS GREATER THAN ZERO, THEN AT THE END
 OF DO-LOOP 300 IJS = (K-1) UNITS AND IJKMS = 1 UNIT.
 L IS CHOSEN SUCH THAT IF ITN IS EVEN THEN $L = (ITN-1-L)-1$ AND
 IF ITN IS ODD THEN $L = (ITN-1-L)-2$. IN THE LATTER CASE AN
 EXTRA TERM MUST BE ADDED TO AK. THE LATTER CONDITION IS
 EQUIVALENT TO IJKMS = IJS.

IF(L.LE.1) GO TO 2200

DO 2100 S = 2,L

AK = R(IJKMS)*R(IJS) - A(S)*A(ITN-1-S) + AK

IJKMS = IJKMS + UNIT

IJS = IJS - UNIT

2100 CONTINUE

2200 IF(IJKMS.LE.IJS) AK = (R(IJS)**2 - A(L+1)**2) * 0.500 + AK

A(ITNM2) = AK/A(1)

GO TO 600

IJK AT THIS POINT EQUALS (K+1) UNITS.

2300 THETAK = 0.00

DO 2400 S = 1,ITNM2

THETAK = X(NSU-ONE+S*ONE) * X(NPR+K+ONE-S*ONE)


```

1      + Y(NSU-ONE+S*ONE) * Y(NPR+K+ONE-S*ONE)
2      + Z(NSU-ONE+S*ONE) * Z(NPR+K+ONE-S*ONE)
3      + A(S)*R(NSUNPS+IJK-S*UNIT) + THETAK

```

2400 CONTINUE

THETAC(ITNM2)= THETAK

RETURN

C

END

104510
104520
104530
104540
104550
104560
104570
104580

0316 CARDS

A-3.2 SUBROUTINE EXPAND

SUBROUTINE EXPAND (KEY,NNA)	96950
IMPLICIT REAL*8(A-H,O-Z)	96960
INTEGER*4 ONE	96970
DIMENSION IDUMMY(2),U(2394),V(2394)	96980
COMMON BLOCK - REDUCED FORM	96990
COMMON /ACOM/	97000
1CNM(136),SNM(136),F(171),C00,C20,EXTRA(99),UMT(2394),VMT(2394)	97010
2,LCT(16),ICT(17),ONE	97020
COMMON /CCOM/	97030
1XPO(16),YPO(16),ZPO(16),XBD(160),YBD(160),ZBD(160),CGB(14),SGB(14)	97040
2,XTL(14),YTL(14),CLB(14),SLB(14),CLT(14),SLT(14),VRB(14)	97050
3RPT(14),RMT(14),RMO(14),RZR(14),RMR(14)	97060
COMMON /DCOM/	97070
1HTS(12),CAV(12),CBV(12),ALT(12),CNA(12),CNB(12),XRD(14),YRD(14)	97080
2ZRD(14),XDD(14),YDD(14),ZDD(14),RHO(14),RPO(14),RVR(14),HNV(14)	97090
3VRN(14),VSR(14)	97100
COMMON /HCOM/	97110
1TON,TEN,EPS,TIN,DEL,SPC,PSA,FSA,TOJ,UPD,TOP,DTP	97120
2,CUD,CUV,CUT,ERD,XMU,ALF,OMG,ECC,CDC,CTW,XIT(6)	97130
COMMON /ICOM/	97140
1NBD,NTE,NHT,NSU,NPR,NPS,NOS,ICN,KTR,KDR,KVE,KDV,KSP,ISP,KIN,MPT	97150
COMMON BLOCK COMPLETED	97160
EQUIVALENCE (IDUMMY(1),I,XXXX),(IDUMMY(2),J2),	97170
*(U(1),UMT(1)),(V(1),VMT(1))	97180
EQUIVALENCE (ONE,J3)	97190
SIN(XXX) = DSIN(XXX)	97200
COS(XXX) = DCOS(XXX)	97210
EXP(XXX) = DEXP(XXX)	97220
ATAN(XXX) = DATAN(XXX)	97230
SQRT(XXX) = DSQRT(XXX)	97240
IF (KEY . GT. 2) GO TO 100	97250
XMUE = XMU / (ERD + ERD)	97260
J = 1	97270
DO 30 M = 1,NTE	97280
NM = LCT (M)	97290
IF(NM . LE. 0) GO TO 30	97300
XMN=XMUE	97310
I2MPI = M+M-1	97320
XMNO= I2MPI	97330
XDIV = 0.00	97340
DO 10 I = 1, I2MPI,2	97350
X=I	97360
10 XMN=XMN*X	97370
DO 20 K=1,NM	97380

	CNM (J) = CNM (J)*XMN	97390
	SNM (J) = SNM(J) * XMN	97400
	J= J+1	97410
	XMNO = XMNO + 2.00	97420
	XDIV = XDIV +1.00	97430
20	XMN = XMN * XMNO/XDIV	97440
30	CONTINUE	97450
	J1 = 1	97460
	NA = NTE +1	97470
	KMAZ = 0	97480
	LA = 0	97490
	LB = LCT (1)	97500
	IF(KVE.LE.2) GO TO 50	97510
	COO= 6.00*CNM(1)/ERD	97520
	C20= 14.00*CNM(3)/ERD	97530
	IF(LB.LE.2) C20= 0.00	97540
	IF (NA . GE. 3) GO TO 40	97550
	NA = 3	97560
	LCT (2) = 0	97570
40	KMAZ = 3	97580
	IF (LB . GT. 2) KMAZ = 5	97590
50	CONTINUE	97600
	DO 90 MPL = 1,NA	97610
	IF (LA . LT. (KMAZ-MPL)) LA = KMAZ-MPL	97620
	IF (LA . LT. LB) LA = LB	97630
	IF (MPL . GE. NA) GO TO 60	97640
	LC = LCT (MPL+1)	97650
	IF (LC . LE. 0) GO TO 60	97660
	IF (LA . LE. LC) LA = LC +1	97670
60	J3 = J1 + LA	97680
	J2 = J3 -1	97690
	IF (LA . LE. 0) GO TO 80	97700
	JPI = J1 + 1	97710
	XMSQ = (MPL-1) * (MPL-1)	97720
	XN = MPL	97730
	DO 70 J = JPI,J3	97740
	F(J) = (XMSQ - XN**2)/(4.00*XN**2 - 1.00)	97750
70	XN = XN + 1.00	97760
80	I = 1 - LA	97770
	IF (I . LT. 0) I = -1	97780
	IF (MPL .GT. 1) I = I + 2	97790
	IF (MPL . GE. NA) I = I + 3	97800
	F(J1) = XXXX	97810
	J1 = J3 + 1	97820

ICT(MPI)= J3	97830
LA = LB - 1	97840
LB = LC	97850
90 CONTINUE	97860
KEY = 3	97870
100 CONTINUE	97880
ITR=3	97890
K = 1	97900
KO=0	97910
KJ=1	97920
CGB(1)=DCOS(ALF)	97930
SGB(1)=DSIN(ALF)	97940
CLB(1)=XPO(1)*CGB(1)+YPO(1)*SGB(1)	97950
SLB(1)=YPO(1)*CGB(1)-XPO(1)*SGB(1)	97960
RPT(1)=XPO(1)*XPO(1)+YPO(1)*YPO(1)+ZPO(1)*ZPO(1)	97970
RMT(1)=1.00/RPT(1)	97980
CLT(1)=ERD*RM(1)*CLB(1)	97990
SLT(1)=ERD*RM(1)*SLB(1)	98000
RZR(1)=ERD*RM(1)*ZPO(1)	98010
RMR(1)=ERD*ERD*RM(1)	98020
RMO(1)=DSQRT(RMT(1))	98030
RMTWO= RMO(1)+RMO(1)	98040
U(1)= RMO(1)	98050
GO TO 490	98060
300 CONTINUE	98070
TX=0.00	98080
TY=0.00	98090
TZ=0.00	98100
KONE= KJ-ONE	98110
IF(NTE.LE.1) GO TO 340	98120
KO= LCT(1)	98130
L= ICT(1) + 1 + KONE	98140
LM1= 2 + KONE	98150
LPI=ICT(2)+ KONE	98160
IN= LCT(2)	98170
IF(IN.LE.0) GO TO 312	98180
DO 310 I=1, IN	98190
TX=(U(LM1+I)-U(LPI+I))*CNM(KO+I)- V(LPI+I) *SNM(KO+I)+TX	98200
TY=(U(LM1+I)+U(LPI+I))*SNM(KO+I)- V(LPI+I) *CNM(KO+I)+TY	98210
TZ = -U(L+I)*CNM(KO+I) - V(L+I)*SNM(KO+I) + TZ	98220
310 CONTINUE	98230
312 IF(NTE.LT.3)GO TO 340	98240
DO 330 MPI=3,NTE	98250
KO= KO+IN	98260

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LM1= L+1
L= LPI +1
LP1=ICT(MPI) + KONE
IN= LCT(MPI)
IF(IN.LE.0) GO TO 330
DO 320 I=1,IN
TX=(U(LM1+I)-U(LP1+I))*CNM(KO+I)+(V(LM1+I)-V(LP1+I))*SNM(KO+I)+TX
TY=(U(LM1+I)+U(LP1+I))*SNM(KO+I)-(V(LM1+I)+V(LP1+I))*CNM(KO+I)+TY
TZ= -U(L+I)*CNM(KO+I) - V(L+I)*SNM(KO+I) + TZ
320 CONTINUE
330 IN=LCT(1)
340 L= IN + 1
LP1= L+ 1 + KONE
L2= ICT(1) + LCT(2) + KONE + 2
TXO=0.00
TYO=0.00
DO 350 I=1,IN
TXO= -CNM(L-I)*U(L2-I) + TXO
TYO= -CNM(L-I)*V(L2-I) + TYO
TZ= -CNM(L-I)*U(LPI-I) + TZ
350 XTL(K) = TXO+TXO+TX
YTL(K) = TYO+TYO+TY
TX= DRX
TY= DRY
KPI = K+I
DO 360 I=1,K
TX=CGB(I)*XTL(KPI-I) - SGB(I)*YTL(KPI-I) + TX
TY=CGB(I)*YTL(KPI-I) + SGB(I)*XTL(KPI-I) + TY
360 XK=K*KPI
XPO(ITR)= TX/XK
YPO(ITR)= TY/XK
ZPO(ITR)= (TZ+TZ+DRZ)/XK
IF(NB0.GT.2) CALL ENEXPS(ITR)
IF(ITR.GE.KTR) RETURN
KPI= ITR
K= ITR-1
KMI=K-1
OMGK=KMI
OMGK=OMG/OMGK
L=K/2
ITR=ITR+1
R2K=XPO(1)*XPO(K)+YPO(1)*YPO(K)+ZPO(1)*ZPO(K)
RM1K=0.00
IF(L.LT.2) GO TO 380

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DC 370 N=2,L
R2K=XPO(N)*XPO(KPI-N)+YPO(N)*YPO(KPI-N)+ZPO(N)*ZPO(KPI-N)+R2K
370 RMIK=RMO(N)*RMO(KPI-N) + RMIK
380 R2K = R2K+R2K
RMIK= RMIK+RMIK
IF((L+L).GE.K) GO TO 390
R2K= XPO(L+1)**2 + YPO(L+1)**2 + ZPO(L+1)**2 + R2K
RMIK= RMO(L+1)**2 + RMIK
390 RPI(K)= R2K
CGB(K)= -OMGK*SGB(KMI)
SGB(K)= OMGK*CGB(KMI)
RCLA=XPO(1)*CGB(K) + YPO(1)*SGB(K) + XPO(K)*CGB(1) + YPO(K)*SGB(1)
RSLA=YPO(1)*CGB(K) - XPO(1)*SGB(K) + YPO(K)*CGB(1) - XPO(K)*SGB(1)
RHOC= 0.00
RHOSL= 0.00
RHODL= 0.00
RM2K= R2K*RM2(1)
IF(KMI.LT.2) GO TO 410
DO 400 N= 2,KMI
RHOC= CLB(N)*RMT(KPI-N) + RHOC
RHOSL= SLB(N)*RMT(KPI-N) + RHOSL
RHODL= ZPO(N)*RMT(KPI-N) + RHODL
RM2K = RPT(N)*RMT(KPI-N) + RM2K
RCLA = XPO(N)*CGB(KPI-N) + YPO(N)*SGB(KPI-N) + RCLA
RSLA = YPO(N)*CGB(KPI-N) - XPO(N)*SGB(KPI-N) + RSLA
400 CLB(K)= RCLA
410 SLB(K)= RSLA
RMT(K) = - RM2K*RMT(1)
CLT(K)= (CLB(1)*RMT(K)+RCLA*RMT(1)+ RHOC) * ERD
SLT(K)= (SLB(1)*RMT(K)+RSLA*RMT(1)+ RHOSL) * ERD
RZR(K) = (ZPO(1)*RMT(K) + ZPO(K)*RMT(1) + RHODL) * ERD
RMR(K)= RMT(K) * ERD*ERD
KU=KJ
KJ=K0+1
RMD(K) = (RMT(K)-RMIK)/RMTWO
U(KJ)= RMO(K)
490 CONTINUE
XXXX = F(1)
UA = 0.00
UB=0.00
VB=0.00
IF (I - GE. 0 ) G O TO 1000
UAN = 0.00
DO 500 N = 1, K

```

	UA = RZR (N) * U (KJ) + UA	99150
	UAM= RMR(N)*U(KJ) + UAM	99160
	UB= CLT(N)*U(KJ) + UB	99170
	VB= SLT(N)*U(KJ) + VB	99180
500	KJ = KJ - ONE	99190
	KJ = KO + 2	99200
	U(KJ) = UA	99210
	UA = UAM * F(2)	99220
	IF (J2 . LE. 2) GO TO 530	99230
	DO 520 J = 3, J2	99240
	UAM = 0	99250
	DO 510 N = 1, K	99260
	UA = RZR (N) * U (KJ) + UA	99270
	UAM= RMR(N)*U(KJ) + UAM	99280
510	KJ = KJ - ONE	99290
	KJ = KO + J	99300
	U (KJ) = UA	99310
520	UA = UAM * F(J)	99320
530	CONTINUE	99330
	DO 540 N = 1, K	99340
	UA = RZR (N) * U (KJ) + UA	99350
540	KJ = KJ - ONE	99360
542	J = J2 + 1	99370
	KJ = KO + J	99380
	U(KJ) = UA	99390
550	IF (J . GE. ONE) GO TO 570	99400
551	J = J + 1	99410
	KJ = KO + J	99420
	U (KJ) = UB	99430
	V(KJ) = VB	99440
	XXX = F(J)	99450
	UA = 0.00	99460
	UB = 0.00	99470
	VA = 0.00	99480
	VB = 0.00	99490
552	GO TO (552, 1020, 1040, 1060, 560, 570), I	99500
	UAM = 0.00	99510
	VAM = 0.00	99520
	DO 554 N = 1, K	99530
	UA = RZR (N) * U (KJ) + UA	99540
	VA = RZR (N) * V(KJ) + VA	99550
	UAM= RMR(N)*U(KJ) + UAM	99560
	VAM= RMR(N)*V(KJ) + VAM	99570
	UB = CLT (N) * U(KJ) - SLT (N) * V (KJ) + UB	99580


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554 VB = CLT (N) * V (KJ) + SLT (N) * U (KJ) + VB 99590
      KJ = KJ - ONE 99600
555 J = J + 1 99610
      KJ = KO + J 99620
      U(KJ) = UA 99630
      V(KJ) = VA 99640
      UA = UAM * F( J ) 99650
      VA = VAM * F(J) 99660
      IF (J . GE. J2) GO TO 560 99670
      J1 = J +1 99680
      DO 558 J = J1,J2 99690
        UAM = 0.00 99700
        VAM = 0.00 99710
        DO 556 N = 1,K 99720
          UA = RZR (N) * U (KJ) + UA 99730
          VA = RZR (N) * V(KJ) + VA 99740
          UAM= RMR(N)*U(KJ) + UAM 99750
          VAM= RMR(N)*V(KJ) + VAM 99760
556 KJ = KJ- ONE 99770
      KJ = KO + J 99780
      U(KJ)= UA 99790
      V(KJ) = VA 99800
      UA = UAM * F(J) 99810
      VA = VAM*F(J) 99820
558 CONTINUE 99830
560 DO 562 N= 1,K 99840
      UA = RZR (N) * U (KJ) + UA 99850
      VA = RZR (N) * V(KJ) + VA 99860
562 KJ = KJ-ONE 99870
564 J = J2+1 99880
      KJ = KO + J 99890
      U(KJ) = UA 99900
      V(KJ) = VA 99910
      GO TO 550 99920
570 CONTINUE 99930
      DRX=0.00 99940
      DRY=0.00 99950
      DRZ=0.00 99960
      IF (KDR . LE. 0 ) GO TO 300 99970
      C COMPUTE THE CORRECTION TERMS FOR DRAG 99980
      IF (KA-1)610,610,700 99990
610 TMA=SQRT(XPO(1)*XPO(1)+YPO(1)*YPO(1)) 10000
      TMB=ZPO(1)/TMA 100010
      TMC=ATAN(TMB) 100020

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XAD= TMC	100470
TMA=TMA+1.00	100480
XRD(KA)=TMA*XPO(KC)-XAD	100490
YRD(KA)=TMA*YPO(KC)-YAD	100500
ZRD(KA)=TMA*ZPO(KC)	100510
TMA=0.00	100520
KC=KA	100530
K=KA/2	100540
DO 720 I=1,K	100550
TMA=TMA+XRD(I)*XRD(KC)+YRD(I)*YRD(KC)+ZRD(I)*ZRD(KC)	100560
720 KC=KC-1	100570
TMA=TMA+TMA	100580
IF (KC-K) 740,740,730	100590
730 TMA=TMA+XRD(KC)*XRD(KC)+YRD(KC)*YRD(KC)+ZRD(KC)*ZRD(KC)	100600
740 VSR(KA)=TMA	100610
TMB=RPRT(KA)	100620
KC=KB	100630
IF (KB-1) 770,770,750	100640
750 DO 760 I=2,KB	100650
TMA=TMA-VRB(I)*VRB(KC)	100660
TMB=TMB-RPO(I)*RPO(KC)	100670
760 KC=KC-1	100680
770 VRB(KA)=TMA/(2.0*VRB(1))	100690
RPO(KA)=TMB/(2.0*RPO(1))	100700
IF (KA-2) 780,780,790	100710
780 TMB=ECC*RZR(1)/SQRT(1.0-ECC*RM(1)*ZPO(1)*ZPO(1))	100720
TMA=RPO(2)-TMB*(ZPO(1)*RMO(1)*RPO(2)-ZPO(2))	100730
TMB=CPB*RHO(1)	100740
HDI=TMA	100750
GO TO 810	100760
790 KC=KB-1	100770
TMA=KB	100780
TMA=CPB/TMA	100790
TMB=HDI*RHO(KB)	100800
TMC=2.00	100810
DO 800 I=3,KA	100820
TMB=TMB+TMC*RPO(I)*RHO(KC)	100830
TMC=TMC+1.00	100840
800 KC=KC-1	100850
810 RHO(KA)=TMA*TMB	100860
TMA=0.00	100870
KC=KA	100880
DO 820 I=1,KA	100890
TMA=TMA+RHO(I)*VRB(KC)	100900

TMD=ERD/637816.500	100030
TME=0.00	100040
KB=10	100050
GO TO 630	100060
620 TMC=ATAN(TMB*(TME+TMF)/(TME+TMF*(1.0-ECC)))	100070
630 TMF = ERD / DSQRT(1.00-ECC*SIN(TMC)**2)	100080
HIT=TMA/COS(TMC)-TMF	100090
TMC=HIT-TME	100100
TME=HIT	100110
IF (TMC)640,670,650	100120
640 TMC=-TMC	100130
650 KB=KB-1	100140
IF (TMC-TMD)670,670,660	100150
660 IF (KB) 670,670,620	100160
670 CONTINUE	100170
DO 680 I=1,NHT	100180
K=I	100190
IF (HIT-ALT(I))680,690,690	100200
680 CONTINUE	100210
690 CPA=CNA(K)	100220
CPB=CNB(K)	100230
CTW=CPB	100240
XAD=-OMG*YPO(1)	100250
YAD= OMG*XPO(1)	100260
XRD(1)=XPO(2)-XAD	100270
YRD(1)=YPO(2)-YAD	100280
ZRD(1)=ZPO(2)	100290
VSR(1)=XRD(1)*XRD(1)+YRD(1)*YRD(1)+ZRD(1)*ZRD(1)	100300
VRB(1)=DSQRT(VSR(1))	100310
RPO(1)=DSQRT(RPT(1))	100320
RHU(1)=CPA*EXP(CPB*HIT)	100330
RVR(1)=RHO(1)*VRB(1)	100340
TMA=CDC*RVR(1)	100350
XDD(1)=XRD(1)*TMA	100360
YDD(1)=YRD(1)*TMA	100370
ZDD(1)=ZRD(1)*TMA	100380
GO TO 840	100390
700 IF (ITR-KDR)710,710,300	100400
710 KB=KA-1	100410
KC=KA+1	100420
TMA=KB	100430
TMB=OMG/TMA	100440
TMC=-TMB*YAD	100450
YAD= TMB*XAD	100460

XAD= TMC	100470
TMA=TMA+1.00	100480
XRD(KA)=TMA*XPO(KC)-XAD	100490
YRD(KA)=TMA*YPO(KC)-YAD	100500
ZRD(KA)=TMA*ZPO(KC)	100510
TMA=0.00	100520
KC=KA	100530
K=KA/2	100540
DO 720 I=1,K	100550
TMA=TMA+XRD(I)*XRD(KC)+YRD(I)*YRD(KC)+ZRD(I)*ZRD(KC)	100560
720 KC=KC-I	100570
TMA=TMA+TMA	100580
IF (KC-K) 740,740,730	100590
730 TMA=TMA+XRD(KC)*XRD(KC)+YRD(KC)*YRD(KC)+ZRD(KC)*ZRD(KC)	100600
740 VSR(KA)=TMA	100610
TMB=RPT(KA)	100620
KC=KB	100630
IF (KB-1) 770,770,750	100640
750 DO 760 I=2,KB	100650
TMA=TMA-VRB(I)*VRB(KC)	100660
TMB=TMB-RPO(I)*RPO(KC)	100670
760 KC=KC-I	100680
770 VRB(KA)=TMA/(2.0*VRB(1))	100690
RPO(KA)=TMB/(2.0*RPO(1))	100700
IF (KA-2) 780,780,790	100710
780 TMB=ECC*RZR(1)/SQR(1.0-ECC*RM(1)*ZPO(1)*ZPO(1))	100720
TMA=RPO(2)-TMB*(ZPO(1)*RMO(1)*RPO(2)-ZPO(2))	100730
TMB=CPB*RHO(1)	100740
HDT=TMA	100750
GO TO 810	100760
790 KC=KB-I	100770
TMA=KB	100780
TMA=CPB/TMA	100790
TMB=HDT*RHO(KB)	100800
TMC=2.00	100810
DO 800 I=3,KA	100820
TMB=TMB+TMC*RPO(I)*RHO(KC)	100830
TMC=TMC+1.00	100840
800 KC=KC-I	100850
810 RHO(KA)=TMA*TMB	100860
TMA=0.00	100870
KC=KA	100880
DO 820 I=1,KA	100890
TMA=TMA+RHO(I)*VRB(KC)	100900

820	KC=KC-1	100910
	RVR(KA)=TMA	100920
	KC=KA	100930
	TMA=0.00	100940
	TMB=0.00	100950
	TMC=0.00	100960
	DO 830 I=1,KA	100970
	TMD=RVR(I)	100980
	TMA=TMA+TMD*XRDK(KC)	100990
	TMB=TMB+TMD*YRDK(KC)	101000
	TMC=TMC+TMD*ZRDK(KC)	101010
830	KC=KC-1	101020
	XDD(KA)=CDC*TMA	101030
	YDD(KA)=CDC*TMB	101040
	ZDD(KA)=CDC*TMC	101050
840	DRX=XDD(KA)	101060
	DRY=YDD(KA)	101070
	DRZ=ZDD(KA)	101080
	K=KA	101090
	GO TO 300	101100
1000	CONTINUE	101110
	DO 1010 N = 1, K	101120
	UA = RZR (N) * U (KJ) + UA	101130
	UB = CLT(N)*U(KJ) + UB	101140
	VB = SLT(N)*U(KJ) + VB	101150
1010	KJ = KJ-ONE	101160
	GO TO 542	101170
1020	CONTINUE	101180
	DO 1030 N = 1,K	101190
	UA = RZR (N) * U (KJ) + UA	101200
	VA = RZR (N) * V(KJ) + VA	101210
	UB = CLT (N) * U(KJ) - SLT (N) * V (KJ) + UB	101220
	VB = CLT (N) * V (KJ) + SLT (N) * U (KJ) + VB	101230
1030	KJ = KJ-ONE	101240
	GO TO 564	101250
1040	CONTINUE	101260
	DO 1050 N = 1,K	101270
	UB = CLT (N) * U(KJ) - SLT (N) * V (KJ) + UB	101280
	VB = CLT (N) * V (KJ) + SLT (N) * U (KJ) + VB	101290
1050	KJ = KJ-ONE	101300
	GO TO 551	101310
1060	CONTINUE	101320
	UAM = 0.00	101330
	VAM = 0.00	101340

```

DO 1070 N = 1, K
  UA = RZR (N) * U (KJ) + UA
  VA = RZR (N) * V (KJ) + VA
  UAM = RMR (N) * U (KJ) + UAM
  VAM = RMR (N) * V (KJ) + VAM
1070 KJ = KJ - ONE
      GO TO 555
      END

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101350
 101360
 101370
 101380
 101390
 101400
 101410
 101420

0448 CARDS

A-3.3 SUBROUTINE VARIEQ

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SUBROUTINE VARIEQ
IMPLICIT REAL*8(A-H,O-Z)
INTEGER*4 ONE
DIMENSION TMT(9)
COMMON BLOCK - REDUCED FORM
COMMON /ACOM/
1CNM(136),SNM(136),F(171),C00,C20,EXTRA(99),UMT(2394),VMT(2394)
2,LCT(16),ICT(17),ONE
COMMON /CCGM/
1XPO(16),YPO(16),ZPO(16),XBD(160),YBD(160),ZBD(160),CGB(14),SGB(14)
2,CSQ(14),XVR(14),SSQ(14),YVR(14),SCS(14),ZVR(14)
3,QAV(14),QBV(14),QCV(14),BXB(14),BYB(14),BZB(14)
COMMON /DCOM/
1H,S(12),CAV(12),CBV(12),ALT(12),CNA(12),CNB(12),XRD(14),YRD(14),
2ZRD(14),XDD(14),YDD(14),ZDD(14),RHO(14),RPO(14),RVR(14),HNV(14),
3VIN(14),VSR(14)
COMMON /FCOM/
1AMT(126),BMT(126),EMT(126),FXXMY(14),TWOXY(14),FXZ(14),FYZ(14)
2,SPARE(70)
COMMON /HCOM/
1TON,TEN,EPS,TIN,DEL,SPC,PSA,FSA,TOJ,UPD,TOP,DTP
2,CUD,CUV,CUT,ERD,XMU,ALF,OMG,ECC,CDC,CTW,XIT(6)
COMMON /ICOM/
INBO,NTE,NHT,NSU,NPR,NPS,NOS,ICN,KTR,KDR,KVE,KOV,KSP,ISP,KIN,MPT
DATA I,L,KA,KB,KC,KDG /6*0/
DATA AU,AV,BU,BV,CU,CV,CFO,TMQ,CTH,TMR,IMS,TMT /20*0.DO/
COMMON BLOCK COMPLETED
EQUIVALENCE (TMT(1),TMA),(TMT(2),TMB),(TMT(3),TMC)
EQUIVALENCE (TMT(4),TMD),(TMT(5),TME),(TMT(6),TMF)
EQUIVALENCE (TMT(7),TMG),(TMT(8),TMH),(TMT(9),TMI)
C
C INITIALIZE ALL OF THE EXTERNAL ARRAYS.
KMAX= KVE-2
IF(KMAX.LE.0) RETURN
CSQ(1)= CGB(1)**2 - 0.500
SCS(1)= CGB(1)*SGB(1)
TWOMEG= OMG+OMG
K= 1
I02= 3
I12= ICT(1) + 2
I22= ICT(2) + 1
KDG= KOV-2
IF(KMAX.LT.KDG) KDG= KMAX
IF(KDG.LE.0) GO TO 100

```


CTH= CDC*OMG	105030
CFO= CDC*CTW	105040
HNV(1)=1.00/RPO(1)	105050
VRN(1)=1.00/VSR(1)	105060
L=9*KDG	105070
CALL CLEAR (BMT,L)	105080
	105090
C 100 CONTINUE	105100
FXXMY(Y(K)= C00*UMT(I22) + C20*UMT(I22+2)	105110
TWO*XY(K)= C00*VMT(I22) + C20*VMT(I22+2)	105120
FXZ(K) = C00*UMT(I12) + C20*UMT(I12+2)	105130
FYZ(K) = C00*VMT(I12) + C20*VMT(I12+2)	105140
FZZK = C00*UMT(I02) + C20*UMT(I02+2)	105150
	105160
TMA= -0.500*FZZK	105170
TMB= 0.00	105180
TMC= 0.00	105190
TMF= 0.00	105200
KMI= K	105210
DO 110 I= 1,K	105220
TMA= CSQ(I)*FXXMY(Y(KMI) - SCS(I)*TWO*XY(KMI) + TMA	105230
TMB= SCS(I)*FXXMY(Y(KMI) + CSQ(I)*TWO*XY(KMI) + TMB	105240
TMC= CGB(I)*FXZ(KMI) - SGB(I)*FYZ(KMI) + TMC	105250
TMF= SGB(I)*FXZ(KMI) + CGB(I)*FYZ(KMI) + TMF	105260
110 KMI= KMI-1	105270
	105280
L= 9*K	105290
AMT(L) = FZZK	105300
AMT(L-4)= -FZZK - TMA	105310
AMT(L-8)= TMA	105320
AMT(L-7)= TMB	105330
AMT(L-5)= TMB	105340
AMT(L-6)= TMC	105350
AMT(L-2)= TMC	105360
AMT(L-3)= TMF	105370
AMT(L-1)= TMF	105380
IF(KDG.LE.0) GO TO 500	105390
CALL CLEAR(TMT,9)	105400
KA= K-1	105410
310 KDG=KDG-1	105420
KB=KA+1	105430
IF (KA) 350,350,320	105440
320 KC=KA	105450
DO 330 I=2,KB	105460

	TMA=TMA-HNV(KC)*RPO(I)	105470
	TMB=TMB-VRN(KC)*VSR(I)	105480
	KC=KC-1	105490
330	HNV(KB)=TMA*HNV(I)	105500
	VRN(KB)=TMB*VRN(I)	105510
	TMA=0.000	105520
	TMB=0.000	105530
350	KC=KB	105540
	DO 360 I=1,KB	105550
	TMA=RVR(KC)	105560
	TMB=TMB+TMA*XPO(I)	105570
	TMC=TMC+TMA*YPO(I)	105580
	TMD=TMD+TMA*ZPO(I)	105590
	TMA=VRN(I)	105600
	TME=TME+TMA*XDD(KC)	105610
	TMF=TMF+TMA*YDD(KC)	105620
	TMG=TMG+TMA*ZDD(KC)	105630
360	KC=KC-1	105640
	BXB(KB)=TMB	105650
	BYB(KB)=TMC	105660
	BZB(KB)=TMD	105670
	XVR(KB)=TME	105680
	YVR(KB)=TMF	105690
	ZVR(KB)=TMG	105700
	THR=-OMG*TMF	105710
	TMS=OMG*TME	105720
	CALL CLEAR (TMT,9)	105730
	KC=KB	105740
	DO 380 I=1,KB	105750
	TMO=HNV(I)	105760
	TMA=TMA+TMQ*BXB(KC)	105770
	TMB=TMB+TMQ*BYB(KC)	105780
	TMC=TMC+TMQ*BZB(KC)	105790
380	KC=KC-1	105800
	QAV(KB)=CFO*TMA+TMR	105810
	QBV(KB)=CFO*TMB+TMS	105820
	QCV(KB)=CFO*TMC	105830
	TMA=0.000	105840
	TMB=0.000	105850
	TMC=0.000	105860
	KC=KB	105870
	DO 400 I=1,KB	105880
	AU=XRD(KC)	105890
	BU=YRD(KC)	105900

CU=ZRD(KC)	105910
AV=QAV(I)	105920
BV=QBV(I)	105930
CV=QCV(I)	105940
TMA=TMA+AU*AV	105950
TMB=TMB+BU*AV	105960
TMC=TMC+CU*AV	105970
TMD=TMD+AU*BV	105980
TME=TME+BU*BV	105990
TMF=TMF+CU*BV	106000
TMG=TMG+AU*CV	106010
TMH=TMH+BU*CV	106020
TMI=TMI+CU*CV	106030
KC=KC-1	106040
TMQ=CTH*RRV(KB)	106050
TMB=TMB-TMQ	106060
TMD=TMD+TMQ	106070
L=9*KA+1	106080
DO 410 I=1,9	106090
AMT(L)=TMT(I)+AMT(L)	106100
L=L+1	106110
CALL CLEAR(TMT,9)	106120
IF(KDG)500,500,420	106130
420 CONTINUE	106140
TMA=CDC*RRV(KB)	106150
TME=TMA	106160
TMI=4.000*TMA	106170
KC=KB	106180
DU 430 I=1,KB	106190
AU=YVR(KC)	106200
BU=ZVR(KC)	106210
AV=XRD(I)	106220
BV=YRD(I)	106230
TMA=TMA+XVR(KC)*AV	106240
TMB=TMB+AU*AV	106250
TMC=TMC+BU*AV	106260
TME=TME+AU*BV	106270
TMF=TMF+BU*BV	106280
KC=KC-1	106290
TMD=TMB	106300
TMG=TMC	106310
TMH=TMF	106320
TMI=TMI-TMA-TME	106330
L=9*KA+1	106340

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DD 450 I=1,9
BMT(L)=TMT(I)
450 L=L+1
500 CONTINUE
IF(K.GE.KMAX) RETURN
KMI=K
TWOMGK=KMI
TWOMGK= TWOMEG/TWOMGK
K=K+1
I02= I02 + ONE
I12= I12 + ONE
I22= I22 + ONE
CSQ(K)= -SCS(KMI)*TWOMGK
SCS(K)= CSQ(KMI)*TWOMGK
GO TO 100
END

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106350
106360
106370
106380
106390
106400
106410
106420
106430
106440
106450
106460
106470
106480
106490
106500

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0192 CARDS

A-3.4 SUBROUTINE FINALP

SUBROUTINE FINALP	137790
IMPLICIT REAL*8(A-H,O-Z)	137800
	137810
	137820
PURPOSE TO PRINT FINAL RESULTS AND RESIDUALS	137830
	137840
	137850
INPUT FILES IARCIN - ARC STABLE PARAMETERS	137860
IPASIN - PASS STABLE PARAMETERS	137870
	137880
OUTPUT FILES NONE	137890
	137900
	137910
	137920
	137930
COMMON BLOCKS	137940
	137950
	137960
COMMON /GENCOM/	137970
1 CONVG,	SUM1,
2 COST,	MXDIVG,
3 ITERS,	ITERNO,
4 IAUTH,	IUNITS,
5 IPRRES,	ISIGNO,
6 MXARCS,	IUPDNO,
7 IPGNO,	NSTA,
	MXMEAS,
	MXSTA,
	MXLIN,
	PGID(10)
	138030
	138040
	138050
	138060
COMMON /TYLE/	138070
1 TITLE(100)	138080
	138090
	138100
COMMON /TSPARM/	138110
1 NOTS,	TSLABL(200), TSINT(200),
2 TSCUR(200),	TSCWT(200), TSDELT(200),
3 ITSEVL(200),	TS2LAB(200), TS2INI(200)
	138140
	138150
	138160
COMMON /ASPARM/	138170
1 NOAS,	ASLABL(200), ASINT(200),
2 ASCUR(200),	ASCNT(200), ASDELT(200),
3 IASEVL(200),	AS2LAB(200), AS2INT(200)
	138200
	136210

C									138220
	COMMON /PSPARM/								138230
	1 NCPS,	NOPS2,	PSLABL(200),	PSINT(200),					138240
	2 PSCUR(200),	PSIWT(200),	PSCWT(200),	PSDELT(200),					138250
	3 IPSEVL(200),	PS2EVL(200),	PS2INT(200)						138260
C									138270
C									138280
	COMMON /CWORK/								138290
	1 ICATA(500),	CATA(500),	ICTL,	NINT,					138300
	2 NFLT								138310
C									138320
C									138330
	COMMON /IONUMB/								138340
	1 MFILE,	ISFILE,	IARCIN,	IPASIN,					138350
	2 IARCOT,	IPASCT,	ICARD,	IRESID,					138360
	3 ITAPE,	IALPFA,	LUA,	LUB,					138370
	4 LUC								138380
C									138390
C									138400
	COMMON /STINFO/								138410
	1 STLABL(100),	STLAT(100),	STLON(100),	STHT(100),					138420
	2 ISTSUR(100),	ISTSID(100)							138430
C									138440
C									138450
	COMMON /ACINFO/								138460
	1 ACLABL(100),	EPOCH(100),	EPOCHD(100),	GHA(100),					138470
	2 IROTAT(100),	IATAB(100,6),	IAPNO(100,6)						138480
C									138490
C									138500
	COMMON /EARTH/ ROTAT,	GRHA,	RADIUS,	GRAV,	ECC				138510
C									138520
C									138530
	DIMENSION XI(6),	XC(6),	XL(6)						138540
	DIMENSION NFLAG(3)								138550
	DATA N601/601/,	NFLAG/1,2,3/,	DATA2/100.00/,	IX/0/,	DATA3/1.D20/				138560
C									138570
C									138580
C	FORMAT STATEMENTS								138590
C									138600
C									138610
	5001 FORMAT(0,39X,' F I N A L R E S U L T S')								138620
	5002 FORMAT(0,9X,'COMMENTS ',9A8,A3/, (20X,9A8,A3))								138630
	5003 FORMAT(//,10X,'NUMBER OF ITERATIONS PERFORMED',I5)								138640
	5004 FORMAT(0,9X,'ANALYSIS TERMINATED BY')								138650

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5005 FORMAT(' ',32X,'MAXIMUM ITERATIONS')
5006 FORMAT(' ',32X,'CONVERGENCE')
5007 FORMAT(' ',32X,'DIVERGENCE')
5008 FORMAT(' ',32X,'MAXIMUM DIVERGENT ITERATIONS')
5009 FORMAT('0',9X,'CONVERGENCE RATIO (COST FUNCTION)',F20.8)
5010 FORMAT('0',9X,'PARAMETER PARAMETER',7X,'APRIORI',11X,
'CALCULATED',11X,'TCTAL',13X,'APRIORI',11X,'CALCULATED',/,
1 12X,'NUMBER',6X,'LABEL',10X,'VALUE',15X,'VALUE',11X,
2 'CORRECTION',11X,'SIGMA',15X,'SIGMA')
3
5011 FORMAT('0',4X,60(' '))
5012 FORMAT('0',35X,'TOTALLY STABLE PARAMETERS')
5013 FORMAT('0',25X,'ARC STABLE PARAMETERS ARC NO.',I4,X,A8)
5014 FORMAT('0',10X,'PASS STABLE PARAMETERS ARC NO.',I4,X,
1 A8,6X,'STATION NO.',I4,X,A8,6X,'PASS NO.',I4)
5015 FORMAT('0',12X,I3,7X,A8,1P,D18.8,4D19.8)
5016 FORMAT('0',25X,'STATE VECTOR ARC NO.',I4,X,A8)
5017 FORMAT('0',9X,'EARTH CENTERED INERTIAL COORDINATES')
5018 FORMAT('///',10X,'EARTH CENTERED FIXED COORDINATES')
5019 FORMAT('0',20X,'LABEL',12X,'APRIORI',15X,'CALCULATED',I4X,
1 'TOTAL',/,39X,'VALUE',18X,'VALUE',15X,'CORRECTION')
5020 FORMAT('0',19X,A8,1P,3(7X,D15.8))
C
C
C DISPLAY COMMENTS AND COST FUNCTION, ETC
C
C
CALL PAGE
WRITE (6,5001)
WRITE (6,5002) TITLE
WRITE (6,5003) ITERNO
WRITE (6,5004)
GO TO ( 11, 12, 13, 14 ), ITERS
GO TO 15
11 CONTINUE
WRITE (6,5006)
GO TO 15
12 CONTINUE
WRITE (6,5005)
GO TO 15
13 CONTINUE
WRITE (6,5007)
GO TO 15
14 CONTINUE
WRITE (6,5008)

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15 CONTINUE
WRITE (6,5009) COST
C
C
C DISPLAY TOTALLY STABLE PARAMETER RESULTS
C
C
IF( NOTS .LE. 0 ) GC TO 30
ICNT = MXLIN + 1
NEXT=10
DO 25 I=1,NOTS
IF( ICNT .LT. MXLIN ) GC TO 22
CALL PAGE
WRITE (6,5001)
WRITE (6,5011)
WRITE (6,5012)
WRITE (6,5011)
WRITE (6,5010)
ICNT = 11
22 CONTINUE
CALL SIGWT (2,SIGI,TSIWT(I) )
CALL SIGWT(2,SIGC,TSICWT(I) )
CORR = TSCUR(I) - TSINT(I)
WRITE (6,5015) I,ISLBI(I),TSINT(I),TSCUR(I),CORR,SIGI,SIGC
WRITE VALUES ON DISK TO UPDATE 601 CARDS
WRITE (10) N601,ISLBI(I),TSCUR(I)
ICNT = ICNT + 2
25 CONTINUE
C
C
C DISPLAY ARC STABLE PARAMETER RESULTS
C
C
30 CONTINUE
IRD = 0
C
C READ ARC STABLE RECORD
C
C
32 CONTINUE
READ (IARCIN,END=90C) ICIL,NINI,NELI,(IDATA(I),I=1,NINI),
1 (DATA(I),I=1,NFLT)
IF( ICTL .NE. 1 ) GC TO 32
IARC = IDATA(1)
NOAS = IDATA(2)

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139100
139110
139120
139130
139140
139150
139160
139170
139180
139190
139200
139210
139220
139230
139240
139250
139260
139270
139280
139290
139300
139310
139320
139330
139340
139350
139360
139370
139380
139390
139400
139410
139420
139430
139440
139450
139460
139470
139480
139490
139500
139510
139520
139530

C		139540
C		139550
C	IF(NOAS .LE. 0) GC TO 60	139560
C		139570
C	STORE ARC STABLE PARAMETERS	139580
C		139590
C		139600
	DO 34 I=1,NOAS	139610
	IASEVL(I) = IDATA(I+2)	139620
	J = 6*I - 5	139630
	ASLABL(I) = DATA(J)	139640
	ASINT(I) = DATA(J+1)	139650
	ASCUR(I) = DATA(J+2)	139660
	ASINT(I) = DATA(J+3)	139670
	ASCHT(I) = DATA(J+4)	139680
	ASDELT(I) = DATA(J+5)	139690
	34 CONTINUE	139700
C		139710
C	ISOLATE AND DISPLAY STATE VECTOR	139720
C		139730
	DO 350 I=1,6	139740
	J = IASTAB(IARC,I)	139750
	K = IAPNO(IARC,I)	139760
	GO TO (351,352),J	139770
	GO TO 35	139780
	351 CONTINUE	139790
	XI(I) = TSINT(K)	139800
	XC(I) = TSCUR(K)	139810
	XL(I) = TSLABL(K)	139820
	GO TO 350	139830
	352 CONTINUE	139840
	XI(I) = ASINT(K)	139850
	XC(I) = ASCUR(K)	139860
	XL(I) = ASLABL(K)	139870
	350 CONTINUE	139880
	CALL PAGE	139890
	WRITE (6,5001)	139900
	WRITE (6,5011)	139910
	WRITE (6,5016) IARC,ACLABL(IARC)	139920
	WRITE (6,5011)	139930
	WRITE (6,5017)	139940
	WRITE (6,5019)	139950
	DO 354 I=1,6	139960
	CORR = XC(I) - XI(I)	139970
	WRITE (6,5020) XL(I),XI(I),XC(I),CORR	

```

354 CONTINUE
IF( IROTAT(IARC) .LE. 0 ) GO TO 35
WRITE (6,5018)
WRITE (6,5019)
GRHA = GHAI(IARC)
CALL ROTFIX(XI,EPOCH(IARC))
CALL ROTFIX(XC,EPOCH(IARC))
DO 356 I=1,6
CORR = XC(I) - XI(I)
WRITE (6,5020) XL(I), XI(I),XC(I), CORR
356 CONTINUE
C
C
35 CONTINUE
ICNT = MXLIN + 1
DO 38 I=1,NOAS
IF( ICNT .LT. MXLIN ) GO TO 36
CALL PAGE
WRITE (6,5001)
WRITE (6,5011)
WRITE (6,5013) IARC,ACLABL(IARC)
WRITE (6,5011)
WRITE (6,5010)
ICNT = 11
36 CONTINUE
CALL SIGWT(2,SIGI,ASIWT(I))
CALL SIGWT(2,SIGC,ASCWT(I))
CORR = ASCUR(I) - ASINT(I)
WRITE (6,5015) I,ASLABL(I),ASINT(I),ASCUR(I),CORR,SIGI,SIGC
WRITE (10) N601,ASLABL(I),ASCUR(I)
WRITE ON DISK TO UPDATE 601 CARDS
C
ICNT = ICNT + 2
38 CONTINUE
C
C
C DISPLAY PASS STABLE PARAMETER RESULTS
C
C
60 CONTINUE
IF( IRD .NE. 0 ) GO TO 66
62 CONTINUE
REAC (IPASIN,END=900) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),
1 (DATA(I),I=1,NFLT)
IF( ICTL .NE. 1 ) GO TO 62

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139980
139990
140000
140010
140020
140030
140040
140050
140060
140070
140080
140090
140100
140110
140120
140130
140140
140150
140160
140170
140180
140190
140200
140210
140220
140230
140240
140250
140260
140270
140280
140290
140300
140310
140320
140330
140340
140350
140360
140370
140380
140390
140400
140410

```

KARC = IDATA(1)	140420
ISTA = IDATA(2)	140430
IPASS = IDATA(3)	140440
NOPS = IDATA(4)	140450
C	140460
C STORE PASS STABLE PARAMETERS	140470
IF(NOPS .LE. 0) GO TO 66	140480
DO 64 I=1,NOPS	140490
IPSEVL(I) = IDATA(I+4)	140500
J = '6'I - 5	140510
PSLABL(I) = DATA(J)	140520
PSINT(I) = DATA(J+1)	140530
PSCUR(I) = DATA(J+2)	140540
PSIWT(I) = DATA(J+3)	140550
PSCWT(I) = DATA(J+4)	140560
PSDELT(I) = DATA(J+5)	140570
64 CONTINUE	140580
C	140590
C	140600
66 CONTINUE	140610
IF(KARC .EQ. IARC) GO TO 70	140620
IRD = 1	140630
GO TO 32	140640
C	140650
C	140660
70 CONTINUE	140670
IF(NOPS .LE. 0) GO TO 62	140680
ICNT = MXLIN + 1	140690
NEMT=10	140700
DO 76 I=1,NOPS	140710
IF(ICNT .LE. MXLIN) GO TO 74	140720
CALL PAGE	140730
WRITE (6,5001)	140740
WRITE (6,5011)	140750
WRITE (6,5014) IARC,ACLABL(IARC),ISTA,SLABL(ISTA),IPASS	140760
WRITE (6,5011)	140770
WRITE (6,5010)	140780
ICNT = 11	140790
74 CONTINUE	140800
CALL SIGWT(2,SIGI,PSIWT(I))	140810
CALL SIGWT(2,SIGC,PSCWT(I))	140820
CORR = PSCUR(I) - PSINT(I)	140830
WRITE (6,5015) I,PSLABL(I),PSINT(I),PSCUR(I),CORR,SIGI,SIGC	140840
MN=ISTA*2-2+I	140850

	WRITE (10) N601,PSLABL(1),PSCUR(1)	140860
	WRITE CN DISK TO UPDATE 601 CARDS	140870
C	ICNT = ICNT + 2	140880
	76 CONTINUE	140890
	GO TO 62	140900
C		140910
C		140920
C	END OF PRINT OUT	140930
C		140940
C		140950
C	900 CONTINUE	140960
	REWIND IARCIN	140970
	REWIND IPASIN	140980
		140990
C		141000
C		141010
	CALL RESID	141020
C		141030
C		141040
	RETURN	141050
	END	

0331 CARDS

A-3.5 SUBROUTINE RESID

A-3.5.1 STANDARD SUBROUTINE RESID

	SUBROUTINE RESID		130840
	IMPLICIT REAL*8(A-H,O-Z)		130850
	LOGICAL*1 LFILE,GRAPH,SYM,SI,BLNK,SO		130860
C			130870
C			130880
C	PURPOSE	COMPUTE, DISPLAY, AND OUTPUT MEASUREMENT RESIDUALS	130890
C			130900
C			130910
C			130920
C	COMMON BLOCKS		130930
	COMMON /COMSOL/	U(100,100), C(100),	AUTOR(20),
1	ASUM(20),	APROC(20),	ANUMB(20),
2	EPS(20),	EPSL(20),	B(20,40),
3	RES(20),	E,	B1,
4	Z,	TIME,	WT,
5	ALP,	DIS,	SIG,
6	YY,		TEST,
A	NBP(20,40),	NBPL(20,40),	NBL(20),
B	NMSNO(20),	NMEAS,	NSIZEU,
C	NSIZEM,	NMSPT,	NPAR,
D	ISTA,	IPASS,	JARC,
E	JPASS,	KARC,	KSTA,
F	IAFLAG,	IPFLAG,	NPARS,
G	IPNO,	ITY,	IA,
H	LA,	LB,	IPRU,
I	ICNT,	IWRK(20)	IAR,
	COMMON /TSPARM/	NOTS,	
1	TSINT(200),	TSCUR(200),	NOTS2,
2	TSDLT(200),	ITSEVL(200),	TS2LAB(200),
			TS2INT(200)
C			
	COMMON /ASPARM/	NOAS,	
1	ASINT(200),	ASCUR(200),	ASLABL(200),
2	ASDELT(200),	IASEVL(200),	ASCWT(200),
			AS2LAB(200),
			AS2IWT(200)
C			
	COMMON /PSPARM/	NOPS,	
1	PSINT(200),	PSCUR(200),	PSLABL(200),
2	PSDELT(200),	IPSEVL(200),	PSCWT(200),
			PS2LAB(200),
			PS2IWT(200)
C			
	COMMON /CWORK/	IDATA(500),	ICIL,
1	NINT,	NFLT	
C			
	COMMON /MSINFO/	XMLABL(300),	MSTYPE(300)
C			
C			

COMMON /ACINFO/	ACLABL(100),	EPOCH(100),	EPOCHD(100),	131270
1	GRA(100),	IROTAT(100),	IATAB(100,6),	IAPNO(100,6)
				131280
				131290
C				
COMMON /STINFO/	STLABL(100),	STLAT(100),	STLON(100),	131300
1	STHT(100),	ISTSUR(100),	ISTSID(100)	131310
				131320
C				
COMMON /GENCOM/				131330
1CONVG	,DIVRG	,SUMO	,SUMI	131340
2COST	,MXITER	,MXDIVG	,ITERNO	131350
ALTERSW				131360
3IDIVNO	,IUNITS	,IGEOTL	,IAUTOR	131370
4IOINP	,ISIGNO	,IUPDNO	,IPRRES	131380
5NARCS	,NSTA	,MXMEAS	,MXARCS	131390
6MXPARM	,MXSTA	,MXLIN	,IPGNO	131400
7	PGIC(10)			131410
				131420
C				
COMMON /CDEBUG/	IDFLG(2),	IPRFLG(2),	ISLFLG(2)	131430
				131440
C				
COMMON /TYLE/	TYILE(100)			131450
				131460
C				
COMMON /IONUMB/	MFILE,	ISFILE,	IARCIN,	131470
1	IPASIN,	IARCCT,	ICARD,	131480
2	IRESID,	ITAPE,	IALPHA	131490
				131500
C				
				131510
C				
DIMENSION XMSNA(20)				131520
DIMENSION GRAPH(83),KI(2),SYM(2)				131530
DATA SYM/'L','M','/GRAPH/83*'				131540
DATA SI/'I','/BLNK/'				131550
DATA ISEQ/O/				131560
DATA XMSNA/'RANGE	, 'AZ COS E', 'ELEV	, 'RA COS D',		131570
1	'DECLIN	, 'COS ALPHA', 'COS BETA', 'X 30		131580
2	'Y 30	, 'ALTIMETR', 'R DOT	, 'AZ DOT	131590
3	'ELEV OCT', 'X 85	, 'Y 85		131600
4				131610
				131620
C				
FORMAT STATEMENTS				131630
				131640
C				
5001 FORMAT('0',20X,'M E A S U R E M E N T	R E S I D U A L S',			131650
1	19X,'ITERATION NO.',I4)			131660
5002 FORMAT('0',10X,'DESIGNATION	MEASUREMENT	MEASUREMENT',4X,		131670
1	'MEASUREMENT',13X,'ALPHA',/29X,'LABEL',8X,'NUMBER',10X,			131680
2	'TYPE',18X,'USED')			131690
5003 FORMAT('0',10X,'DESIGNATION	MEASUREMENT	MEASUREMENT',4X,		131700

1	'MEASUREMENT',/,29X,'LABEL',8X,'NUMBER',10X,'TYPE')	131710
5004	FORMAT('0',12X,'MEAS',12,8X,A8,8X,14,7X,I3,'-',A8,5X,D15.8)	131720
5005	FORMAT('0',YR MO DA HR MI SEC',6X,'MEAS',12,9X,'MEAS',12)	131730
5006	FORMAT('0',4X,'NO. CF PCINTS',4X,F11.0,5(7X,F11.0),/)	131740
1	{15X,6F18.0}	131750
5007	FORMAT('0',8X,'MEAN',6X,6(3X,D15.8),/,(19X,6(3X,D15.8)))	131760
5008	FORMAT('0',STANDARD DEVIATION',6(3X,D15.8),/,(19X,6(3X,D15.8)))	131770
5009	FORMAT('0',22X,'ARC NO.',14,3X,A8,3X,'STATION NO.',14,3X,A8,	131780
1	3X,'PASS NO.',14)	131790
5010	FORMAT('0',12,4I3,F6.2)	131800
5011	FORMAT('0',21X,D12.4)	131810
5012	FORMAT('0',35X,D12.4)	131820
5013	FORMAT('0',57X,D15.8)	131830
5014	FORMAT('0',75X,D15.8)	131840
5015	FORMAT('0',93X,D15.8)	131850
5016	FORMAT('0',111X,D15.8)	131860
5017	FORMAT(24X)	131870
5801	FORMAT('1',10X,'PREMATURE END OF FILE ENCOUNTERED ON IARCIN',)	131880
1	'PROGRAM TERMINATED')	131890
5802	FORMAT('1',10X,'PREMATURE END OF FILE ENCOUNTERED ON IPASIN',)	131900
1	'PROGRAM TERMINATED')	131910
		131920
		131930
		131940
		131950
	INITIALIZATION	131960
	REWIND ISFILE	131970
	REWIND IARCIN	131980
	REWIND IPASIN	131990
	REWIND IALPHA	132000
	REWIND IRESID	132010
	REWIND IARCOT	132020
		132030
	CLEAR ALL STORAGE AREAS	132040
	DO 5 I=1,NSIZEM	132050
	NB(I) = 0	132060
	NBL(I) = 0	132070
	CMW(I) = 0.00	132080
	EPS(I) = 0.00	132090
	EPSL(I) = 0.00	132100
	AUTOR(I) = 0.00	132110
	ASUM(I) = 0.00	132120
	APROD(I) = 0.00	132130
	ANUMB(I) = 0.00	132140
	NVSN(I) = 0	

DO 5 J=1, NSIZEB	132150
NBP(I,J) = 0.00	132160
NBPL(I,J) = 0.00	132170
B(I,J) = 0.00	132180
BL(I,J) = 0.00	132190
5 CONTINUE	132200
COVAR=0.00	132210
C	132220
C	132230
LFILS=.FALSE.	132240
GRAPH(42)=SI	132250
C SET FLAGS FOR 1ST ARC + PASS	132260
IASQLN = 0	132270
IPSQLN = 0	132280
C	132290
C READ CONTROL FILE	132300
C	132310
100 CONTINUE	132320
READ (ISFILE,END=4000)ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),	132330
1 (DATA(I),I=1,NFLT)	132340
C	132350
GO TO (1000, 2000, 3000), ICTL	132360
GO TO 100	132370
C	132380
C	132390
C	132400
C BEGINNING OF AN ARC	132410
C	132420
C	132430
C	132440
1000 CONTINUE	132450
C	132460
C TEST FOR FIRST ARC	132470
IF(IASQLN.NE.0) GO TO 1002	132480
IASQLN = 1	132490
GO TO 1010	132500
C	132510
C GO TO PRINT STATISTICS ROUTINE	132520
1002 CONTINUE	132530
ISTAT = 1	132540
GO TO 6000	132550
1004 CONTINUE	132560
C	132570
C READ + STORE ARC PARAMETERS	132580
C	

1010 CONTINUE	132590
IARC = IDATA(1)	132600
1012 CONTINUE	132610
READ (IARCIN,END=41C0) ICIL,NINT,NFLT,(IDATA(I),I=1,NINT),	132620
1 (DATA(I),I=1,NFLT)	132630
C	132640
C IF NOT TYPE 1 RECORD, READ AGAIN	132650
IF(ICIL.NE.1) GC TO 1012	132660
C	132670
C STORE PARAMETERS	132680
NOAS = IDATA(2)	132690
KARC = IDATA(1)	132700
C	132710
C SET FLAGS FOR FIRST PASS OF AN ARC	132720
IPSCN = 0	132730
IF(NOAS.LE. 0) GC TO 1018	132740
DO 1016 I=1,NOAS	132750
IASEVL(I) = IDATA(I+2)	132760
J = 6*I - 5	132770
ASLABL(I) = DATA(J)	132780
ASIN(I) = DATA(J+1)	132790
ASCUR(I) = DATA(J+2)	132800
ASINT(I) = DATA(J+3)	132810
ASCWT(I) = DATA(J+4)	132820
ASDEL(I) = DATA(J+5)	132830
1016 CONTINUE	132840
1018 CONTINUE	132850
GO TO 100	132860
C	132870
C	132880
C BEGINNING OF A PASS	132890
C	132900
C	132910
2000 CONTINUE	132920
C	132930
C IF NOT FIRST PASS OF AN ARC, PRINT STATISTICS FROM LAST PASS	132940
IF(IPSCN.NE. 0) GO TO 2002.	132950
IPSCN = 1	132960
GO TO 2008	132970
2002 CONTINUE	132980
:STAT = 2	132990
GO TO 6000	133000
2004 CONTINUE	133010
C	133020

C	STORE MEASUREMENT INFO FOR THIS PASS	133030
C		133040
	2008 CONTINUE	133050
	KARC = IDATA(1)	133060
	ISTA = IDATA(2)	133070
	IPASS = IDATA(3)	133080
	NMEAS = IDATA(4)	133090
	DO 2010 I=1,NMEAS	133100
	NMSNO(I) = IDATA(I+4)	133110
	CMW(I) = DATA(I)	133120
	2010 CONTINUE	133130
C		133140
C	IF FINAL PRINT AND AUTOREGRESSIVE CONSTANTS USED, READ IALPHA	133150
C	AND SCORE CONSTANTS	133160
C		133170
	IF ((ITERSW.EQ.0) .OR.	133180
	1 (IAUTOR.NE.0)) GO TO 2020	133190
	READ (IALPHA) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),	133200
	1 (DATA(I),I=1,NFLT)	133210
	DO 2016 I=1,NMEAS	133220
	DO 2014 J=1,NMEAS	133230
	IF(IDATA(I+4) .NE. NMSNO(J)) GO TO 2014	133240
	AUTGR(J) = DATA(I)	133250
	GO TO 2016	133260
	2014 CONTINUE	133270
	2016 CONTINUE	133280
C		133290
C	READ PASS STABLE PARAMETERS	133300
C		133310
	2020 CONTINUE	133320
	READ (IPASIN,END=41C1) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),	133330
	1 (DATA(I),I=1,NFLT)	133340
	IF(ICTL.NE. 1) GC TO 2020	133350
		133360
C		133370
C	STORE PARAMETER VALUES FROM TYPE 1 RECORD	133380
	JARC = IDATA(1)	133390
	JSTA = IDATA(2)	133400
	JPASS = IDATA(3)	133410
	NOPS = IDATA(4)	133420
	IF(NOPS.LE.0) GC TO 2030	133430
	DO 2024 I=1,NOPS	133440
	IPSEVL(I) = IDATA(I+4)	133450
	J = 6*I - 5	133460
	PSLABL(I) = DATA(J)	

PSINT(I) = DATA(J+1)	133470
PSCUR(I) = DATA(J+2)	133480
PSWT(I) = DATA(J+3)	133490
PSCWT(I) = DATA(J+4)	133500
PSDELT(I) = DATA(J+5)	133510
2024 CONTINUE	133520
C	133530
C	133540
C	133550
2030 CONTINUE	133560
CALL PAGE	133570
WRITE (6,5001) ITERNO	133580
WRITE (6,5009) JARC, ACLABL(IARC), ISTA, STLABL(ISTA), IPASS	133590
IF ((ITERSW .NE. 0) .AND.	133600
1 IAUTOR .EQ. 0) GO TO 2036	133610
C	133620
C	133630
NO AUTOREGRESSIVE CONSTANTS PRINTED	133640
WRITE (6,5003)	133650
DO 2034 I=1,NMEAS	133660
WRITE (6,5004) I, XMLABL(NMSNO(I)), NMSNO(I), MSTYPE(NMSNO(I)),	133670
1 XMSNA(MSTYPE(NMSNO(I)))	133680
2034 CONTINUE	133690
GO TO 2040	133700
C	133710
C	133720
PRINT ALPHAS Y00	133730
2036 CONTINUE	133740
WRITE (6,5002)	133750
DO 2038 I=1,NMEAS	133760
WRITE (6,5004) I, XMLABL(NMSNO(I)), NMSNO(I), MSTYPE(NMSNO(I)),	133770
1 XMSNA(MSTYPE(NMSNO(I))), AUTOR(I)	133780
2038 CONTINUE	133790
C	133800
C	133810
2040 CONTINUE	133820
WRITE (6,5005) (I,I=1,NMEAS)	133830
ICNT = 10 + 2 *NMEAS	133840
GO TO 100	133850
C	133860
C	133870
C	133880
C	133890
MEASUREMENT POINT RECORD	133900
3000 CONTINUE	
C	

C	CHECK FOR PAGE OVERFLOW	133910
	IF(ICNT.LT. MXLIN) GO TO 3002	133920
	CALL PAGE	133930
	WRITE (6,5001) ITERNO	133940
	WRITE (6,5009) IARC,ACLABL(IARC),ISTA,STLABL(ISTA),IPASS	133950
	WRITE (6,5005) (I,I=1,NMEAS)	133960
	ICNT = 7	133970
	3002 CONTINUE	133980
C		133990
C	CONVERT DAYS + TIME TO YR,MON,DAY,HR,MIN,SEC + DISPLAY	134000
	CALL DAYHMS(DATA(1),DATA(2),IYR,IMO,IDA,IHR,IMIN,SEC)	134010
	WRITE (6,5010) IYR,IMO,IDA,IHR,IMIN,SEC	134020
		134030
C	PROCESS THE MEASUREMENT POINT RECORD	134040
		134050
C		134060
C	CLEAR STORAGE AREAS	134070
	DO 3004 I=1,NSIZEM	134080
	EPS(I) = 0.00	134090
	RES(I) = 0.00	134100
	NB(I) = 0	134110
	IWORK(I) = 0	134120
	DO 3004 J=1,NSIZEB	134130
	B(I,J) = 0	134140
	3004 CONTINUE	134150
C		134160
C	STORE MEASUREMENT DISCREPENCIES	134170
	NMSPT = IDATA(1)	134180
	NPAR = IDATA(2)	134190
	DO 3008 I=1,NMSPT	134200
	DO 3006 J=1,NMEAS	134210
	IF(ICATA(I+2) .NE. NMSNC(J)) GO TO 3006	134220
	IWORK(J) = NMSNC(J)	134230
	EPS(J) = DATA(I+2)	134240
	GO TO 3008	134250
	3006 CONTINUE	134260
C	NO MATCH ERROR	134270
	3008 CONTINUE	134280
C		134290
C	STORE PARTIALS BY MEASUREMENT NO INDICATOR	134300
		134310
	IF(NPAR .LE. 0) GO TO 2016	134320
	DO 3012 I=1,NPAR	134330
C	CALCULATE PARAMETER NO	134340
	IPNC = IDATA(I*3+NMSPT +1)	

```

ITY = IDATA(I*3+NMSPT) 134350
MNO = IOATA(I*3+NMSPT+2) 134360
IF( ITY .GE. 2 ) IPNO = IPNO + NOTS 134370
IF( ITY .EQ. 3 ) IPNO = IPNO+NOAS 134380
C 134390
FIND MEAS NO INDICATOR 134400
DO 3010 J=1,NMEAS 134410
IF( MNO .NE. NMSNO(J) ) GO TO 3010 134420
NB(J) = NB(J) + 1 134430
B(J,NB(J)) = DATA(NMSPT+I+2) 134440
NBP(J,NB(J)) = IPNO 134450
GO TO 3012 134460
3010 CONTINUE 134470
C 134480
NO MATCH ERROR 134490
3012 CONTINUE 134500
C 134510
CALCULATE RESIDUALS AND DISPLAY 134520
C 134530
OUTPUT RESIDUALS IF FINAL CALL TO RESID 134540
C 134550
3016 CONTINUE 134560
DO 3036 I=1,NMEAS 134570
SKIP TO NEXT LINE IF LINE IS FULL 134580
J = I/6*6 + 1 134590
IF( I.NE.1 ).AND.( I.EQ.J ) WRITE(6,5017) 134600
IF( EPS(I) .EQ. 0.DC ) GO TO 3036 134610
E = EPS(I) 134620
C 134630
CHECK FOR USE OF AUTOREGRESSIVE CONSTANTS 134640
IF( ITERSW .NE. 0 ).AND.( IAUTOR.EQ. 0 ) E = E - AUTOR(I)*EPSL(I) 134650
RES(I) = E 134660
C 134670
IF NO PARTIALS, DISPLAY AND GO TO NEXT MEAS 134680
IF( NB(I) .LE. 0 ) GO TO 3034 134690
NPARS = NB(I) 134700
DO 3032 J=1,NPARS 134710
BI = B(I,J) 134720
C 134730
CHECK FOR USE OF AUTOREGRESSIVE CONSTANTS 134740
IF( ITERSW .NE. 0 ).AND.( IAUTOR.EQ. 0 ) BI = BI - AUTOR(I)*BL(I,J) 134750
IPNO = NBP(I,J) 134760
IF( IPNO .GT. NOTS ) GO TO 3020 134770
RES(I) = RES(I) - TSDLT(IPNO) * BI 134780
GO TO 3032 134790
3020 CONTINUE 134800
IPNO = IPNO - NOTS 134810
IF( IPNO .GT. NOAS ) GO TO 3022 134820
RES(I) = RES(I) - ASDEL(I*3+NMSPT) * BI 134830
GO TO 3032 134840

```



```

3022 CONTINUE
IPNC = IPNO - NOAS
RES(I) = RES(I) - PSELT(IPNO) * B1
134790
134800
134810
134820
134830
134840
134850
134860
134870
134880
134890
134900
134910
134920
134930
134940
134950
134960
134970
134980
134990
135000
135010
135020
135030
135040
135050
135060
135070
135080
135090
135100
135110
135120
135130
135140
135150
135160
135170
135180
135190
135200
135210
135220

3032 CONTINUE
PRINT CALCULATED RESIDUALS
C
3034 CONTINUE
J = I
3024 IF( J .LE. 6 ) GO TO 3026
J = J - 6
GO TO 3024
3026 CONTINUE
GO TO (3041,3042,3043,3044,3045,3046),J
3041 CONTINUE
WRITE (6,5011) RES(I)
GO TO 3050
3042 CONTINUE
WRITE (6,5012) RES(I)
GO TO 3050
3043 CONTINUE
WRITE (6,5013) RES(I)
GO TO 3050
3044 CONTINUE
WRITE (6,5014) RES(I)
GO TO 3050
3045 CONTINUE
WRITE (6,5015) RES(I)
GO TO 3050
3046 CONTINUE
WRITE (6,5016) RES(I)
3050 CONTINUE
C
C ACD TO COUNTS, SUMS, PRODUCTS
ANUMB(I) = ANUMB(I) + 1.00
ASUM(I) = ASUM(I) + RES(I)
APROD(I)=APROD(I)+RES(I)*#2
3036 CONTINUE
COVAR=CQVAR + RES(I)* RES(I)
DO 3090 I=1,2
IF (RES(I)) 3070,3070,3080
3070 KK=(RES(I)-.050-04)/(-.20-04)
IF (KK .GT. 40) KK=41
GRAPH (42-KK)=SYM(I)
K1(I)=42-KK
GO TO 3090

```

```

3080 KK=(RES(I)+.05D-04)/.2D-04
      IF (KK .GT. 40) KK=41
      GRAPH(42+KK)=SYM(I)
      KI(I)=42+KK
3090 CONTINUE
      IF (KI(I) .NE. KI(2)) GO TO 3095
      GRAPH(KI(I))=S0
3095 WRITE (6,3091) GRAPH
3091 FORMAT ('+',49X,83A1)
      GRAPH(KI(I))=BLNK
      GRAPH(KI(2))=BLNK
      IF (KI(I) .EQ. 42) GRAPH(42)=SI
      IF (KI(2) .EQ. 42) GRAPH(42)=SI
      ICNT = ICNT + (NMEAS+5)/6
C
C
C IF FINIAL CALL TO RESID, GUPUT RESIDUALS
C
      IF( ITERSW .EQ. 0 ) GO TO 3060
C
      ICTL = 1
      NINT = NMEAS + 4
      NFLT = NMEAS + 2
C
      WRITE(IRESID) ICTL,NINT,NFLT,IARC,ISTA,IPASS,NMEAS,
C
      * (IWORK(I),I=1,NMEAS),DATA(1),DATA(2),(RES(I),I=1,NMEAS)
C
C IF USING AUTOREGRESSIVE CONSTANTS MOVE CURRENT VALUES TO PREVIOUS
3060 CONTINUE
      IF(IITERSW.EQ.0).OR.(IAUTOR.NE.0)) GO TO 100
      DO 3066 I=1,NSIZEM
        NBL(I) = NB(I)
        EPSL(I) = EPS(I)
      DO 3066 J=1,NSIZEB
        BL(I,J) = B(I,J)
        NBPL(I,J) = NBP(I,J)
3066 CONTINUE
      GO TO 100
C
C
C DISPLAY RESIDUAL STATISTICS
C
C
C
6000 CONTINUE
      WRITE (6,5006) (ANUMB(I),I=1,NMEAS)
C
      COMPUTE MEAN AND STANDARD DEVIATION

```

```

GO 6004 I=1,NMEAS
IF( ANUMB(I) .LE. 1.00 ) GO TO 6002
APROD(I) = DSQRT((APROD(I)-ASUM(I)**2/ANUMB(I))/(ANUMB(I)-1.00))
ASUM(I) = ASUM(I)/ANUMB(I)
GO TO 6004
6002 APROD(I) = 0.00
6004 CONTINUE
WRITE (6,5007) (ASUM(I),I=1,NMEAS)
WRITE (6,5008) (APROD(I),I=1,NMEAS)
IF (ANUMB(I) .LE. 1.00) SCV=0.00
IF (ANUMB(I) .GT. 1.00) SCV= (COVAR-ANUMB(I)*ASUM(2))/
((ANUMB(I)-1.00)*APROD(I)*APROD(2))
*
WRITE (6,8000) SCV
8000 FORMAT (0,'CORRELATION COEFFICIENT',3X,F6.2)
C
WRITE RESIDUALS ON SUMMARY FILE
9000 FORMAT (1H1,30X,'MEAS 1',11X,'MEAS 2',11X,'MEAS 1',
11X,'MEAS 2',5X,'COEFFICIENT'//)
*
IF (LFILE) GO TO 9050
LFILE = .TRUE.
WRITE (34,9000)
WRITE (34,9002)
9001 FORMAT (1X,13,3X,A8,3(2X,13),213,15,13,1X,F5.2,1X,4(D15.8,2X),
F7.2)
*
9050 WRITE (34,9001) ISTA,STLABL(ISTA),IARC,IPASS,
IYR,IMO,IDA,IHR,IMIN,SEC
ASUM(I),A UM(2),APROD(1),APROD(2),SCV
C
WRITE ON DISK TO BE USED BY SUMMARY PRINT PROGRAM
C
CUTPUT : MEAS 2 LABEL, MEAS 2 NO.,CORRELATION COEFFICIENT,
MEAN 1, STD DEV 1, MEAN2, STD DEV 2
C
WRITE (10) XMLABL(NMSNO(2)),NMSNO(2),SCV,ANUMB(2),ASUM(1),
APROD(1),ASUM(2),APROD(2)
*
C
IF( ITERS .EQ. 0 ) GO TO 6010
IC = 1
NI = 4 + NMEAS
NF = 3 * NMEAS
WRITE (IARCOT) IC,NI,NF,IARC,ISTA,IPASS,NMEAS,(NMSNO(I),I=1,NMEAS)
1 , (ANUMB(I),ASUM(I),APROD(I),I=1,NMEAS)
6010 CONTINUE
C

```

C	CLEAR ARRAYS	136110
	DO 6008 I=1, NSIZEB	136120
	ANUMB(I) = C.D0	136130
	ASUM(I) = 0.C0	136140
	APRCD(I) = C.D0	136150
	NMSNO(I) = 0	136160
	NBL(I) = 0	136170
	DO 6008 J= 1, NSIZEB	136180
	BL(I,J) = 0.D0	136190
	NBPL(I,J) = 0	136200
	6008 CONTINUE	136210
	COVAR=0.D0	136220
C		136230
	GO TO (1004, 2004, 4004), ISTAT	136240
C		136250
C		136260
C		136270
C	END OF INPUT DATA	136280
C		136290
	4000 CONTINUE	136300
	ISTAT = 3	136310
	GO TO 6000	136320
	4004 CONTINUE	136330
	ENDFILE IARCOT	136340
	REWIND IARCOT	136350
C	ENOFIL IRESID	136360
C	REWIND IRESID	136370
	REWIND ISFILE	136380
	REWIND IARCIN	136390
	REWIND IPASIN	136400
	REWIND IALPHA	136410
	ENDFILE IO	136420
	REWIND IO	136430
	RETURN	136440
C		136450
C		136460
C	PREMATURE END OF FILE - IARCIN. - ERROR	136470
	4100 CONTINUE	136480
	WRITE (6,5801)	136490
	4103 CONTINUE	136500
	STOP	136510
C		136520
C	PREMATURE END OF FILE - IPASIN - ERROR	136530
	4101 CONTINUE	136540

WRITE (6,5802)

GO TO 4103

END

136550

136560

136570

0576 CARDS

A-3.5.2 SPECIAL SUBROUTINE RESID

SUBROUTINE RESID 130840
 IMPLICIT REAL*8(A-H,O-Z) 130850
 LOGICAL*1 LFILE,GRAPH,SYM,SI,BLNK,SO 130860
 130870
 130880
 130890
 130900
 130910
 130920
 130930

PURPOSE COMPUTE, DISPLAY, AND OUTPUT MEASUREMENT RESIDUALS

COMMON BLOCKS

COMMON /COMSOL/ U(110,110), C(110), ANUMB(20), CMW(20), 130950
 1 ASUM(20), APR00(20), B(20,40), BL(20,40), 130960
 2 EPS(20), E, TIME, DAYS, WT, 130970
 3 RES(20), E1, SIG, TEST, 130980
 4 Z, DIS, 130990
 5 ALP, 131000
 6 YY, 131010
 A NBP(20,40), NBL(20), NBL(20), 131020
 B NMSNO(20), NMEAS, NSIZEU, NSIZEB, 131030
 C NSIZEM, NMSPT, NPAR, IARC, 131040
 D ISTA, IPASS, JARC, JSTA, 131050
 E JPASS, KARC, KSTA, KPASS, 131060
 F IAFLAG, IPFLAG, NPARS, MNO, 131070
 G IPNO, ITY, IA, IB, 131080
 H LA, LB, IPRU, IAR, 131090
 I ICNT, IWORK(20) 131100

COMMON /TSPARM/ NOTS2, TSLABL(200), 131110
 1 TSINT(200), TSCUR(200), TSIWT(200), TSCWT(200), 131120
 2 TSDELT(200), ITSEVL(200), TS2LAB(200), TS2INT(200) 131130

COMMON /ASPARM/ NOAS2, ASLABL(200), 131140
 1 ASINT(200), ASCUR(200), ASIWT(200), ASCWT(200), 131150
 2 ASDELT(200), IASEVL(200), AS2LAB(200), AS2IWT(200) 131160
 131170

COMMON /PSPARM/ NOPS2, PSLABL(200), 131180
 1 PSINT(200), PSCUR(200), PSIWT(200), PSCWT(200), 131190
 2 PSDELT(200), IPSEVL(200), PS2LAB(200), PS2IWT(200) 131200
 131210

COMMON /CWORK/ IDATA(500), DATA(500), ICTL, 131220
 1 NINT, NFLT 131230
 131240
 131250
 131260
 131270

COMMON /MSINFO/ XMLABL(300), MSTYPE(300) 131280
 COMMON /ACINFO/ ACLABL(100), EPOCH(100), EPOCHD(100), 131290

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C      1  GHA(100),      IROTAT(100),      IASTAB(100,6),      IAPNO(100,6)      131280
      COMMON /STINFO/      STLABL(100),      STLAT(100),      STLON(100),      131290
      1  SHTT(100),      ISTSUR(100),      ISTSID(100)      131300
      131310
      131320
      131330
      COMMON /GENCOM/
      1CONVG      ,DIVRG      ,SUMO      ,SUMI      131340
      2COST      ,MXITER      ,MXDIVG      ,ITERNO      131350
      131360
      3DIDVNO      ,IUNITS      ,IGEOFL      ,IAUTOR      131370
      4IOINP      ,ISIGNO      ,IUPDNO      ,IPRRS      131380
      5NARCS      ,NSTA      ,MXMEAS      ,MXARCS      131390
      6MXPARM      ,MXSTA      ,MXLIN      ,IPGNO      131400
      7      PGID(10)      131410
      131420
C      COMMON /CDEBUG/      IDEFLG(2),      IPRFLG(2),      ISLFLG(2)      131430
      131440
C      COMMON /TYLE/      TITLE(100)      131450
      131460
C      COMMON /IONUMB/      MFILE,      ISFILE,      IARCIN,      131470
      1  IPASIN,      IARCOT,      IPASOT,      ICARD,      131480
      2  IRESID,      ITAPE,      IALPHA      131490
      131500
      131510
C      DIMENSION ADUM(6)
      DIMENSION XMSNA(20)
      DIMENSION GRAPH(83),K1(2),SYM(2)
      DATA SYM/'L','M','/','GRAPH/83*','/
      DATA SI/'I','BLNK/'/'/','SO/'*','/
      DATA ISEQ/0/
      DATA XMSNA/'RANGE      ','AZ COS E','ELEV      ','RA COS D',
      1  'DECLIN      ','COS ALPH','COS BETA','X 30      ',
      2  'Y 30      ','ALTIMETR','R DOT      ','AZ DOT      ',
      3  'ELEV DOT','X 85      ','Y 85      ',
      4  '      ','      ','      ','/'
C      FORMAT STATEMENTS
      131520
      131530
      131540
      131550
      131560
      131570
      131580
      131590
      131600
      131610
      131620
      131630
      131640

```

```

9001  FORMAT ( I4, I4, A8, I4, 2I3, I4, I3, F7.3, I5, 20I4.5,
*      20I2.3, I8, I5)
9002  FORMAT ( 79X 'STANDARD' /
1  52X 'MEAN ERROR' 16X 'DEVIATION' 11X 'NO. PTS.'/
2  2X 'STATION' 29X 'PASS' 6X 'MEAS' 10X 'MEAS' 9X 'MEAS'
3  8X 'MEAS' 7X 'MEAS MEAS' /

```


4 2X 'NO NAME' 6X 'Y M D H M SEC NO' 8X '1' 13X '2'

5 12X '1' 11X '2' 11X '1 2' ///)

5001 FORMAT(0',10X,'M E A S U R E M E N T R E S I D U A L S',

* 10X,'ARC',13,10X,'ITERATION',14///)

5017 FORMAT(24X)

5801 FORMAT(1',10X,'PREMATURE END OF FILE ENCOUNTERED ON IARCIN,',

1 'PROGRAM TERMINATED')

5802 FORMAT(1',10X,'PREMATURE END OF FILE ENCOUNTERED ON IPASIN,',

1 'PROGRAM TERMINATED')

131870

131880

131890

131900

131910

131920

131930

131940

131950

131960

131970

131980

131990

132000

132010

INITIALIZATION

REWIND ISFILE

REWIND IARCIN

REWIND IPASIN

REWIND IALPHA

REWIND IRESID

REWIND IARCOT

NUTAPE=35

NUPASS=36

NURITE=37

END FILE NURITE

IF(ITERSW.EQ.0) GO TO 4

REWIND 10

3 READ(10,END=4) N,X,Y

WRITE(NURITE) N,X,Y

GO TO 3

4 REWIND 10

132020

132030

132040

132050

132060

132070

132080

132090

132100

132110

132120

132130

132140

132150

132160

CLEAR ALL STORAGE AREAS

DO 5 I=1,NSIZEM

NB(I) = 0

NBL(I) = 0

CMW(I) = 0.00

EPS(I) = 0.00

EPSL(I) = 0.00

AUTOR(I) = 0.00

ASUM(I) = 0.00

APROD(I) = 0.00

ANUMB(I) = 0.00

NMSNO(I) = 0

DO 5 J=1,NSIZEB

NBP(I,J) = 0.00

IF(NOAS .LE. 0) GO TO 1018	132740
DO 1016 I=1,NOAS	132750
IASVL(I) = IDATA(I+2)	132760
J = 6*I - 5	132770
ASLVL(I) = DATA(J)	132780
ASINT(I) = DATA(J+1)	132790
ASCUR(I) = DATA(J+2)	132800
ASWT(I) = DATA(J+3)	132810
ASWT(I) = DATA(J+4)	132820
ASDEL(I) = DATA(J+5)	132830
CONTINUE	132840
1018 CONTINUE	132850
GO TO 100	132860
	132870
	132880
BEGINNING OF A PASS	132890
	132900
	132910
2000 CONTINUE	132920
STORE MEASUREMENT INFO FOR THIS PASS	133030
	133040
2008 CONTINUE	133050
KARC = IDATA(1)	133060
ISTA = IDATA(2)	133070
IPASS = IDATA(3)	133080
NMEAS = IDATA(4)	133090
DO 2010 I=1,NMEAS	133100
NMSNO(I) = IDATA(I+4)	133110
CMW(I) = DATA(I)	133120
	133130
2010 CONTINUE	133140
	133290
READ PASS STABLE PARAMETERS	133300
	133310
2020 CONTINUE	133320
READ (IPASIN,END=4101) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),	133330
1 (DATA(I),I=1,NFLT)	133340
IF(ICTL .NE. 1) GO TO 2020	133350
	133360
STORE PARAMETER VALUES FROM TYPE 1 RECORD	133370
JARC = IDATA(1)	133380
JSTA = IDATA(2)	133390
JPASS = IDATA(3)	133400
NOPS = IDATA(4)	133410

IF(NOPS .LE. 0) GO TO 100
 DO 2024 I=1,NOPS
 IPSEVL(I) = IDATA(I+4)
 J = 6*I - 5
 PSLABL(I) = DATA(J)
 PSINT(I) = DATA(J+1)
 PSCUR(I) = DATA(J+2)
 PSINT(I) = DATA(J+3)
 PSCWT(I) = DATA(J+4)
 PSDELT(I) = DATA(J+5)
 2024 CONTINUE
 C
 GO TO 100
 C
 MEASUREMENT POINT RECORD
 C
 3000 CONTINUE
 C
 CHECK FOR PAGE OVERFLOW
 IF(ICNT .LT. MXLIN) GO TO 3002
 CALL PAGE
 WRITE(6,5001) IARC,ITERNO
 WRITE(6,9002)
 ICNT = 7
 3002 CONTINUE
 C
 CONVERT DAYS + TIME TO YR,MON,DAY,HR,MIN,SEC + DISPLAY
 CALL DAYHMS(DATA(1),DATA(2),IYR,IMO,IDA,IHR,IMIN,SEC)
 C
 PROCESS THE MEASUREMENT POINT RECORD
 C
 CLEAR STORAGE AREAS
 DO 3004 I=1,NSIZEM
 EPS(I) = 0.00
 RES(I) = 0.00
 NB(I) = 0
 IWORK(I) = 0
 DO 3004 J=1,NSIZEB
 B(I,J) = 0
 3004 CONTINUE
 C
 STORE MEASUREMENT DISCREPANCIES
 C

C6

NMSPT = IDATA(1)	134170
NPAR = IDATA(2)	134180
DO 3008 I=1,NMSPT	134190
DO 3006 J=1,NMEAS	134200
IF(IDATA(I+2) .NE. NMSNO(J)) GO TO 3006	134210
IWORK(J) = NMSNO(J)	134220
EPS(J) = DATA(I+2)	134230
GO TO 3008	134240
3006 CONTINUE	134250
C NO MATCH ERROR	134260
3008 CONTINUE	134270
C	134280
STORE PARTIALS BY MEASUREMENT NO INDICATOR	134290
C	134300
C	134310
IF(NPAR .LE. 0) GO TO 3016	134320
DO 3012 I=1,NPAR	134330
CALCULATE PARAMETER NO	134340
IPNO = IDATA(I*3+NMSPT +1)	134350
ITY = IDATA(I*3+NMSPT)	134360
MNO = IDATA(I*3+NMSPT+2)	134370
IF(ITY .GE. 2) IPNO = IPNO + NOTS	134380
IF(ITY .EQ. 3) IPNO = IPNO+NOAS	134390
C FIND MEAS NO INDICATOR	134400
DO 3010 J=1,NMEAS	134410
IF(MNO .NE. NMSNO(J)) GO TO 3010	134420
NB(J) = NB(J) + 1	134430
B(J,NB(J)) = DATA(NMSPT+I+2)	134440
NBP(J,NB(J)) = IPNO	134450
GO TO 3012	134460
3010 CONTINUE	134470
C NO MATCH ERROR	134480
3012 CONTINUE	134490
C	134500
CALCULATE RESIDUALS AND DISPLAY	134510
OUTPUT RESIDUALS IF FINAL CALL TO RESID	134520
C	134530
3016 CONTINUE	134540
DO 3036 I=1,NMEAS	134550
C SKIP TO NEXT LINE IF LINE IS FULL	134560
J = I/6*6 + 1	134570
IF(I.NE.1).AND.(I.EQ.J)) WRITE(6,5017)	134580
IF(EPS(I) .EQ. 0.D0) GO TO 3036	134590
E = EPS(I)	134600
C CHECK FOR USE OF AUTOREGRESSIVE CONSTANTS	

```

IF((ITERSW .NE.0).AND.(IAUTOR.EQ.0)) E = E - AUTOR(I)*EPSL(I)
RES(I) = E
134610
134620
134630
134640
134650
134660
134670
134680
134690
134700
134710
134720
134730
134740
134750
134760
134770
134780
134790
134800
134810
134820
134830
134840

C
IF NO PARTIALS, DISPLAY AND GO TO NEXT MEAS
IF( NB(I) .LE. 0 ) GO TO 3034
NPARS = NB(I)
DO 3032 J=1,NPARS
BI = B(I,J)
CHECK FOR USE OF AUTOREGRESSIVE CONSTANTS
IF((ITERSW .NE.0).AND.(IAUTOR.EQ.0)) BI = BI -AUTOR(I)*BL(I,J)
IPNO = NBP(I,J)
IF( IPNO .GT. NOTS ) GO TO 3020
RES(I) = RES(I) - TSDEL(T(IPNO) * BI
GO TO 3032
3020 CONTINUE
IPNO = IPNO - NOTS
IF( IPNO .GT. NOAS ) GO TO 3022
RES(I) = RES(I) - ASDEL(T(IPNO) * BI
GO TO 3032
3022 CONTINUE
IPNO = IPNO - NOAS
RES(I) = RES(I) - PSDEL(T(IPNO) * BI
3032 CONTINUE
C PRINT CALCULATED RESIDUALS
3034 CONTINUE
3036 CONTINUE
READ(NUPASS) NOSTA,NOPASS,L1,L2,SIGMA1,SIGMA2
WRITE(6,9001) ISTA,STLABL(ISTA),IYR,IMO,IDA,IHR,IMIN,SEC,IPASS,
* RES(1),RES(2),SIGMA1,SIGMA2,L1,L2
IF((ITERSW.NE.0) WRITE(NURITE) XMLABL(NMSNO(2)),NMSNO(2),L1,L2,
* XMLABL(NMSNO(1)),RES(1),SIGMA1,RES(2),SIGMA2
ICNT= ICNT+1
CLEAR ARRAYS
DO 6008 I=1,NSIZEM
NMSNO(I) = 0
NBL(I) = 0
DO 6008 J= 1,NSIZEB
BL(I,J) = 0.00
NBPL(I,J) =0
6008 CONTINUE
GO TO 100
136110
136120
136160
136170
136180
136190
136200
136210
136230
136270
136280
136290

C
C
C
C
END OF INPUT DATA

```

4000 CONTINUE 136300
 REWIND ISFILE 136380
 REWIND IARCIN 136390
 REWIND IPASIN 136400
 REWIND IALPHA 136410
 REWIND NUPASS

IF(ITERSW.EQ.0) RETURN
 END FILE NURITE
 4010 READ(NUTAPE,END=4020) ADUM
 WRITE(NURITE) ADUM
 GO TO 4010
 4020 REWIND NURITE
 RETURN

C 136450
 C 136460
 C 136470
 4100 PREMATURE END OF FILE - IARCIN - ERROR
 CONTINUE 136480
 WRITE (6,5801) 136490
 4103 CONTINUE 136500
 STOP 136510
 136520

C 136530
 C 136540
 4101 PREMATURE END OF FILE - IPASIN - ERROR
 CONTINUE 136550
 WRITE (6,5802) 136560
 GO TO 4103 136570
 END

0378 CARDS

A-3.6 SPECIAL SUBROUTINE PARTIAL

SUBROUTINE PRTIAL	70980
IMPLICIT REAL*8 (A-H,O-Z)	70990
LOGICAL*1 ELEVOK,IEND	
	71000
VERSION OF 12/05/68 FOR THE NETWORK ANALYSIS PROGRAM (NAP-2)	71010
FORTAN SUBROUTINE	71020
FOR USE WITH H LEVEL FORTRAN COMPILER ON IBM 360/MOD 95.	71030
	71040
PURPOSE	71050
PRTIAL IS THE CONTROL PROGRAM FOR THE CALCULATION OF THE	71060
PARTIAL DERIVATIVES, FUNCTIONAL DISCREPANCIES, AND PARAMETER	71070
DISCREPANCIES.	71080
	71090
CALLING SEQUENCE	71100
CALL PRTIAL	71110
	71120
INPUT	71130
	71140
OUTPUT	71150
	71160
	71170
	71180
REFERENCE	71190
	71200
METHOD	71210
	71220
	71230
RESTRICTIONS	71240
	71250
	71260
	71270
ACCURACY	71280
FLOATING POINT - ALL CONSTANTS AND VARIABLES ARE CARRIED IN	71290
DOUBLE PRECISION TO 16 DECIMAL DIGITS.	71300
MIN. MAGNITUDE = 1.D-75	71310
MAX. MAGNITUDE = 1.D+75	71320
FIXED POINT - MAGNITUDE OF ALL CONSTANTS AND VARIABLES ARE	71330
.LE. 2147483647	71340
	71350
REQUIRED SUBPROGRAMS - FORTRAN LIBRARY	71360
	71370
	71380
REQUIRED SUBPROGRAMS - OTHER	71390
ERRORP - CONTROL THE PRINT-OUT OF ERROR MESSAGES	71400

C	MEASUR - PARTIAL DERIVATIVES WRT MASTER COORDINATE SYSTEM AND -	71410
C	WRT THE ERROR MODEL COEFFICIENTS	71420
C	REFRCT - REFRACTION CORRECTION	71430
C	ROTFIX - ROTATES VECTOR FROM INERTIAL TO EARTH FIXED COORD.	71440
C	ROTIPT - ROTATION MATRIX FROM EARTH-FIXED TO LOCAL STABLE -	71450
C	COORDINATES.	71460
C	STORAGE REQUIREMENTS	71470
C		71480
C		71490
C	TIMING	71500
C	NO ESTIMATE AVAILABLE	71510
C	ANALYSIS	71520
C	JOE LYNN ,PROJECT LEADER ,DBA SYSTEMS INC.	71530
C	RAUL GARZA-ROBLES ,SEN. PROGRAMMER/ANALYST ,	71540
C	MRS. SHIRAS GUION ,	71550
C	ROBERT DEVANEY ,	71560
C		71570
C	PROGRAMMER	71580
C	ROBERT DEVANEY ,	71590
C		71600
C		71610
C	PROGRAM MODIFICATIONS	71620
C		71630
C		71640
C		71650
C	***** START PROGRAM *****	71660
C		71670
C	COMMON - ARC INFORMATION	71680
	COMMON /COMSOL/ FREP(500) , IFREP(500),NTSPN,NEGTP,IRITKN,KOUT	71690
	COMMON /ACINFO/	71700
	1ACLABL(100) ,EPOCH(100) ,EPOCHD(100) ,GHA(100) ,	71710
	2IROTAT(100) ,IASTAB(100,6) ,IAPNO(100,6)	71720
C		71730
C	COMMON - ARC STABLE PARAMETERS	71740
	COMMON /ASPARM/	71750
	1NOAS ,NOAS2 ,ASLABL(200) ,ASINT(200) ,	71760
	2ASCUR(200) ,ASWT(200) ,ASCWT(200) ,ASDELT(200) ,	71770
	3IASEVL(200) ,AS2LAB(200) ,AS2INT(200)	71780
C		71790
C	COMMON - DEBUG PRINTING	71800
C		71810
	COMMON /CDEBUG/	71820
	1IDEFLG(2) ,IPRFLG(2) ,ISLFLG(2)	71830
C		71840

```

COMMON - PARAMETERS COMPUTED ON INITIAL CALL TO MEASURE
COMMON /CMEASR/
1RANGE
2SINE
,EL
,ROOT
,EDOT
,COSE
71850
71860
71870
71880
71890
71900
71910
71920
71930
71940
71950
71960
71970
71980
71990
72000
72010
72020
72030
72040
72050
72060
72070
72080
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - CONVERSION CONSTANTS LOADED BY MAIN PROGRAM
COMMON /CONMET/
1XMETKM
,XMETFT
,XMETUD
C
COMMON - WORK AREA
COMMON /CWORK/
1IDATA(500)
,DATA(500)
,ICTL
,NINT
2NFLT
71960
71970
71980
71990
72000
72010
72020
72030
72040
72050
72060
72070
72080
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - INTEG I/O
COMMON /CINTEG/ PV(6), VEM(6,6), SV(6), SVEM(6,6), TE, IT
1
,T2
72010
72020
72030
72040
72050
72060
72070
72080
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - GENERAL CONTROL INFORMATION
COMMON /GENCOM/
1CONVG
,DIVRG
,SUMO
,SUML
2COST
,MXITER
,MXDIVG
,ITERNO
AITERSW
,IUNITS
,IGEOFL
,IAUTOR
3IDIVNO
,ISIGNO
,IUPDNO
,IPRES
4IOINP
,NSTA
,MXMEAS
,MXARCS
5NARCS
,MXSTA
,MXLIN
,IPGNO
6MXPARM
PGID(10)
7
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - INTEG I/O
COMMON /EXTCM/ XP(10), YP(10), ZP(10), XV(10), YV(10), ZV(10),
1 BD(10), BT(10), BR(10), BM(10), BG(10), TZ, TF, TJ, TU, DP,
3 EP, SP, CD, D, V, T, NB, NS, NE, NM, NP, NC, KT, KO, KV, KE,
3 KS, LA, LB, LW
72090
72100
72110
72120
72130
72140
72150
72160
72170
72180
72190
72200
72210
72220
72230
72240
72250
72260
72270
72280

COMMON - I/O FILE ASSIGNMENTS
COMMON /IONUMB/
1MFILE
,ISFILE
,IARCIN
,IPASIN
2IARCOT
,IPASOT
,ICARD
,IPASID
3ITAPE
,IALPHA
,LUA
4 LUC
,LUB
72230
72240
72250
72260
72270
72280

COMMON - MEASUREMENT INFORMATION
COMMON /MEAS/
1MFILE
,ISFILE
,IARCIN
,IPASIN
2IARCOT
,IPASOT
,ICARD
,IPASID
3ITAPE
,IALPHA
,LUA
,LUB
4 LUC
,LUB
72230
72240
72250
72260
72270
72280

```



```

2      ' *** PTIAL SPEAKING ***'/ 72710
3      ' ***/ 72720
4      ' *****/ 72730
2 FORMAT('O*** STANDARD FILE FORMAT *** - FOR INTERPRETATION REFER T 72740
10 DOCUMENTATION WITH INDICATED FILE AND ICTL'/ 72750
2'OICTL ='I4/ 72760
3' NINT ='I4/ 72770
4' NFLT ='I4/ 72780
5'OIDATA(I) , I=1,NINT'/(10X,20I5)) 72790
3 FORMAT('ODATA(I) , I=1,NFLT'/(9X,1P6D18.10)) 72800
8 FORMAT('O IASTAB('I3,IH,I1,3H) =I2,'WILL CONTINUE PROCESSING WIT 72840
1H STABILITY FLAG (IASTAB) = 1.') 72850
10 FORMAT('O MASTER TABLE OF MEAS. NUMBERS DOES NOT CONTAIN MEAS. N 72860
10. FOR THIS POINT. PTIAL WILL IGNORE THIS PT..'/ 72870
2' NMS(N) ='I3) 72880
11 FORMAT('O*** ISFILE OUTPUT RECORD ***') 72890
12 FORMAT('O NMEAS AND/OR NPARMS ARE TOO LARGE. PTIAL CANNOT PRO 72900
1CEED.'/5X,'NMEAS ='I5,' , NPARMS ='I5) 72910
13 FORMAT('E = ',D20.12,' E PRIME = ',D20.12/ 72920
1 ' F = ',D20.12,' F PRIME = ',D20.12/ 72930
2 ' G = ',D20.12,' G PRIME = ',D20.12) 72940
15 FORMAT(' TIME',D20.10/' XYZ ',6D20.10/(6D20.10)) 72950
17 FORMAT(' COS(DEC) AND COS(EL) ',2D20.10) 72960
72970
C SET UP C = SPEED OF LIGHT IN APPROPRIATE UNITS 72980
C 72990
C C = 2.997925D8 73000
IF( IUNITS .EQ. 1 ) C = C * XMETKM 73010
IF( IUNITS .EQ. 2 ) C = C * XMETFT 73020
IF( IUNITS .EQ. 3 ) C = C * XMETUD 73030
C 73040
C 73050
ZERO= 0.D0
NUTAPE= 35
NUPASS= 36
NURITE=37
IF(ITERNO.LE.1) REWIND ITAPE
REWIND NURITE
73060
C ALL REFERENCES TO IPRFLG(1) .NE. 0 EXERCISES DEBUG PRINTOUT 73070
C IF((IPRFLG(1).NE.0).AND.(IPRFLG(2).GE.ITERNO)) WRITE (6,1) 73080
C 73090
C INPUT MFILE - ARC NUMBER 73100
C READ (MFILE) 73110

```

1	ICL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)	73120
1000	CONTINUE	
C	NOARC = IDATA(1)	73200
C		73210
C	STORE INFORMATION FOR INTEGRATOR IN /EXTCM/	73220
C		73230
	NOSSEC = IDATA(2)	73240
	NB = IDATA(3)	73250
	NS = IDATA(4)	73260
	NE = IDATA(5)	73270
	NM = IDATA(6)	73280
	NP = IDATA(7)	73290
	NC = IDATA(8)	73300
	KT = IDATA(9)	73310
	KD = IDATA(10)	73320
	KV = IDATA(11)	73330
	KE = IDATA(12)	73340
	KS = IDATA(13)	73350
	LA = IDATA(14)	73360
	LB = IDATA(15)	73370
	LW = IDATA(16)	73380
	TZSEC = DATA(2)	73390
	TZDAY = DATA(1)	73400
	TFSEC = DATA(4)	73410
	TFDAY = DATA(3)	73420
	DO 1003 I=1,10	73430
	XP(I) = DATA(I+4)	73440
	YP(I) = DATA(I+14)	73450
	ZP(I) = DATA(I+24)	73460
	XV(I) = DATA(I+34)	73470
	YV(I) = DATA(I+44)	73480
	ZV(I) = DATA(I+54)	73490
	BD(I) = DATA(I+64)	73500
	BT(I) = DATA(I+74)	73510
	BR(I) = DATA(I+84)	73520
	BM(I) = DATA(I+94)	73530
	BG(I) = DATA(I+104)	73540
1003	CONTINUE	73550
	TZ = DATA(115)	73560
	TF = DATA(116)	73570
	TJ = DATA(117)	73580
	TU = DATA(118)	73590
	DP = DATA(119)	73600
	EP = DATA(120)	73610

SP = DATA(121)	73620
CD = DATA(122)	73630
O = DATA(123)	73640
V = DATA(124)	73650
T = DATA(125)	73660
XPOLAR = DATA(126)	73670
YPOLAR = DATA(127)	73680
C	73690
C	73700
C	73710
C	73720
OUTPUT ISFILE - ARC RECORD - ICTL=1	73730
NINT = 1	73740
NFLT = 1	73750
WRITE (ISFILE)	73760
1 ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)	73770
C	73780
READ (MFILE) ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(FREP(J),J=1,NFLT)	73790
NTSPN = IDATA(1)	73800
NEGTSF = IDATA(2)	73810
DO 1005 I = 1,500	73820
1005 IFREP(I) = 0	73830
IRITKN = 0	73840
KOUT = 0	73850
C	73860
INPUT IARCIN - ARC STABLE PARAMETERS	73870
READ (IARCIN)	73940
1 ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)	73950
1010 IF(ICTL.EQ. 1) GO TO 1020	73960
C	73970
STORE ARC STABLE PARAMETERS NOT ENTERING INTO SOLUTION	73980
NOAS2 = IDATA(2)	73990
DO 1011 I = 1,NOAS2	74000
K = 2*I - 1	74010
AS2LAB(I) = DATA(K)	74020
1011 AS2INT(I) = DATA(K+1)	74030
C	74040
INPUT IARCIN - ARC STABLE PARAMETERS	74050
READ (IARCIN)	74120
1 ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)	74130
1020 NOAS = IDATA(2)	74140
IF(NOAS.EQ. 0) GO TO 1050	74150
C	74160
STORE ARC STABLE PARAMETERS ENTERING INTO SOLUTION	74170
DO 1030 I = 1,NOAS	
K = 6*I - 5	

ASLBLE(I) = DATA(K)	74180
ASINT(I) = DATA(K+1)	74190
ASCUR(I) = DATA(K+2)	74200
ASINT(I) = DATA(K+3)	74210
ASCWT(I) = DATA(K+4)	74220
ASDEL(I) = DATA(K+5)	74230
1030 IASEVL(I) = IDATA(I+2)	74240
	74250
	74260
	74270
C OBTAIN STATE VECTORS AND GENERATE POWER SERIES	74280
	74290
	74300
1050 CONTINUE	74310
IF(NOSEC .LE. 0) GO TO 1060	74320
	74330
C SECONDARY ARC	74340
	74350
	74360
REWIND LUC	74370
N = NOSEC	74380
LW = 1	74390
LB = LUC	74400
IRET = 1	74410
GO TO 1900	74420
1060 CONTINUE	74430
IRTKN1 = IRTKN	74440
	74450
C PRIMARY ARC	74460
	74470
REWIND LUB	74480
N = NOARC	74490
LW = 1	74500
LB = LUB	74510
IRET = 2	74520
GO TO 1900	74530
1070 CONTINUE	74540
KOUT = IRTKN1	74550
IPS1 = 1	74560
IPS2 = 1	74570
	74580
C INPUT MFILE - PASS/STATION RECORD - ICTL=2	74590
READ (MFILE)	74600
1 ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)	
2000 CONTINUE	

C STORE PASS INFORMATION 74670

C 2010 NOSTA = IDATA(2) 74680

NOPASS = IDATA(3) 74690

NMEAS = IDATA(4) 74700

NPARMS = IDATA(5) 74710

IF((NMEAS .LE. 30) .AND. (NPARMS .LE. 300)) GO TO 2018 74720

74730

74740

74750

74760

74770

74780

74790

C *** ERROR CONDITION

2014 CONTINUE

WRITE(6,12) NMEAS,NPARMS

GO TO 7100

2018 DO 2020 I = 1,NMEAS

LO(I)=0

QSUM(I)=0.00

QSQ(I)=0.00

K = 3*I + 3

NOMEAS(I) = IDATA(K)

NRFC(I) = IDATA(K+1)

NRC(I) = IDATA(K+2)

K = 4*I - 3

ELMIN(I) = DATA(K)

ELMAX(I) = DATA(K+1)

RINDEX(I) = DATA(K+2)

2020 WGTM(I) = DATA(K+3)

74800

74810

74820

74830

74840

74850

74860

74870

74880

74890

74900

C STORE PARAMETER TABLE

ITEMP = 3 * NMEAS

DO 2025 I = 1,NPARMS

K = 4*I + ITEMP - 3

NPMEAS(I) = IDATA(K+5)

NEMT(I) = IDATA(K+6)

NOPARM(I) = IDATA(K+7)

2025 NPTYPE(I) = IDATA(K+8)

L=0

74980

74990

75000

75010

75080

75090

75100

75110

75120

C INPUT IPASIN - PASS STABLE PARAMETERS

READ (IPASIN)

1 ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)

2100 IF(ICTL .EQ. 1) GO TO 2200

C

C STORE PASS STABLE PARAMETERS NOT ENTERING INTO SOLUTION

NQPS2 = IDATA(4)

DO 2110 I = 1,NQPS2

```

K = 2*I - 1
PS2LAB(I) = DATA(K)
2110 PS2INT(I) = DATA(K+1)
C
C INPUT IPASIN - PASS STABLE PARAMETERS
  READ (IPASIN)
  I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)
2200 NOPS = IDATA(4)
  IF(NOPS.EQ. 0) GO TO 2250
C
C STORE PASS STABLE PARAMETERS ENTERING INTO SOLUTION
  DO 2230 I = 1,NOPS
    K = 6*I - 5
    PCLABL(I) = DATA(K)
    PSINT(I) = DATA(K+1)
    PCCUR(I) = DATA(K+2)
    PSIWT(I) = DATA(K+3)
    PSCWT(I) = DATA(K+4)
    PSDEL(I) = DATA(K+5)
    2230 IPSEVL(I) = IDATA(I+4)
C
C OUTPUT ISFILE (FOR SOLVER) - PASS RECORD - ICTL=2
2250 ICTL = 2
  NINT = NMEAS + 4
  NFLT = NMEAS
  IDATA(4) = NMEAS
  DO 2275 I = 1,NMEAS
    IDATA(I+4) = NMEAS(I)
  2275 DATA(I) = WGTN(I)
  WRITE (ISFILE)
  I ICTL,NINT,NFLT,(IDATA(I),I=1,NINT),(DATA(I),I=1,NFLT)
C
C ROTATION MATRIX FROM EARTH-FIXED TO LOCAL STABLE COORDINATES
  = TLC(1,1) TO TLC(3,3)
C
C TRANSLATION VECTOR
  = TLC(1,4) TO TLC(3,4)
C
  CALL ROTINT(STLAT(NOSTA),STLON(NOSTA),STHT(NOSTA),TLC)
C
C APPLY POLAR MOTION IF DEFAULTS OF 0.000 ON X,Y ANGLES WERE OVERRIDDEN
C
  E = TLC(1,4)
  F = TLC(2,4)
  G = TLC(3,4)

```

```

TLC(1,4) = E - XPOLAR * G
TLC(2,4) = F + YPOLAR * G
TLC(3,4) = G + XPOLAR * E - YPOLAR * F
IF ((IPRFLG(1) .EQ. 0) .OR. (ITERNO .GT. 1)) GO TO 2280
WRITE (6,13) E,TLC(1,4) , F,TLC(2,4) , G,TLC(3,4)
2280 CONTINUE
SAVE1 = TLC(1,1)
SAVE2 = TLC(2,1)
C
C
C STATION OFFSETS
      = TLC(1,5) TO TLC(3,5)
DO 2300 I = 1,3
2300 TLC(I,5) = 0.00
C
C SEARCH ERROR MODEL TABLE FOR SURVEY CORRECTIONS , IF ANY
C
DO 2500 I=1,NPARMS
IF((NEMT(I)-LT.7).OR.(NEMT(I).GT.9)) GO TO 2500
K= NPTYPE(I)
GO TO (2410,2420,2430,2440,2450,2460), K
2410 TLC(NEMT(I)-6,5) = TSCUR(NOPARM(I))
GO TO 2500
2420 TLC(NEMT(I)-6,5) = ASCUR(NOPARM(I))
GO TO 2500
2430 TLC(NEMT(I)-6,5) = PSCUR(NOPARM(I))
GO TO 2500
2440 TLC(NEMT(I)-6,5) = TS2INT(NOPARM(I))
GO TO 2500
2450 TLC(NEMT(I)-6,5) = AS2INT(NOPARM(I))
GO TO 2500
2460 TLC(NEMT(I)-6,5) = PS2INT(NOPARM(I))
2500 CONTINUE
C
C INPUT MFILE - MEASUREMENT POINT RECORD - ICTL=3
7000 CONTINUE
READ (MFILE,END=7100)
1 ICTL,NINT,NFLT, (IDATA(I),I=1,NINT), (DATA(I),I=1,NFLT)
GO TO (5100,5100,3000), ICTL
C
C *** NORMAL EXIT ***
7100 IEND=.TRUE.
IF(L.GT.0) GO TO 5110

```

7105	REWIND ISFILE	
	REWIND NUTAPE	
	REWIND NUPASS	
	REWIND MFILE	76070
	REWIND IARCIN	76080
	REWIND IPASIN	76090
	RETURN	76100
C		76110
C	PROCESS MEASUREMENT POINT DATA	76120
	3000 CONTINUE	
C		76190
C	STORE MEASUREMENT POINT DATA	76200
	3010 NMSPT = NINT	76210
	DU 3020 I = 1,NMSPT	76220
	NMS(I) = IDATA(I)	76230
	3020 DMS(I) = DATA(I+2)	76240
C		76250
C	DTARR = DELTA TIME FOR AVERAGE RANGE RATE DATA	76260
C		76270
C	DTARR = DATA (NMSPT + 3)	76280
C		76290
C		76300
C	CURRENT TIME OF MEAS. PT. (JULIAN DAYS SINCE 1950)	76310
	TDCURR = DATA(1)	76320
C		76330
C	TIME IN SECONDS OF GIVEN DAY	76340
	TSCURR = DATA(2)	76350
C		76360
	L=L+1	
	TIMSEC(L)=TSCURR	
	DO 3030 I=1,NMEAS	
3030	QMEAS(L,I) = 1.D50	
3040	CONTINUE	
C	T FOR NAP INTEG = TIME(SEC) FROM MIDNIGHT OF EPOCH DAY	76370
	T1 = EPOCHD(NOARC)	76380
	DTDAY = TDCURR - EPOCHD(NOARC)	76390
	T2 = DTDAY * 86400.D0 + TSCURR	76400
C		76410
C		76420
C		76430
C	SOLVE FOR VECTOR AND MATRIZANT	76440
C		76450
C		76460

TT= TDCURR*86400.D0 + TSCURR

TMP = TT - TJ	76480
C PRIMARY ARC	76580
C	76590
3050 CONTINUE	76600
CALL SOFORT(IPS1,LUB,0,DO,TMP,D,V,T,PV,VEM)	76610
C	76620
C	76650
IPS1 = 2	76660
GRHA = GHA (NOARC)	76670
C	76680
C ROTATE STATE VECTOR FROM INERTIAL TO EARTH-CENTERED/EARTH FIXED COORD	76690
CALL ROTFIX(PV,T2)	76700
C	76710
C	76720
NPAK = 0	76730
C	76740
C SAVE PARAMETERS THAT WOULD BE DESTROYED BY MEASUR	76750
3270 CONTINUE	76760
SAVE3 = PV(1)	76770
C ***	76780
C *** MAIN LOOP -- PROCESS EACH MEASUREMENT FOR THIS POINT	76790
C ***	
IF(NMSPT.LE.0) GO TO 6100	76800
DO 4000 N = 1,NMSPT	76810
DO 3200 I = 1,NMEAS	76820
IF(NMS(N).NE. NOMEAS(I)) GO TO 3200	76830
MINDEX = I	76840
GO TO 3250	76850
3200 CONTINUE	76860
C *** ERROR CONDITION	76870
C	
C MEAS. NO. FOR THIS PT DOES NOT MATCH MASTER TABLE OF MEAS. NUMBERS	76880

WRITE(6,10) NMS(N)	76890
GO TO 4000	
C RESTORE PARAMETERS THAT ARE DESTROYED BY MEASUR	76910
C	76920
C	76930
3250 CONTINUE	76940
TLC(1,1) = SAVE1	76950
TLC(2,1) = SAVE2	76960
PV(1) = SAVE3	76970
MS = MSTYPE(NOMEAS(MINDEX))	76980
C	76990
C AVERAGE RANGE-RATE DATA (MYTYPE=18)	77000
C PRIMARY ARC ONLY	77010
C	77020
IF (MS .NE. 18) GO TO 3254	77030
RPLUS = 0.0D0	77040
RMINUS = 0.0D0	77050
DTARR2 = DTARR/2.0D0	77060
TMPI = TMP + DTARR2	77070
C	77080
CALL SOFORT(IPS1,LUB,0.0D0,TMPI,D,V,T,PV1,AVVEM)	77090
T3 = T2 + DTARR2	77100
CALL ROTFIX(PV1,T3)	77110
C COMPUTE RANGE FOR TIME + DT/2 (RPLUS)	77120
DO 3252 I=1,3	77130
TMPI = PV1(I) - TLC(I,4)	77140
RPLUS = RPLUS + TMPI * TMPI	77150
3252 CONTINUE	77160
RPLUS = DSQRT (RPLUS)	77170
C	77180
TMPI = TMP - DTARR2	77190
C	77200
CALL SOFORT(IPS1,LUB,0.0D0,TMPI,D,V,T,PV1,AVVEM)	77210
T3 = T2/- DTARR2	77220
CALL ROTFIX(PV1,T3)	77230
C	77240
C COMPUTE RANGE FOR TIME - DT/2 (RMINUS)	77250

```

VALUE = (RPLUS - RMINUS) / DTARR
C
3254 CONTINUE
C
C
C
C MEASUR RETURNS RANGE,EL,RDOT,EDOT,SINE,COS FOR JTERM = 0
C
C CALL MEASUR( MS, 0, TLC, PV, VALUE )
C
C SAVE COS(DEC)
C
C COSDEC = VALUE
C VALUE = 0.000
C
C COMPUTE COS(ELEV)
C COSL = DCOS(EL)
C IF ((IPRFLG(1).GE.2).AND.(ITERNO.LE.IPRFLG(2))) WRITE(6,17)
C 1 COSDEC,COSL
C
C CHECK FOR ACCEPTABLE ELEVATION
C
C
C
C ELEVOK=.TRUE.
C IF((EL.LT.ELMIN(MINDEX)).OR.(EL.GT.ELMAX(MINDEX))) ELEVOK=.FALSE.
C
C ELEVATION OK
C 3300 CONTINUE
C
C CLEAR ARRAYS FOR SAVING PARTIAL DERIVATIVES OF VECTOR
C DO 3290 I=1,6
C NBDO(I) = 0
C NBDOOS(I) = 0
C BDO(I) = 0.00
C BDOS(I) = 0.00
C 3290 CONTINUE
C
C CALL MEASUR WITH JTERM=1 TO GET CALCULATED MEASUREMENT
C CALL MEASUR( MS, 1, TLC, PV, VALUE )
C
C DO 3500 I = 1,NPARMS
C IF(NOMEAS(MINDEX) .NE. NPMEAS(I)) GO TO 3500
C

```

```

C   FOR ERROR MODEL TERMS GE 10, FIND CURRENT PARAMETER VALUE
C
IF( NEMT(I) .EQ. 1 ) GO TO 3390
IF (NEMT(I) .LT. 10) GO TO 3380
K = NPTYPE(I)
GO TO (3310,3320,3330,3340,3350,3360), K
3310 CONTINUE
TLC(1,1) = TSCUR(NOPARM(I))
GO TO 3380
3320 CONTINUE
TLC(1,1) = ASCUR(NOPARM(I))
GO TO 3380
3330 CONTINUE
TLC(1,1) = PSCUR(NOPARM(I))
GO TO 3380
3340 CONTINUE
TLC(1,1) = TS2INT(NOPARM(I))
GO TO 3380
3350 CONTINUE
TLC(1,1) = AS2INT(NOPARM(I))
GO TO 3380
3360 CONTINUE
TLC(1,1) = PS2INT(NOPARM(I))
3380 CONTINUE
CALL MEASUR( MS, NEMT(I), TLC, PV, VALUE )
C
C   CHECK FOR PARAMETER EVALUATION TYPE 2 - NOT TRANSMITTED TO SOLVER
C       NPTYPE(I) = 4  TOTALLY STABLE - NOT ENTERING SOLUTION
C       = 5  ARC STABLE - NOT ENTERING SOLUTION
C       = 6  PASS STABLE - NOT ENTERING SOLUTION
C
3390 CONTINUE
IF(L.GT.0) GO TO 3500
IF(.NOT.ELEVOK) GO TO 3500
IF(NPTYPE(I) .GT. 3) GO TO 3500
IF (MS .EQ. 2) PV(1) = PV(1) * COSEL
IF (MS .EQ. 4) PV(1) = PV(1) * COSDEC
NPAR = NPAR + 1
ITEMP = NPAR + NMSPT
ITEMP1 = 3*NPAR + NMSPT - 2
C
C   IF PARTIAL OF VECTOR WRT MEAS, SAVE IT FOR ROTATION IT INERTIAL COORD
C
IF(NEMT(I) .GT. 6 ) GO TO 3400

```



```

      NBD0(NEMT(I)) = ITEMP + 2
      BDO(NEMT(I)) = PV(1)
      3400 CONTINUE
C
C
C   PARAMETER
      IDATAW(ITEMP1+2) = NPTYPE(I)
C   PARAMETER NUMBER
      IDATAW(ITEMP1+3) = NOPARM(I)
C   MEASUREMENT NUMBER
      IDATAW(ITEMP1+4) = NPMEAS(I)
C   PARTIAL
      DATAW(ITEMP + 2) = PV(1)
      3500 CONTINUE
C
C   IF NO PARTIALS OF VECTOR, SKIP ROTATION
      IF( NBD0(1) .LE.0 ) GO TO 3540
C
C   ROTATE PARTIALS OF VECTOR FROM FIXED TO INERTIAL COORDINATES
      CALL ROTPAR( BDO, T2 )
C
C   RELATE VECTOR TO EPOCH TIME
      DO 3520 K=1,6
      BDOM(K) = 0.00
      DO 3520 J=1,6
      3520 BDOM(K) = BDOM(K) + BDO(J) * VEM(J,K)
C
      DO 3530 J=1,6
      3530 DATAW(NBD0(J)) = BDOM(J)
C
      3540 CONTINUE
C
C   CHECK FOR PARTIALS OF SECONDARY VECTOR
      IF( NBD0S(1) .LE. 0 ) GO TO 3570
C   ROTATE TO INERTIAL
      CALL ROTPAR( BDO, T2 )
C   RELATE TO EPOCH VIA MATRIZANT
      IF ((IPRFLG(1).GE.2) .AND. (ITERNO .LE. IPRFLG(2))) WRITE (6,15)
      1  T, (SV(I), I=1,6), ((SVEM(I,J), I=1,6), J=1,6)
      DO 3550 K=1,6
      BDOM(K) = 0.00
      DO 3550 J=1,6
      3550 BDOM(K) = BDOM(K) + BDO(J) * SVEM(J,K)

```

78180
78190
78200
78210
78280
78290
78310
78330
78350
78370
78380
78390
78400
78410
78420
78430
78440
78450
78460
78470
78480
78490
78500
78510
78520
78540
78550
78560
78570
78580
78590
78600
78610
78620
78630
78640
78650
78660
78670

C			78680
	00 3560 J=1,6		78690
	3560 DATA(NBDOOS(J)) = BDOM(J)		78700
C			78710
	3570 CONTINUE		78720
C			78730
C			78740
C	CALL MEASUR WITH ACTUAL MEASUREMENT VALUE FOR CORRECT SIGN FOR		78750
C	ANGULAR DATA		78760
C			78770
C			78780
C			78790
	PV(1) = DMS(N)		78800
	CALL MEASUR(MS, -1, TLC, PV, VALUE)		78810
	IF(NRFRG(MINDEX) .EQ. 0) GO TO 3600		78820
C			78830
C	REFRACTION CORRECTION		78840
	CALL REFRACT(RINDEX(MINDEX),STLAT(NOSTA),MS,CORR)		78850
	VALUE = VALUE + CORR		78860
C			78870
C	MEASUREMENT NUMBERS		78890
	3600 IF (L.LE.0) GO TO 6000		78900
C			78910
C	MEASUREMENT DISCREPANCIES		78920
	DATA(N + 2) = DMS(N) - VALUE		78930
	IF (IOINP .EQ. 6) DATA(N+2) = -DMS(N)		78940
	IF (IOINP .LT. 7).AND.(MS.EQ.2)) DATA(N+2) = DATA(N+2) * COSEL		
	IF (IOINP .LT. 7).AND.(MS.EQ.4)) DATA(N+2) = DATA(N+2) * COSDEC		
	IF(L.LE.0) GO TO 6000		
	QMEAS(L,MINDEX) = DATA(N+2)		
	QSUM(MINDEX) = QSUM(MINDEX) + DATA(N+2)		
	QSQ(MINDEX)= QSQ(MINDEX) + DATA(N+2)*DATA(N+2)		
	LO(MINDEX)= LO(MINDEX) + 1		
	4000 CONTINUE	79050	
	IF(L.GT.0) GO TO 7000		
C	OUTPUT ISFILE - MEASUREMENT RECORD - ICTL=3	79070	
	4010 CONTINUE		
	ICTL=3		
	JFLT=NMSPT+2+NPARG		
	JINT=JFLT+2+NPARG		
	IDATAW(1)=NMSPT		
	IDATAW(2)=NPARG		
	WRITE(ISFILE) JCTL,JINT,JFLT,(IDATAW(1),I=1,JINT),(DATAW(1),I=1,		
	*JFLT)		
	DATAW(1)= NOARG		

```

DATAW(2)= ISTDID(NOSTA)
DATAW(3)= NOPASS
IF(LQ(1).GT.0) GO TO 4020
DMS(2)= DMS(1)
DMS(1)= 0.00
CSQ(1)= 0.00
4020 IF(LQ(2).GT.0) GO TO 4030
DMS(2)= 0.00
CSQ(2)= 0.00
4030 WRITE(NTAPE) ZERO,DATAW(1),DATAW(2),DATAW(3),ZERO,ZERO
WRITE(NTAPE) TDCURR,TSCURR,DMS(1),DMS(2),ZERO,ZERO
WRITE(NUPASS) NOSTA,NOPASS,LO,OSQ
WRITE(NURITE)NOARC,NOPASS,ISTDID(NOSTA),STLABL(NOSTA),
*ELEVOK,LMEAN,LA,QSQ,DMS(1),DMS(2),TDCURR,TSCURR,
*(TIMSEC(L),L=1,LA),((QMEAS(L,I),L=1,LA),I=1,2)
IF(IEND) GO TO 7105
GO TO 5105

```

79060

C

```

5100 IEND=.FALSE.
IF(L.GT.0) GO TO 5110
5105 IF(ICIL-1) 1000,1000,2000
5110 LMEAN=(L+1)/2
NMSPT=0
DO 5140 LL=1,NMEAS
IF(LQ(LL).LE.0) GO TO 5140
NMSPT= NMSPT+1
NMS(NMSPT)= NOMEAS(LL)
QSUMT= QSUM(LL)
QSQT= QSQ(LL)
5120 IF(LQ(LL).LE.1) GO TO 5150
QL= LQ(LL)
LA=0
QBAR= QSUMT/QL
SIGMAT= DSQRT((QSQT-QSUMT*QBAR)/(QL-1.00))
TWSIG=3.00*SIGMAT
QSQT= QSQ(LL)
QSUMT= QSUM(LL)
DO 5130 LB=1,L
IF(DABS(QMEAS(LB,LL)-QBAR).LE.TWSIG) GO TO 5125
IF(QMEAS(LB,LL).GE.0.1050) GO TO 5130
QSUMT= QSUMT- QMEAS(LB,LL)
QSQT= QSQT- QMEAS(LB,LL)*QMEAS(LB,LL)
GO TO 5130
5125 LA=LA+1

```

5130 CONTINUE
IF(LA.GE.LO(LL)) GO TO 5135
LO(LL)= LA

GO TO 5120

5135 QSUM(LL)=QBAR

QSQ(LL)= SIGMAT

5140 CONTINUE

IF(TSCURR.LT.TIMSEC(LMEAN)) TDCURR=TDCURR-1.00

TSCURR=TIMSEC(LMEAN)

DATAW(1)=TDCURR

DATAW(2)=TSCURR

LA=L

L=0

GO TO 3040

5150 QSQ(LL)=0.00

GO TO 5140

6000 DMS(N)=QSUM(MINDEX)

IF(MS.EQ.2) DMS(N)= DMS(N)/COSEL

IF(MS.EQ.4) DMS(N)=DMS(N)/COSDEC

DMS(N)=DMS(N) + VALUE

DATAW(N+2)=QSUM(MINDEX)

IDATAW(N+2)=NMS(N)

IF(ELEVOK) GO TO 4000

DATAW(N+2)=0.00

IDATAW(N+2)=0

GO TO 4000

C

6100 NMSPT=1

IDATAW(3)=0

DATAW(3)=0.00

GO TO 4010

C

C

C ROUTINE TO PICK UP STATE VECTORS AND GENERATE POWER SERIES

C N = ARC NO.

C

C

C

1900 CONTINUE

BG(NC) = GHA(N) + EPOCH(N) * ROTAT

REWIND LUA

DO 1960 I=1,6

XX(I) = 0.00

ITEMP = IASTAB(N,I)

GO TO (1920,1930,1910,1940,1950,1910),ITEMP

79220

79230

79240

79250

79260

79270

79280

79290

79300

79310

79320

79330

79340

C		79350
C	ERROR	79360
1910	CONTINUE	79370
	WRITE (6,8) N,I,ITEMP	79380
	GO TO 1960	79390
C		79400
C	TOTALLY STABLE ENTERING INTO SOLN	79410
C		79420
	1920 XX(I) = TSCUR(IAPNO(N,I))	79430
	GO TO 1960	79440
C		79450
C	ARC STABLE ENTERING INTO SOLN	79460
C		79470
	1930 XX(I) = ASCUR(IAPNO(N,I))	79480
	GO TO 1960	79490
C		79500
C	TOTALLY STABLE NOT IN SOLN	79510
C		79520
	1940 XX(I) = TS2INT(IAPNO(N,I))	79530
	GO TO 1960	79540
C		79550
C	ARC STABLE NOT IN SOLN	79560
C		79570
	1950 XX(I) = AS2INT(IAPNO(N,I))	79580
	1960 CONTINUE	79590
C		79600
C	STORE IN /EXTCM/	79610
C		79620
	XP(NP) = XX(1)	79630
	YP(NP) = XX(2)	79640
	ZP(NP) = XX(3)	79650
	XV(NP) = XX(4)	79660
	YV(NP) = XX(5)	79670
	ZV(NP) = XX(6)	79680
C		79690
C	TJ IS EPOCH TIME (1950.0) IN SECONDS	79700
C		79710
	TJ = EPOCHD(N)*86400.00 + EPOCH(N)	79720
	TE = TJ	79730
C		79740
C	TZ IS INTEG START TIME	79750
C	TF IS INTEC STOP TIME	79760
C		79770
	TZ = 0.00	79780

TSTART = TZSEC + TZDAY * 86400.D0
TFINAL = TFSEC + TFDAY * 86400.D0

79790
79800
79810
79820
79830
79840
79850
79860
79870

IF(TSTART .GE. TJ) GO TO 1970
IF(TJ .GE. TFINAL) GO TO 1980

C ARC SPANS EPOCH -- MUST INTEG TWO SUBARCS

TF = TFINAL - TJ
CALL KICKER(2)
TF = TSTART - TJ
CALL KICKER(2)
GO TO 1990

79880
79890
79900
79910
79920
79930
79940
79950
79960

C ARC FOLLOWS EPOCH

1970 CONTINUE

TF = TFINAL - TJ
CALL KICKER(2)
GO TO 1990

79970
79980
79990
80000
80010
80020

C ARC PRECEDES EPOCH

1980 CONTINUE

TF = TSTART - TJ
CALL KICKER(2)
1990 CONTINUE

GO TO (1060,1070), IRET

C END OF POWER SERIES ROUTINE

C
END

80030
80040
80050
80060
80070
80080
80090
80100
80110

0385 CARDS

Appendix A-4
Constraints Imposed on
NAP-II Deck Setup

A-4.1 CONSTRAINTS IMPOSED BY MINITRACK PREPROCESSOR

There are constraints imposed on the NAP-II deck setup by the preprocessing program. This appendix is an attempt to outline the constraints in a concise, quick-reference form.

The Minitrack Preprocessor (Section 2.2.3) imposes an order to the stations in NAP-II (Key 1, Category 201), depending on the order the Minitrack data is preprocessed (data set 5 of Minitrack Preprocessor). The station ID's required by the NAP-II program are generated from the fifty-fifth and fifty-sixth characters of the Minitrack message format (Section 2.2.1). This code is used for the equatorial data, and the code plus 100 is used for the polar data.

Example: Station constants for Minitrack processor are in the following order:

Ft. Meyers
Quito
Lima
Santiago
Newfoundland.

The following information would be generated by the preprocessor for each station:

	Equatorial		Polar	
	Sta. ID	Sta. No.	Sta. ID	Sta. No.
Ft. Meyers	03	1	103	2
Quito	05	3	105	4
Lima	06	5	106	6
Santiago	08	7	108	8
Newfoundland	12	9	112	10

However, if the station's constants have been in order of:

Newfoundland

Santiago

Lima

Quito

Ft. Meyers,

then the information generated would be

	Equatorial		Polar	
	Sta. ID	Sta. No.	Sta. ID	Sta. No.
Newfoundland	12	1	112	2
Santiago	08	3	108	4
Lima	06	5	106	6
Quito	05	7	105	8
Ft. Meyers	03	9	103	10

The station numbers are required on the NAP-II cards (Key 1 of Category 301 and Key 2 of Category 201 and 202) punched by the preprocessor program. The station identification is required in Keys 3 and 4 of the Category 301 card.

Pass numbers are also generated in the preprocessor and are punched in Key 3 of the Category 201, 202, and 999 cards.

In summary, the following information is generated for the Minitrack Preprocessor for the NAP-II program.

- | | | | |
|----|----------------|--------------|-------|
| A. | STATION ID | Category 301 | Key 4 |
| B. | STATION NUMBER | Category 301 | Key 1 |
- 1) Even number for polar
 - 2) Odd number for equatorial

- C. Start and Stop times of the data pass Category 201 and 202
- D. End of pass control card Category 999.

A-4.2 CONSTRAINTS IMPOSED BY THE PRE-NAP PROGRAM

This program is used to modify, add, or delete NAP-II control cards.

The following are the instructions for its usage:

- | | |
|-----------|--|
| INS I1 | Inserts cards after sequence number I1. |
| DEL I1 I2 | Deletes cards between (and including) sequence numbers I1 and I2. |
| REP I1 I2 | Deletes cards between (and including) sequence numbers I1 and I2, and then inserts cards |
| MOD I1 I2 | Modifies cards between (and including) sequence numbers I1 and I2. |

Format for above four cards (A4, x, I5, 5x, I5) note that INS, DEL, REP, and MOD start in column 1 and that column 2 should be blank.

INS and REP must be followed by the cards to be inserted. The cards must be followed by a blank card to signify the end of the particular set of inserted cards.

The MOD cards must be followed by a modifying card. Columns not to be modified should be left blank.

When using the computed mid-point Minitrack data, the Category 704 cards have to be deleted from the control cards. The "704" cards should be used only when the entire data spans are used.

A-4.3 CONSTRAINTS IMPOSED ON NAP-II SETUP

A very basic assumption made when processing Minitrack data is that a good estimate of the state vector is available. This is the basis of the whole process.

The a priori sigma information should be realistically assigned with respect to the error model terms and the observed data.

When processing with the "single-data, point pen pass" data file, be sure to delete Category 704 cards that were used for the processing of the entire observed data file.

Measurement numbers (Category 701) have a limitation as to their assignment. Odd measurement numbers are reserved for cosine alpha (ℓ) measurements, and even numbers are reserved for cosine beta (m) measurements. This limitation is imposed by the Post-NAP processor.

Error model term definition cards (Category 601 cards) must be in order of totally stable, arc stable, and pass stable. There can be only one 601 card for each error model term. Duplicates inserted to override a previous 601 card are not permitted.

A-4.4 ADDITIONAL CONSTRAINTS

This section is reserved for constraints not mentioned above that have not come to light. If, in the course of reducing Minitrack data, using the procedure outlined in this report, new constraints are found, please note them in this section.